A SURVEY OF
POLYCHLORINATED BIPHENYLS
IN AMBIENT AIR IN ONTARIO

PHASE II - VOLUME II

METEOROLOGICAL CORRELATION FOR A 1979
SURVEY OF POLYCHLORINATED BIPHENYLS

Final Report

Report ARB-025-81-ARSP

TD 887 .P64 S87 1981

Ministry of the Environment

The Honourable Keith C. Norton, Q.C., Minister

Gérard J. M. Raymond Deputy Minister LIBKARY

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METEOROLOGICAL CORRELATION FOR A 1979 SURVEY OF POLYCHLORINATED BIPHENYLS

Final Report

MOE Report-ARB-025-81-ARSP

Prepared by

International Environmental Consultants

for

Ontario Ministry of Environment Air Resources Branch 880 Bay Street, Toronto

ONTARIO MINISTRY
OF THE ENVIRONMENT

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AIR RESOURCES BRANCH DIRECTOR

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METEOROLOGICAL CORRELATIONS FOR
A SURVEY OF POLYCHLORINATED
BIPHENYLS IN THE PROVINCE OF ONTARIO

31 MARCH 1981

Prepared for:

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This report is part of a series of reports published by the Ministry of the Environment, Air Resources Branch - on the development of techniques for collection, detection and determination of Polychlorinated Biphenyls in ambient air and results of surveys performed in Ontario in the periods of Sept.-October 1979 and June 1981. The reports of this series are:

ARB-TDA-08-80-Phase I - Development of Laboratory and Field Procedures

ARB-011-81-ARSP-Phase II - Volume I; Sampling Site Selection and Analytical Procedures.

ARB-025-81-ARSP-Phase II - Volume II; Meteorological
Correlation for the 1979
Survey of Polychlorinated
Biphenyls in Air in Ontario.

ARB-026-81-ARSP-Phase III - 1980 Survey of Polychlorinated Biphenyls in Air in Ontario.

This series of reports should be considered as a unit, and the individual members of the series should be evaluated in concert with the other members. This situation arises since this work was developmental in nature and the reports present a chronological picture of the work done over period of time on the sampling, sample processing and analytical procedures. The Phase III Report describes the current state-of-the-art for PCB sampling and analysis as developed by MOE Scientists.

DISCLAIMER

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A SURVEY OF POLYCHLORINATED BIPHENYLS IN THE PROVINCE OF ONTARIO

ONTARIO MINISTRY OF THE ENVIRONMENT

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1.0 SUMMARY

IEC International Environmental Consultants Ltd. was retained by the Ontario Ministry of the Environment to operate samplers at six sites in the Toronto area during the 28 day province wide survey of PCB's conducted in September - October, 1979. IEC was also retained to conduct data analysis for all 25 sites sampled in the survey using PCB concentration data supplied by the Ministry and meteorologic data obtained from the Ministry and Atmospheric Environment Service of Environment Canada.

The purpose of the survey was to provide data on ambient PCB levels at the 25 sites which were selected by MOE and to correlate the measured PCB concentrations with meteorological conditions during the sampling period.

The data reduction and analysis were intended to demonstrate whether any significant correlations between PCB concentration and the meteorological factors wind direction, wind speed, and air temperature existed.

Linear regression correlations between PCB concentration and meteorological parameters were performed. Few significant correlations between PCB concentration and temperature or standard deviation of temperature were found. Sixty-five statistically significant correlations between PCB concentration and wind direction were found, while thirty-four significant correlations between PCB concentration and wind speed were obtained.

Further examination of eighteen of the most significant correlations showed that while all were statistically significant, the data were skewed such that the correlations were based on relatively few data points. Consequently, the correlations should be interpreted as trends.

2.0 INTRODUCTION

In June 1979 the Ontario Ministry of the Environment invited proposals for a "Survey of Polychlorinated Biphenyls in Ambient Air in the Province of Ontario". The intent of the program was to obtain baseline data on ambient PCB concentrations in a summer survey and in a winter survey at 25 stations in Ontario and to evaluate the significance of correlations between PCB concentrations and meteorologic data at each station. In addition to this, there was to be an intensive survey in the Mississauga area during a test burn of PCB-containing oil at the St. Lawrence Cement Plant.

The program was subsequently reduced to one province-wide survey undertaken in September-October, 1979. This report presents the results of the evaluation of PCB concentration and meteorologic data for correlations, along with all computer output for the September-October, 1979 survey. Raw meteorologic data for each station have been submitted in a separate report.

3.0 DATA ACQUISITION AND REDUCTION

3.1 Meteorological Data

The meteorological data used in the regression analyses were obtained from the Ontario Ministry of the Environment, the Atmospheric Environment Service of Environment Canada and Ontario Hydro. Meteorologic data were obtained from the stations listed in Table 1. As there were 25 PCB sampling stations and only 13 meteorologic stations, data from one meteorologic station frequently was used at more than one PCB sampling station for purposes of correlation as indicated in Table 2.

TABLE 1: METEOROLOGICAL STATIONS

Station Name	Station Address
1. MOE-14016	Opposite Lambton generating station, Hwy. 40, Courtright
2. MOE-12032	Windsor (not used - temperature data not available)
3. MOE-12034	C.P. Tower, Riverside Drive, Windsor
4. AES-LOND	London Airport (London-A)
5. MOE-29026	Brampton/Woodward Avenue, Hamilton
6. MOE-27049	Niagara Falls (Temp. from AES-St. Catherines "A")
7. MOE-35033	Evans/Arnold Ave. Etobicoke
8. MOE-33003	Lawrence/Kennedy Ave. Scarborough
9. MOE-45025	Ritson Rd./Olive Ave. Oshawa (Temp. from AES, Oshawa
	Water Pollution Control Plant).
10. AES-KING	Kingston "A", Kingston Airport
11. MOE-77025	CKNC TV Tower, Frood Road, Sudbury
12. AES-TBAY	Thunder Bay "A", Thunder Bay Airport
13. HYD-NANT	Ontario Hydro, Nanticoke Generating Station

The data consisted of hourly readings of temperature, wind speed and wind direction. Where meteorological data was missing at a particular location the missing data were obtained from another source. Originally, the MOE station at Allanburg was to be used rather than the one at Niagara Falls. However, instrument failures resulted in an unacceptably high percentage of missing data (>50%). Temperature data were not available at the Niagara Falls location, but were obtained from the AES St. Catherine's "A" Station. Similarly, the temperature data for MOE-45025 (Oshawa) were obtained from AES. These stations provide only daily temperature maxima and minima, therefore an average, calculated for each day, was used.

Wind direction data are coded by AES into 36 classes of 10 degrees each. Thus the actual degree reading is approximately equal to ten times the class number. Because the classes used by AES, and by IEC in the preparation of this report, were different (ie. 36 classes of 10 degrees by AES versus 16 classes of 22.5 degrees by IEC) one degree was subtracted from the reading obtained by multiplying AES classification by 10. This prevented any intersection of class limits and allowed an immediate verification that wind direction data were originally coded.

The formula used to translate classes back to degrees was:

Direction = (CODE X 10) -1

This gave a reading in degrees which was approximately centered in the code class defined by AES. MOE and Ontario Hydro data were not coded.

Wind speed values were given in nautical miles per hour in the AES Data. A conversion factor of 1.852 (CRC, 1973) was used to convert the data to units of km/hour. MOE and Ontario Hydro data were available in metric units.

Copies of raw meteorological data output are provided in a separate volume of this report.

TABLE 2: LOCATION OF PCB SAMPLING SITES

PCB Station	Location	Met Station
BUR-S-U1	Burlington, Urban	MOE - 29026
HAM-S-I1	Hamilton, Industrial	MOE - 29026
HAM-S-I2	Hamilton, Industrial	MOE - 29026
HAM-S-U1	Hamilton, Urban	MOE - 29026
HAM-S-U2	Hamilton, Urban	MOE - 29021
KIN-S-U1	Kingston, Urban	AES - KING
LON-S-U1	London, Urban	AES - LOND
MIS-S-U1	Mississauga, Urban	MOE - 35033
MIS-S-U2	Mississauga, Urban	MOE - 35033
MIS-S-U3	Mississauga, Urban	MOE - 35033
MIS-S-U4	Mississauga, Urban	MOE - 35033
MOR-S-U1	Mooretown, Urban	MOE - 12034
NAN-S-R1	Nanticoke, Rural	HYD - NANT
NAN-S-R2	Nanticoke, Rural	HYD - NANT
OSH-S-U1	Oshawa, Urban	MOE - 45025
STC-S-R1	St. Catherines, Rural	MOE - 27049
SAR-S-I1	Sarnia, Industrial	MOE - 14016
SAR-S-U1	Sarnia, Urban	MOE - 14016
SUD-S-S1	Sudbury, Suburban	MOE - 77025
SUD-S-R1	Sudbury, Rural	MOE - 77025
THU-S-R1	Thunder Bay, Rural	AES - TBAY
THU-S-U1	Thunder Bay, Urban	AES - TBAY
TOR-S-S1	Toronto, Suburban	MOE - 33003
TOR-S-U1	Toronto, Urban	MOE - 33003
WIN-S-U1	Windsor, Urban	MOE - 12034

Note: U = Urban, I = Industrial, S = Suburban, R = Rural

3.2 PCB Data

Blank-corrected PCB data for each site were provided to IEC by MOE. No modification or editing was performed. PCB station names and locations are given in Table 2.

PCB samplers were operated on a 24 hour basis, but the time at which sampling started and stopped varied slightly from day to day at each station and varied substantially between stations. The average start time for each station was determined from the field data sheets and input to the computer along with the PCB data. This was done to achieve as close a match between sampling periods (of 24 hours) and meteorological data as possible.

While most stations started the study period on the 27th of September, two did not. These were BUR-S-U1, which started on the 26th of September, and KIN-S-U1, which started on the 29th of September. The meteorological data files used with these stations were modified to give correct results with these stations.

Listings of the PCB data files used are provided in Appendix 1.

3.3 Data Reduction

A computer program was developed to perform the data analysis. It had provisions for entering and modifying PCB and meteorological data, and performed the correlation analysis between any PCB sampling station and any meteorological station. A complete listing of the program, written in BASIC, is provided in Appendix 2.

Linear correlation analysis was used to calculate correlation coefficients. MOE uses similiar programs to correlate such parameters as suspended particulate matter and wind direction.

3.4 Statistical Calculations

The calculation of means, standard deviation, linear regression constants and correlation coefficients were performed using standard formulae. They are given below:

A. Mean
$$Mean = \frac{\sum x_i}{\sum x_i}$$

x_i - ith data point
n - total number of data points

B. Standard Deviation

$$= \sqrt{\sum x_i^2 - n(Mean)^2}$$
n-1

Source - Barrowdale, Roberts, Ehle, "Elementary Computer Applications", Toronto, 1974.

C. Correlation Coefficient

$$r = \frac{\sum x_i y_i - \frac{1}{n} \sum x_i \sum y_i}{\sqrt{(\sum x_i^2 - \frac{1}{n} (\sum x_i)^2)} \times (\sum y_i^2 - \frac{1}{n} (\sum y_i)^2)}$$

Source - Barrowdale, Roberts, Ehle, ibid.

D. Linear Regression Constants

Slope =
$$\frac{n\Sigma xy - \Sigma x\Sigma y}{n\Sigma x^2 - (\Sigma x)^2}$$

Source - Barrowdale, Roberts, Ehle, ibid.

The t-test was used to evaluate the significance of the correlation coefficients calculated for each data set. The test was based on the null hypothesis that the calculated regression line was not significantly different from a line of zero slope (representing the mean value of all "y" values).

The formula used to calculate the value of the t-statistic is as follows:

$$t = \frac{r\sqrt{n-2}}{1-r^2}$$

Where: r = correlation coefficient

n = number of data points

Source: Volk, "Applied Statistics for Engineers", Toronto, 1958.

Thus, if a correlation is found to have t-value greater than the tabulated value at the 90% confidence limit but less than that for the 95% confidence limit then the null hypothesis is false at the 90% confidence level, but remains true at the 95% level and the correlation is therefore significant at the 90%, but not at the 95% level.

There are two possible errors which may result from any statistical test of this type, known as Type 1 and Type 2. Type 1 are those in which the null hypothesis is rejected (ie said to be false) when it is not, while Type 2 is the reverse, that is, it is said to be true when in fact it is false.

Since these are mirror images of each other, it follows that attempting to eliminate the possibility of a Type 1 error may result in a Type 2 error. The way to avoid this is to increase the sample size.

Statisticians commonly state that a 90% significance level is the minimum level for a correlation to be accepted as significant, while the 95 and 99% levels are better, and tend to balance Type 1 and Type 2 errors the best, as well. Consequently, these three levels have been used in the assessment of the significance of the correlations between PCB concentrations and meteorologic data.

The correlations to be performed were:

- 1) PCB concentration vs wind direction class
- 2) PCB concentration vs wind speed
- 3) PCB concentration vs ambient temperature
- 4) PCB concentration vs standard deviation of daily temperature

The approach used in the program was as follows:

- 1) load PCB data file for one station and sampling start time
- 2) load corresponding meteorological data file
- 3) calculate daily average temperatures, with "day" starting at start time for the PCB station
- calculate standard deviation of daily temperatures from daily mean temperatures
- 5) classify wind direction into 16 classes
- 6) classify wind speeds into five classes
- 7) normalize absolute counts (number of hours per wind direction) obtained in (5) and (6) above to % time
- 8) perform linear regression analysis as outlined above
- 9) output results in tabular form
- 10) output wind direction results in histogram form.

Output from all stations is provided in Appendix 3 of this report. The program requires approximately 40 Kbytes of memory to run, divided between program storage, 17 Kbytes and data storage, 23 Kbytes.

4.0 RESULTS AND DISCUSSION

4.1 PCB Data

In general, the standard deviation for each station was high, indicating a large day-to-day variability in ambient PCB concentration. While there was only one station in which standard deviation exceeded the mean, in most cases the standard deviation was at least 66% of the mean.

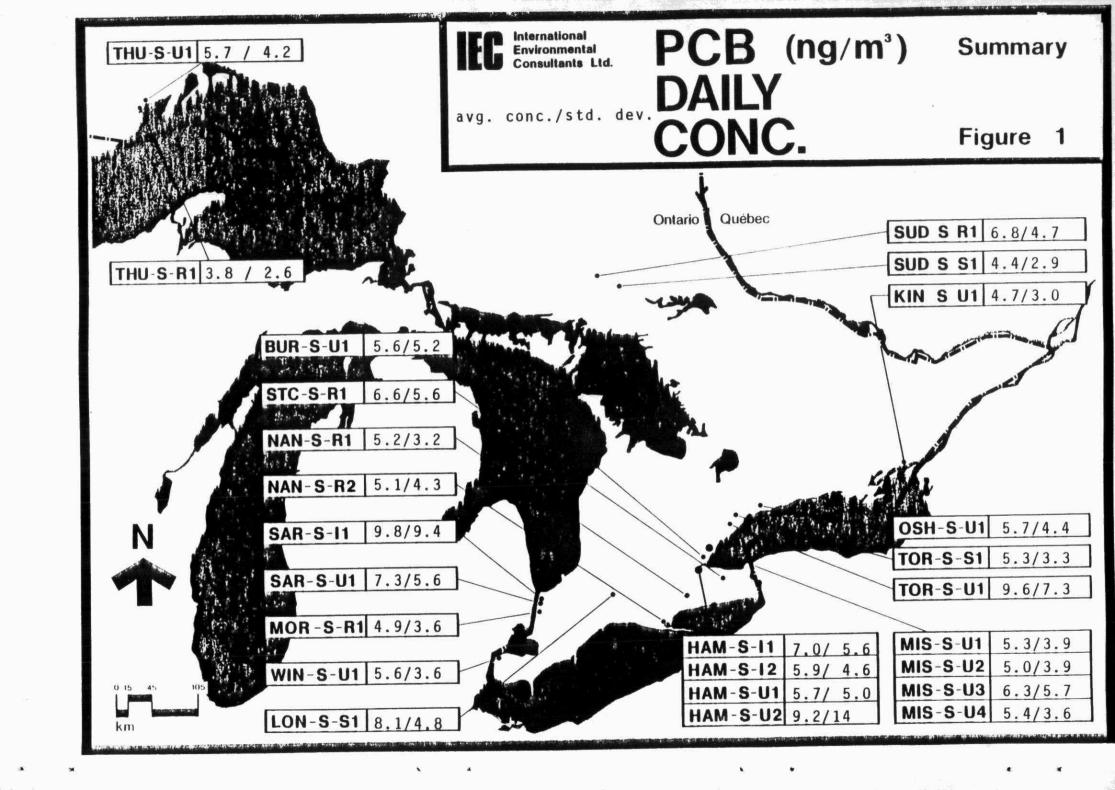
A map of Ontario indicating the 25 sampling sites is presented in Figure 1. The mean and standard deviation of the PCB concentrations at each site during the study are shown. Daily concentrations for all stations are shown on similiar maps in Appendix 4.

4.2 Correlations

The use of a simple linear regression analysis to determine possible relationships between the PCB concentration and the various meteorological parameters is not a statistically rigorous treatment of the data. To be accurate, multiple correlation analysis incorporating all of the meteorological parameters in the study would have to be performed. This would ensure that there are no internal correlations, for instance, between wind direction and wind speed. If this were the case, then a strictly rigorous treatment of the problem would demand that the statistically less significant variable be discarded and the regression re-run. Meteorologists commonly assume that there is no significant relation between the various parameters on a large scale over a long period of time. A 28 day time

TABLE 3: RAW PCB DATA STATISTICS

STATION	# VALID OBSERVATIONS	MIN ₃ (ng/m ³)	MAX (ng/m ³)	MEAN ₃	STANDARD DEVIATION
BUR-S-UI	25	1.0	24	5.6	5.2
HAM-S-11	26	1.1	22	6.9	5.6
HAM-S-12	25	1.0	18	5.9	4.6
HAM-S-UI	25	1.0	22	5.7	5.0
HAM-S-U2	26	1.2	74	9.2	13.9
KIN-S-UI	24	0.4	10	4.7	3.0
LON-S-UI	18	0.4	18	8.1	4.8
MIS-S-UI	24	0.9	15	5.3	3.9
MIS-S-U2	25	0.8	15	4.9	3.9
MIS-S-U3	25	0.6	21	6.3	5.7
MIS-S-U4	27	0.9	15	5.3	3.6
MOR-S-U1	26	0.6	16	4.8	3.6
NAN-S-R1	27	1.0	14	5.2	3.7
NAN-S-R2	27	0.9	18	5.1	4.3
0SH-S-U1	26	1.0	14	5.7	4.4
STC-S-RI	26	1.6	23	6.6	5.6
SAR-S-II	24	0.6	21	7.3	5.6
SAR-S-UI	24	1.8	47	9.8	9.4
SUD-S-SI	24	1.0	12	4.4	2.9
SUD-S-R1	26	1.7	17	6.8	4.7
THU-S-R1	26	0.7	10	3.8	2.6
THU-S-UI	27	1.3	13	5.7	4.2
TOR-S-SI	23	1.6	15	5.3	3.3
TOR-S-UI	25	1.9	32	9.6	7.3
WIN-S-UI	27	1.5	16	5.6	3.6
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period should minimize these problems as well as provide an adequate data base to begin to define ambient and background levels of PCB's in the Province of Ontario.

4.2.1 Correlations Between PCB Concentration and Temperature

A total of five significant correlations with average daily temperature were found; only two of these were significant at the 95% level, while the others were significant at the 90% level. Table 4 summarized all the calculated correlation coefficients.

Correlations with standard deviation of daily temperature were performed to provide a rough estimate of the behaviour of PCB's contained in the atmosphere under varying conditions of atmospheric stability. It was anticipated that few significant correlations would be found and that those that did occur would have negative correlation coefficients. Increasing standard deviation of temperature would indicate less atmospheric stability, and thus greater mixing between boundary layer and upper atmosphere, with resultant dilution of PCB concentration. The calculated correlation coefficient are given in Table 4. Of the three significant correlations found only one had the expected negative correlation coefficient.

4.2.2 Correlations Between PCB Concentration and Wind Direction and Speed

The calculated correlation coefficients for PCB concentration with wind direction classes are presented in Table 5a. Those correlations which are statistically significant are presented in Table 5b. A summary of the number of statistically significant correlations by wind direction and level of significance is presented in Table 6.

The values of the t statistic necessary for the correlations to be significant at the 90%, 95% and 99% levels are given in Table 7. In this case, a significance of 90% means that in one out of 10 cases, a correlation rejected as insignificant will actually be significant. (ie. a Type 2 error).

TABLE 4: CORRELATION COEFFICIENTS - PCB CONCENTRATION vs TEMPERATURE

	STATION	٧S	AVERAGE TEMPERATURE	100112000	STD. DEV. TEMPERATURE
					4
	BUR-S-U1		0.0515		-0.0711
	HAM-S-I1		0.0662		0.0593
	HAM-S-I2		0.2656		2.1025
	HAM-S-U1		0.2065		0.0185
	HAM-S-U2		0.3026		-0.1843
	KIN-S-U1		0.0604		-0.0784
	LON-S-U1		0.4046		-0.1239
	MIS-S-U1		0.3772		0.0824
	MIS-S-U2		0.3819		0.1799
	MIS-S-U3		0.41152		-0.0368
	MIS-S-U4		0.0561		0.4323 ²
	MOR-S-U1		0.0620		-0.1325
	NAN-S-R1		0.2734		0.0477
	NAN-S-R2		0.2593		0.3069
	OSH-S-U1		0.3630		0.0234
	STC-S-R1		0.1142		-0.4103 ²
	SAR-S-I1		0.45742		-0.0901
	SAR-S-U1		0.1983		0.0722
	SUD-S-S1		0.0247		0.4341 ²
	SUD-S-R1		0.2400		-0.0089
	THU-S-R1		0.0257		-0.0043
	THU-S-U1		0.3643 ¹		0.1211
	TOR-S-S1		0.3391		0.0248
	TOR-S-U1		0.3218		-0.1867
	WIN-S-U1		0.1847		0.0021
12					

NOTES - 1 Significant at 90% level

² Significant at 95% level

TABLE 5a: CORRELATION COEFFICIENTS - PCB CONCENTRATION vs WIND DIRECTION CLASS

STATION	N	NNW	NW	WNW	¥	wsw	2₩	SSW
BUR - S - U1	0.2958	-0.37121	-0.1369	0.43242	0.62273	0.8443	-() (0) 71	-0.0713
HAM-S-I1	0.3160	-0.0727	-0.0482	0.2605	0.1895	0.0785	-0.0171 0.3931	0.0727
HAM-S-12	0.7321 3	-0.0010	0.1681	0.5093	0.5299	0.1426	-0.0820	-0.1615
HAM-S-U1	0.72273	-0.1344	0.1613	0.45992	0.54363	0.3327	0.1250	-0.0643
HAM-S-U2	-0.0935	-0.0636	-0.1543	-0.0139	-0.0055	-0.0951	-0.0977	-0.0643
KIN-S-U1	-0.2596	-0.1219	0.1512	-0.2005	0.1367	-0.0708	0.0359	0.1201
LON-S-U1	0.3625	0.2424	0.2488	0.3447	0.1954	0.3767	-0.0370	-0.0106
MIS-S-Ul	0.2094	-0.0125	0.0424	0.0008	-0.2945	0.0122	0.1261	0.7300
MIS-S-U2	0.1722	-0.1291	-0.1151	-0.0338	-0.3041	-0.1594	-0.1238	0.5295
MIS-S-U3	0.2654	0.1986	0.2539	0.0018	-0.3110	-0.1617	0.1086	0.5092
MIS-S-U4	0.0261	-0.2145	-0.2132	-0.0110	-0.0629	-0.0466	-0.062	0.2137
MOR-S-U1	0.0074	-0.1259	0.0522	-0.0446	0.2403	-0.0706	0.0871	0.6312
NAN-S-R1	0.2930	0.1346	0.1011	0.0714	-0.0267	-0.0404	-0.0903	-0.1094
NAN-S-R2	0.1686	0.2673	0.42452	0.35601	0.1329	0.0539	0.0779	0.0091
OSH-S-U1	-0.0339	0.1694	0.1031	0.2262	0.3041	-0.1369	-0.0831	-0.0419
STC-S-R1	0.46712	0.2050	0.0226	0.0108	-0.2817	0.39282	0.42682	0.1035
SAR-S-11	0.1560	0.63923	0.55413	0.1033	0.1906	-0.1124	-0.0809	0.1460
SAR-S-U1	0.1910	0.68943	0.48272	-0.0768	0.0127	-0.1419	-0.2020	-0.0449
SUD-S-S1	0.3011	0.2631	0.36591	0.2370	0.0455	0.2379	0.0683	-0.2234
SUD-S-R1	-0.1342	-0.0731	-0.0098	-0.0150	-0.2319	-0.0415	-0.2562	-0.2153
THU-S-R1	0.0403	-0.0242	-0.3871	-0.2591	-0.52313	-0.41272	-0.2781	0.0076
THU-S-U1	0.3096	-0.0784	-0.4469 ²	-0.34961	-0.4645 ²	-0.2287	-0.0330	0.2052
TOR-S-S1	0.5794 3	0.42802	0.36821	-0.0724	-0.0075	0.52052	0.1704	0.2928
TOR-S-U1	0.1983	0.1952	0.48562	0.43772	0.1238	0.35091		0.4360
WIN-S-U1	0.1983	0.0026	0.38282	0.4377	0.1238		-0.0417	
W1H-3-01	0.0423	0.0020	0.3826	0.3430	0.6304	0.1538	0.3062	0.2074
STATION	S	SSE	SE	ESE	E	ENE	NE	NKE
BUR-S-U1	0.0287	-0.2513	-0.1657	-0.0449	0.2071	0.0612	-0.0181	-0.0791
HAM-S-I1	0.0844	-0.1929	-0.0904	0.1598	-0.1896	-0.1388	-0.0348	-0.1115
HAM-5-12	0.0728	-0.1704	-0.3172	0.0062	-0.3012	-0.1304	0.1906	0.0726
HAM-S-U1	0.1082	-0.2781	-0.3650 ¹	-0.0412	-0.2122	-0.1047	0.1227	0.0470
HAM-S-U2	-0.1304	0.53643	0.2755	-0.1530	-0.1837	-0.1203	-0.0167	-0.0068
KIN-S-U1	0.1135	0.0436	0.0778	-0.1389	-0.2572	-0.1907	0.2087	-0.2102
LON-S-U1	0.1689	0.0438	-0.2064	-0.0770	-0.2976	-0.3088	0.0429	-0.0640
MIS-S-U1	0.51332	-0.0455	-0.2863	-0.1776	-0.0137	-0.0471	-0.0998	0.0728
MIS-S-U2	0.61213	-0.0003	-0.1503	-0.1216	0.0380	0.2083	-0.0496	0.0023
MIS-S-U3	0.55173	-0.0146	-0.2070	-0.2442	0.0686	0.0133	-0.1703	0.0785
MIS-S-U4	0.38432	-0.0349	-0.1555	-0.2299	0.0039	0.0881	0.1416	0.1702
MOR-S-U1	0.45252	-0.2678	-0.1002	0.0049	-0.2279	-0.1216	-0.0854	-0.0086
NAN-S-R1	0.0519	-0.1448	-0.1309	0.0047	-0.0026	-0.0529	-0.0689	0.1810
NAN-S-R2	0.1301	-0.0829	-0.3787 1	-0.1546	-0.2362	-0.2168	0.0602	0.1918
OSH-S-U1	-0.3666 1	0.0138	0.43672	0.0741	0.1455	-0.0038	-0.0182	0.0865
STC-S-R1	0.0291	0.0174	-0.2176	0.0128	-0.2502	-0.0728	0.0045	-0.2394
SAR-S-II	0.0745	-0.2743	-0.2042	-0.1562	-0.2680	0.0065	-0.1695	
SAR-S-U1	0.1293	-0.1657	-0.1234	-0.1982	-0.1359	-0.0753	-0.0309	0.1347
SUD-S-51	-0.3493 1	-0.2118	-0.1939	-0.0419	-0.1029	-0.1478	0.0441	0.0706
SUD-S-R1	0.1761	0.4312 2	0.2421	0.0929	0.2845	0.3844	-0.0758	
THU-S-R1	0.4745 2	0.3700 1	0.4168 2	0.3393 1	0.1910	0.52843	0.1518	0.0068 0.3323
THU-S-U1	0.40272	0.2891	0.2172	0.2400	0.0811	0.3164	0.35492	0.3323
TOR -S -S1	0.1021	-0.1051	-0.3156	-0.4361 ²	-0.1958	-0.1848	-0.1761	0.0504
TOR-S-U1	-0.0578	-0.2699	-0.3805 ¹	-0.2770	-0.0070	-0.1297	-0.1761	
AND DESCRIPTION OF THE PARTY OF								0.0204
NIN-S-U1	0.0054	-0.2850	-0.2889	-0.1810	-0.0758	-0.0729	0.0380	-0.0543

Notes: 1 Significant at 90% level

² Significant at 95% level

³ Significant at 99% level

TABLE 5b: SIGNIFICANT CORRELATIONS - PCB CONCENTRATIONS vs WIND DIRECTION

TATION	N	MIN	No.	WNW	W	WSW	SW	228
IUR-S-U1		-0.37121		0.43242	0.6227 3	0.84483		
AM-S-I1		0.3/10		01,300,3		aa	0.39312	
AM-S-12	0.73213			0.5293	0.52993			
AM-S-U1	0.72273			0.45992	0.5436 3			
M-S-U2				1 months minimum 1				
IN-S-U1								
N-S-U1								
IS-S-Ul								0.7306 ³
IS-S-U2								0.52993
IS-S-U3								0.56923
S-S-U4								
R-S-U1								0.63123
N-S-R1								
N-S-R2			0.42452	0.3560 ¹				
H-S-U1								
C-S-R1	0.46712					0.39282	0.42682	
R-S-11		0.63923	0.55413					
AR-S-U1		0.68943	0.48272					
JD-S-S1		o-testa FOFOIL	0.36591					
JD-S-R1								
HU-S-R1			-0.3871 1		-0.5231 ³	-0.41272		
IU-S-U1			-0.4469 ²	-0.3496 ¹	-0.4645 ²			
R-S-S1	0.5794 3	0.42802	0.3682			0.52052		
DR-S-U1	0.0754		0.48562	0.43772		0.35091		0.43602
IN-S-U1			0.38282	0.34361	0.63043	(A. 10 (A		
114-3-07								
TATION	S	322	SE	ESE	E	ENE	NE	NNE
								- 189/E
UR - S - U 1						ş		
AM-S-I1								
AM-S-12			-0.3650 ¹					
M-S-U1		70 20 20 1	-0.3650					
M-S-U2		0.53643						
N-S-U1								
N-S-U1	10 CO - CO - CO							
S-S-U1	0.51332							
S-S-U2	0.61213							
IS-S-U3	0.5517 ³							
15-5-44	0.38432							
DR-S-U1	0.45252							
N-S-R1			540					
AN-S-R2			-0.3787 1					
H-S-U1	-0.3666 ¹		0.4367 2					
C-S-R1								
IR-S-11								
AR-S-U1								
JD-S-S1	-0.3493 ¹							
JD-S-R1		0.4312 2				0.38441		
IU-S-R1	-0.4745 2	0.3700 1 .	0.4168 2	0.3393 ¹		0.5284 3		0.33231
	0.4027 1	(227)				0.3364	0.3849 ²	
IU-S-U1				-0.4361 2				
HU-S-U1 DR-S-S1								
DR-S-S1			-0.3805 ¹					
			-0.3805 ¹					

Notes: 1 Significant at 90% level

Significant at 95% levelSignificant at 99% level

TABLE 6: SIGNIFICANT CORRELATIONS - PCB CONCENTRATION vs WIND DIRECTION

SIG	NIFICANC	E				h	IND DIR	ECTION											
	(%)	N	NNW	NW	WNW	W	WSW	SW	SSW	S	SSE	SE	ESE	Ε	ENE	NE	NNE	TOTAL	
	90	:-	1	3	3	(—)	1	9 -	-	2	1	3	1	: - 5	2	215-	1	18	
	95	1	1	5	3	1	3	2	-	5	1	2	1	2 .= 8	:-	1	-	29	
	99	3	2	1	1	5	1	a - a	4	2	1	-	-		1		(=)	18	
тот	AL	4	4	9	7	6	5	2	4	9	3	5	2	0	3	1	1	65	

TABLE 7: ABSOLUTE VALUE OF t-STATISTIC NECESSARY FOR GIVEN SIGNIFICANCE LEVELS

# VALID	90%	95%	99%
DAYS	SIGNIFICANCE	SIGNIFICANCE	SIGNIFICANCE
Š.			
20	1.734	2.181	2.878
21	1.729	2.593	2.861
22	1.725	2.086	2.845
23	1.721	2.888	2.631
24	1.717	2.074	2.819
25	1.714	2.369	2.807
26	1.711	2.064	2.797
27	1.708	2.060	2.787
28	1.706	2.056	2.779
			Service Company

Table 8 presents the correlation coefficients found for PCB concentration versus wind speed and Table 9 presents a survey of the statistically significant correlations.

When interpreting the results of correlation analyses, care must be taken to avoid attributing greater importance to the correlations than is justified. As an example, at station SAR-S-U1 the correlation coefficient for PCB concentration versus wind from the north-northwest is 0.6894, and is significant at the 99% level. Examination of a graph of the data, included as Figure 2, shows that the majority of the points, are on the ordinate of the graph. Thus the data are skewed towards the lower end of the graph, and the correlation is being based primarily on the four other points on the graph. Consequently, the correlations should be interpreted as trends in most cases. The solution to this type of problem is a larger data base. Plots of a representative number of the most significant correlations are given in Appendix 5.

In general, sources of PCB's may be characterized as local, medium range and long range. To identify a local source conclusively, it must be encompassed by sampling stations, thus allowing observation during all wind conditions. The correlation with wind speed, however, can provide an indication of the distance of the sample site from the source. A significant positive correlation between PCB concentration and a single wind direction, combined with a significant positive correlation with wind speeds of 0-5 km/hr may imply local or medium-range sources of PCB's. As internal correlations may exist between wind direction and speed, it is not possible to draw more definite conclusions without undertaking multiple regression or vector analysis of the data. This was beyond the scope of this project.

No province-wide trends in correlations of PCB concentrations with transport of PCB's based on the data presented in this report because of potential interferences from local meteorologic conditions. As discussed in this section, however, there are definite trends suggesting short and medium range transport at many stations. The use of the histogram plots produced by the computer program makes identification of these trends relatively easy. A discussion of trends at each sampling station follows.

TABLE 8: CORRELATION COEFFICIENT - PCB CONCENTRATION vs WIND SPEED

		WIND SPEED) (km/hr.)		
STATION	0-5	5-10	10-15	15-20	>20
BUR-S-U1	0.2825	0.0596	0.0241	-0.874	-0.2678
HAM-S-I1	0.3116	0.1667	0.2997	-0.2075	-0.4617 ²
HAM-S-I2	0.6204 ³	0.0674	0.6818	-0.3898 ¹	-0.3945 ¹
HAM-S-U1	0.6898 ³	-0.0453	-0.0038	-0.4231 ²	-0.3792 ¹
HAM-S-U2	-0.0453	-0.2067	-0.4222 ²	-0.2502	0.5517 ³
KIN-S-U1	0.3978 ¹	-0.0679	-0.3995 ¹	-0.2705	0.0970
LON-S-U1	0.0740	0.3181	0.1910	-0.0953	-0.3011
MIS-S-U1	0.2650	-0.1669	-0.0348	-0.2510	0.0317
MIS-S-U2	0.0648	-0.0576	0.0586	-0.1168	0.0129
MIS-S-U3	0.2094	0.0517	-0.1781	-0.3142	0.0397
MIS-S-U4	-0.1753	-0.0267	0.1475	-0.0303	0.5189 ³
MOR-S-U1	0.1761	-0.0703	0.0207	-0.1090	-0.0907
NAN-S-R1	0.4108 2	0.1790	-0.0558	-0.2350	-0.3278 ¹
NAN-S-R2	0.3120	0.33831	-0.1065	-0.2508	-0.3408 ¹
0SH-S-U1	0.1502	-0.1700	-0.0690	-0.0289	-0.0498
STC-S-R1	0.4558 ²	-0.3894 ²	-0.3383 ¹	-0.2015	-0.0820
SAR-S-I1	0.1303	0.2478	0.2160	-0.1676	-0.2769
SAR-S-U1	-0.0028	0.1189	0.4367 ²	-0.0639	-0.2548
SUD-S-S1	-0.2911	0.2502	0.2360	0.1466	-0.1300
SUD-S-R1	-0.3625 ¹	-0.4082 ²	-0.3532 ¹	0.2445	0.5320 ³
THU-S-R1	0.4328 ²	0.2115	-0.3900 ²	-0.3583 ¹	-0.2125
THU-S-U1	0.4788 ²	-0.0227	-0.4141 ²	-0.2886	-0.0181
TOR-S-S1	0.3130	-0.0217	-0.1559	-0.2261	-0.1976
TOR-S-U1	0.5177 ³	-0.0177	-0.3975 ¹	-0.3325	-0.3139
WIN-S-U1	0.5775 ³	0.1731	-0.4769 ²	-0.4194 ²	-0.2981

Notes: 1 Significant at 90% level

² Significant at 95% level

³ Significant at 99% level

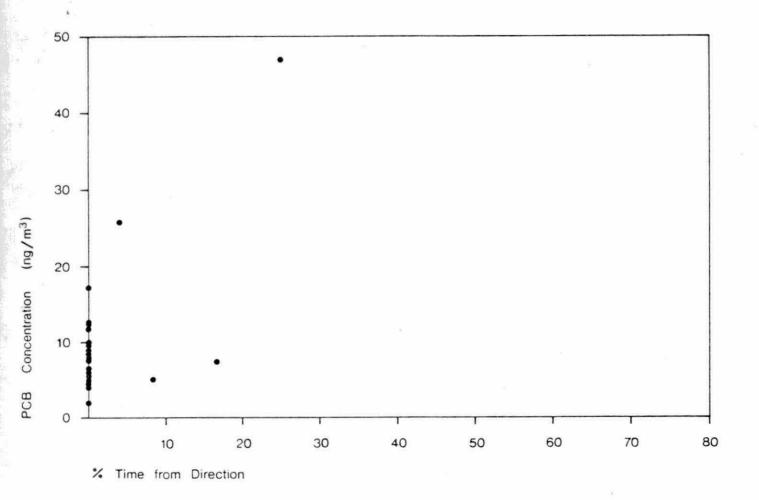
TABLE 9 SIGNIFICANT CORRELATIONS - PCB CONCENTRATION vs WIND SPEED

SIGNIFICAN	ICE 0-5	5-10	WIND S	PEED (km/hr. 15-20) >20	TOTAL
90	2	1	4	2	4	13
95	4	2	5	2	1	14
99	4	*	=	-	3	7
TOTAL	10	3	9	4	8	34

Figure 2

PCB Concentration vs Wind Direction Class

Station SAR-S-U1
Direction NNW





BUR-S-U1

A definite trend is observed when winds are coming from the west towards the station. The largest correlation coefficient observed, 0.8448, was found at this station. There is a large electrical substation to the south-southwest of the station. As the Niagara escarpment is northwest of the station, it is possible that this resulted in local wind direction being different from that recorded at Hamilton airport from which the meteorological data was obtained. Graphs of the data for the west and west-southwest directions are provided in Appendix 5. There were no significant correlations with wind speed.

HAM-S-I1

A 95% signficance level correlation was found with winds from the southwest. A general trend may also be inferred with winds ranging from WNW through S. A 95% level correlation was found with winds in the >20 km/hr class. As this was a negative correlation, it implies that cleaner air was coming into the area during periods of high winds. This implies accumulation of PCB's from anthropogenic sources in the urban envelope, with dispersal during periods of high winds.

HAM-S-I2

A high correlation coefficient was found when winds were from the north. A trend was also found from the NW to the WSW directions. The largest correlation coefficient in that quadrant was with winds from the west. When winds were from the east, a negative correlation coefficient was found. This suggests local or medium range sources. This is supported by a 99% level correlation with wind speeds in the 0-5 km/hr class. It is further supported by the 90% level negative correlations with wind speeds in the 15-20 and >20 km/hr classes, which suggests that cleaner air enters the area during periods of high winds. A graph of the data for wind from the north and the 0-5 km/hr wind speed class is provided in Appendix 5.

HAM-S-U1

The same trends and patterns as were found at HAM-S-II were found at this station. A plot of data for wind from the north and the 0-5 km/hr wind speed class is given in Appendix 5.

HAM-S-U2

In contrast to the previous stations, only the south-southeast direction showed a significant correlation, which may indicate local sources. The >20 km/hr class showed a 99% level positive correlation, suggesting that this station may be further from the source than the previous stations, as well. A plot of the >20 km/hr wind speed class data is given in Appendix 5.

KIN-S-U1

This is an excellent example of a substantially clean area. There is no significant pattern apparent from examination of the histogram, but the 0-5 and 10-15 km/hr classes both showed correlations at the 90% level. This could be due to the skewed data problem outlined earlier or it could be local sources. The west-east pair show that a source may be located to the west of the site, but the correlations are not statistically significant, and so no definite conclusion can be drawn from the data.

LON-S-U1

While no significant correlations were found at this station, the pattern suggests that PCB's may be transported from the Sarnia area. This is supported by a corresponding pattern at the Sarnia sites.

MIS-S-U1, MIS-S-U2, MIS-S-U3, MIS-S-U4

A trend with winds ranging from S to SW is evident at these stations, with the south-southwest direction showing the highest correlation coefficient of 0.7306. All of the stations in Mississauga showed this pattern. This may be indicative of a local source generally to the south-southwest of the stations, as the stations in Toronto (TOR-S-Ul and TOR-S-Sl) did not show this pattern under similar meteorological conditions. A report prepared by the Ontario Research Foundation for the Ministry entitled "An Assessment of Atmospheric PCB Levels in Mississauga" found similar results using sampling sites very near to the ones used in this study. Plots of the data for winds from the south at stations -U2 and -U3, and from the south-southwest at stations -U1 and -U3 are given in Appendix 5. Only MIS-S-U4 had a significant correlation with wind speed, this being in the >20 km/hr class at a significance level of 99%.

MOR-S-U1

A trend indicating sources to the south-southwest was found at this station, with the south-southwest correlation having a 99% significance level. No significant correlations with wind speed were found.

NAN-S-R1

While there were no significant correlations with wind direction at this station, a trend was observed with winds coming from the NNE through to WNW. A 95% significance level correlation was found for the 0-5 km/hr wind speed class and a 90% level negative correlation was found for the >20 km/hr class. These trends suggest the possibility of medium range transport from a generally northerly direction.

NAN-S-R2

At this station, the pattern observed at NAN-S-R1 is repeated, but the correlations with winds from the northeast and west-northwest had 95% and 90% significance levels, respectively. The south-southeast showed a 90% level negative correlation. This tends to support the trend inferred above for the northerly direction and indicates relatively cleaner air enters the area from the southeast.

OSH-S-U1

There was a 95% level correlation with wind direction from the southeast at this station, suggesting local sources. A trend was also apparent in the NNW to W directions, although the correlations were not statistically significant.

STC-S-R1

The correlation data indicate local sources to the north and possibly to the west-southwest and south-southwest of this station. All three directions had correlations significant at the 95% level. The 0-5 km/hr wind speed class showed a 95% significance level correlation while the 5-10 and 10-20 km/hr classes showed 95% and 90% level significant correlations, respectively, indicating short to medium range transport.

SAR-S-I1, SAR-S-U1

Both of these stations showed trends indicating PCB sources to the north-northwest. The generally east-southeast direction showed negative correlations, showing that the London area is not a significant source of PCB's. The 10-15 km/hr wind speed class at station SAR-S-U1 showed a 95% significant correlation. It should be noted that while a statistically significant correlation was found for the NNW wind direction at SAR-S-U1, the data are too limited to indicate more than a trend, as indicated in Figure 2. Plots of SAR-S-I1 data for winds from the NW and NNW, and SAR-S-U1 for winds from the NNW are given in Appendix 5.

SUD-S-S1

Winds from the south gave a 90% significant negative correlation at this station. A general positive trend with winds from the northwest quadrant was found, but no statistically significant correlations were obtained.

SUD-S-R1

A 95% significant correlation was found with winds from the south-southeast. Correlation for the south and southeast are elevated but not significant indicating the presence of sources in a generally southerly direction. When winds were from the east-northeast a 90% level negative correlation was found. Negative correlations significant at the 90%, 95% and 90% levels were found with wind speeds in the 0-5, 5-10 and 10-15 km/hr classes, respectively.

THU-S-R1

A significant pattern of correlation coefficients can be seen on the histogram for this station. The correlation coefficients from the south-southwest direction through to the north-northeast are all positive and most are significant at the 90% level or greater. The opposite directions show almost all negative correlation coefficients. This suggests that medium range sources exist in a generally southerly-to-easterly direction. The largest correlation coefficient was 0.5284 (sig. level 90%), with winds from the east-northeast. Local sources are suggested by the 95% significant 0-5 km/hr wind speed class correlation.

THU-S-U1

The same general trends found at THU-S-R1 were found at this station as well.

TOR-S-S1, TOR-S-U1

Both stations exhibited the same pattern - generally positive correlations with winds from the west and north and negative correlation with winds from the east and south. This suggests medium range sources to the north and west. TOR-S-U1 showed a 99% significance level correlation in the 0-5 km/hr class and a 90% significant negative correlation with winds in the 10-15 km/hr wind speed class. This indicates trapping of PCB's in the city envelope during periods of low winds. A plot of TOR-S-S1 data for winds from the north is give in Appendix 5.

WIN-S-U1

A pattern of positive correlations with winds generally from the west suggests PCB's are being transported from the Detroit vicinity into Canada. The largest correlation coefficient was for winds from the west, and had a 99% significance. The 0-5 km/hr wind speed class showed a 99% significant correlation. This implies trapping of PCB's in an urban air mass over Detroit and Windsor during periods of low winds. A plot of the wind speed data is given in Appendix 5.

5.0 CONCLUSIONS AND RECOMMENDATIONS

5.1 Conclusions

Statistically significant correlations of PCB concentrations with wind direction were found for twenty-two of the twenty-five PCB sampling stations. A total of 65 significant wind direction correlations were found out of 400 wind direction correlations tested. However, no provincial or regional trends with specific wind directions were found.

Of the correlations between wind speed class and PCB concentration, 34 were found to be statistically significant out of 125 performed.

Some of the correlation data for wind speed and direction suggested the presence of local sources of PCB's in the vicinity of many of the sampling stations. Other wind direction and speed correlations appear to indicate medium range transport of PCB's. No comment can be made about long range PCB transport on the basis of the correlations performed and discussed in this report.

5.2 Recommendations

As discussed in Section 4.0, some of the significant correlations are based on limited data. As a second survey was undertaken in June 1980 it is recommended that when this data is available, it should be combined with the data in this report to form a larger data base to confirm the correlations already established.

It is also recommended that the meteorological data be examined for internal correlations by means of multiple regression techniques. In addition, correlations between PCB concentration and wind vector (made up of direction and speed) should be performed.

Evaluation of large air mass movements should be undertaken to assess the potential for long range transport of PCB's.

APPENDIX 1

PCB DATA

PCB STATION: BUR-S-U1

1	5.2	
2	10	
3	16	
4	12	
5	-	
6	1.0	
7	2.6	
8	_	
9	5.7	
10	2.9	
11	5.4	
12	23	
13	6.4	
14	1.5	
15	5.0	
16	i -	
17	4.7	
18	4.6	
19	5.4	
20	1.2	
21	3.2	
22	2.0	
23	2.1	
24	2.3	
25	2.5	
26	7.1	
27	2.4	
28	3.2	

PCB STATION: HAM-S-I1

DAY	PCB	CONCENTRATION	(ng/m**3)
1		16	
2		15	
3		15	
4		7.4	
5		12	
6		1.8	
7		5.8	
8		5.0	
9		11	
10		13	
11		5.3	
12		6.3	
13		9.4	
14		3.1	
15		22	
16		6.3	
17		3.1	
18		5.0	
19			
20		1.1	
21		1.8	
22		Section Section 1	
23		1.8	
24		2.6	
25		1.8	
26		2.3	
27		3.9	
28		2.7	

PCB STATION: HAM-S-I2

DAY	PCB	CONCENTRATION	(ng/m**3)
1		-	
2		13	
3		17	
4		18	
5		i=:	
6		5.0	
7		3.0	
8		9.0	
9		4.7	
10		8.2	
11		5.0	
12		11	
13		4.2	
14		4.7	
15		4.6	
16		4.2	
17		1.0	
18		4.6	
19		•	
20		3.7	
21		3.0	
22		2.7	
23		9.4	
24		2.0	
25		2.1	
26		3.4	
27		1.4	
28		2.6	

PCB STATION: HAM-S-U1

1	9.5
2	16
3	22
4	12
5	s = .
6	1.7
7	2.4
8	8.8
9	2.9
10	6.2
11	7.6
12	9.4
13	2-2
14	3.7
15	-
16	4.0
17	1.0
18	3.2
19	1.6
20	2.1
21	4.0
22	8.8
23	5.6
24	1.3
25	2.6
26	2.5
27	1.7
28	3.1

PCB STATION: HAM-S-U2

	10	
2	13	
3	1	
4	9	
5		
6	3.8	
7	3.6	
8	8.2	
9	18	
10	5.6	
11	4.4	
12	11	
13	5.0	
14	7.7	
15	9.5	
16	4.2	
17	5.7	
18	4.4	
19	4.1	
20	1.2	
21	14	
22	11	
23	1.9	
24	74	
25	1.2	
26	3.5	
27	.=	
28	2.7	

PCB STATION: KIN-S-U1

DAY	PCB	CONCENTRATION	(ng/m**3)	

1	5.6
2	10
3	9.5
4	10
5	•
6	1.1
7	1.9
8	:=
9	4.7
10	6.0
11	8.4
12	6.5
13	6.3
14	1.6
15	8.2
16	2.1
17	0.4
18	-
19	5.7
20	-
21	2.4
22	1.9
23	4.3
24	2.4
25	1.2
26	3.8
27	5.2
28	4.3

PCB STATION: LON-S-U1

DAY	PCB	CONCENTRATION	(ng/m**3)
1		:-:	
2		(-)	
3		(_)	
4		í = x	
5		: - -:	
6		2 — 2	
7		13	
8		(=)	
9		3 3	
10		14	
11		5.9	
12			
13		3.5	
14		3.8	
15		11	
16		4.7	
17		6.4	
18		7.7	
19		18	
20		13	
21		9.3	
22		P= 1	
23		11	
24		6.6	
25		11	
26		3.8	
27		1.5	
28		0.4	

PCB STATION: MIS-S-U1

1		11
2		14
3		15
4		8.7
5		-
6		2.1
7		5.8
8		4.1
9		3.0
10		7.2
11		4.0
12		6.7
13		10.2
14		2.3
15		-
16		-
17		5.1
18		3.5
19		•
20		1.9
21		6.0
22		1.6
23		1.6
24	(90)	0.9
25		4.3
26		3.0
27		3.4
28		2.1

PCB STATION: MIS-S-U2

1	15
2	11
3	10
4	5.3
5	-
6	1.1
7	3.4
8	7.0
9	3.5
10	10
11	6.9
12	5.5
13	10
14	0.8
15	
16	7.3
17	1.4
18	3.2
19	4.5
20	
21	1.8
22	0.8
23	1.7
24	2.8
25	1.4
26	2.0
27	4.4
28	1.3

PCB STATION: MIS-S-U3

1	11
2	11
3	18
4	11
5	15
6	5.6
7	2.7
8	9.0
9	2.7
10	21
11	5.8
12	8.7
13	9.9
14	3.2
15	
16	:
17	2.3
18	3.0
19	-
20	2.2
21	2.5
22	0.6
23	1.6
24	0.8
25	2.7
26	2.1
27	2.2
28	1.6

PCB STATION: MIS-S-U4

1	12
2	7.2
3	9.4
4	3.1
5	-
6	0.9
7	5.0
8	5.3
9	2.6
10	.11
11	7.7
12	15
13	8.9
14	3.5
15	5.5
16	5.0
17	4.0
18	4.5
19	2.3
20	9.0
21	4.7
22	1.3
23	1.6
24	3.3
25	3.4
26	3.3
27	3.7
28	1.4

PCB STATION: MOR-S-U1

DAY	PCB	CONCENTRATION	(ng/	/m**3)	ĺ
-----	-----	---------------	------	--------	---

1	16	
2	6.8	
3	2.6	
4	3.9	
5	12	
6	6.0	
7	1.0	
8	1.8	
9	4.8	
10	5.2	
11	6.4	
12	8.6	
13	7.3	
14	0.6	
15	-	
16	6.4	
17	8.6	
18	6.8	
19	1.8	
20	2.2	
21	1.8	
22	3.2	
23	, -	
24	3.0	
25	~	
26	2.3	
27	1.8	
28	3.9	

PCB STATION: NAN-S-R1

1	7.5
2	9.3
3	11
4	-1
5	14
6	9.5
7	4.3
8	12
9	9.6
10	7.8
11	3.0
12	5.0
13	7.7
14	1.0
15	3.4
16	4.8
17	2.0
18	4.9
19	1.6
20	1.6
21	2.2
22	1.1
23	1.5
24	2.4
25	3.3
26	3.2
27	3.6
28	2.5

PCB STATION: NAN-S-R2

1	14
2	9.2
3	12
4	9.4
5	18
6	1.8
7	1.3
8	4.9
9	2.3
10	7.1
11	4.4
12	7.9
13	4.7
14	1.1
15	2.5
16	7.8
17	2.6
18	5.4
19	景
20	2.5
21	2.1
22	3.9
23	2.1
24	3.8
25	2.3
26	1.8
27	0.9
28	2.4

PCB STATION: OSH-S-U1

1	6.6	
2	14	
3	12	
4	10	
5	-	
6	1.2	
7	4.1	
8	7.1	
9	14	
10	12	
11	7.3	
12	10	
13	12	
14	1.2	
15	- 1000 MES	
16	3.5	
17	1.0	
18	2.2	
19	4.8	
20	1.2	
21	2.2	
22	1.7	
23	3.5	
24	1.0	
25	6.3	
26	3.5	
27	2.6	
28	2.0	

PCB STATION: SAR-S-I1

1	20	
2	-	
3	21	
4	7.8	
5	17	
6	10	
7	3.7	
8	10	
9	6.6	
10	6.5	
11	3.8	
12	11	
13	9.8	
14	0.6	
15	3.5	
16	8.3	
17	4.4	
18	2.0	
19	2.6	
20	-	
21	2.2	
22	4.9	
23	3.0	
24	=	
25	6.5	
26	8.3	
27	1.1	
28	P <u>a</u> y	

PCB STATION: SAR-S-U1

DAY	PCB	CONCENTRATION	(na/m**3)
A-0-2011 A-1-20			(11.37) (11)

1	-	
2	17	
3	47	
4	! -	
5	9 - 5	
6	7.4	
7	5.0	
8	10	
9	6.2	
10	8.6	
11	5.7	
12	26	
13	13	
14	5.2	
15	=	
16	9.0	
17	4.1	
18	12	
19	7.8	
20	5.0	
21	1.8	
22	4.6	
23	8.0	
24	9.0	
25	3.8	
26	4.4	
27	9.3	
28	6.2	

PCB STATION: STC-S-R1

DAY PCB CONCENTRATION (ng/m*	**3	ng/m	ON (TRATI	CONCE	PCB	DAY
------------------------------	-----	------	------	-------	-------	-----	-----

1	19	
2	8.3	
3	23	
4	10	
5	16	
6	2.2	
7	2.1	
8	-	
9	5.7	
10	12	
11	4.7	
12	6.4	
13	6.9	
14	5.9	
15	8.0	
16	4.4	
17	1.9	
18		
19	2.0	
20	3.2	
21	11	
22	1.6	
23	3.2	
24	1.8	
25	2.6	
26	2.9	
27	2.4	
28	4.3	

PCB STATION: SUD-S-S1

1	4.3
2	12
3	9.2
4	5.0
5	<u>-</u> 6
6	4.2
7	1.1
8	6.7
9	-
10	8.1
11	6.3
12	5.2
13	9.4
14	3.7
15	-
16	
17	2.2
18	5.0
19	2.3
20	2.4
21	2.6
22	1.0
23	1.4
24	2.1
25	1.5
26	3.2
27	2.3
28	3.9

PCB STATION: SUD-S-R1

1	15
2	12
3	9.6
4	3.9
5	7.7
6	4.2
7	2.9
8	6.2
9	-
10	5.6
11	11
12	5.9
13	10
14	3.0
15	3.5
16	1.8
17	-
18	2.6
19	1.9
20	2.3
21	6.4
22	1.7
23	8.7
24	16
25	10
26	3.0
27	3.0
28	17

PCB STATION: THU-S-R1

1	8.8
2	9.3
3	7.1
4	2.0
5	-
6	3.5
7	0.7
8	-
9	3.3
10	4.3
11	4.8
12	10
13	4.7
14	2.5
15	2.5
16	2.4
17	5.8
18	4
19	2.5
20	2.2
21	2.5
22	3.6
23	1.3
24	0.8
25	1.0
26	1.9
27	2.4
28	3.2

PCB STATION: THU-S-U1

DAY	PCB	CONCENTRATION	(ng/m**3)
-----	-----	---------------	-----------

1	13
2	7.7
3	14
4	12
5	9.9
6	5.0
7	1.6
8	13
9	11
10	3.9
11	5.7
12	6.8
13	7.9
14	3.7
15	₩
16	1.7
17	11
18	6.8
19	1.7
20	1.7
21	1.5
22	1.3
23	2.2
24	2.7
25	2.6
26	1.3
27	1.5
28	4.3

PCB STATION: TOR-S-S1

DAY	PCB	CONCENTRATION	(na/m**3)
D/ 11	1 00	CONCENTION	(114/111 37

1	11
2	10
3	=
4	15
5	-
6	2.2
7	3.8
8	5.8
9	4.6
10	8.2
11	4.0
12	6.3
13	7.3
14	2.9
15	=
16	:=:
17	3.1
18	3.5
19	; -
20	1.9
21	5.1
22	4.6
23	2.6
24	3.5
25	5.0
26	4.5
27	4.4
28	1.6

PCB STATION: TOR-S-U1

DAY	PCB	CONCEN	TRATION	(ng/	(m**3)	

1	14	
2	33	
3	11	
4	11	
5	25	
6	5.9	
7	17	
8	15	
9	16	
10	7.9	
11	3.0	
12	5.9	
13	11	
14	5.2	
15	7.8	
16	=	
17	-	
18	5.6	
19	020 030	
20	2.3	
21	14	
22	3.4	
23	4.5	
24	1.9	
25	6.3	
26	6.0	
27	3.9	
28	5.2	

PCB STATION: WIN-S-U1

DAY PCB CONCENTRATION	(nq/m**3)	
-----------------------	-----------	--

1	6.6
2	11
3	13
4	10
5	16
6	4.8
7	2.2
8	5.9
9	9.5
10	6.1
11	8.5
12	5.2
13	6.0
14	5.6
15	6.8
16	2.9
17	3.2
18	4.5
19	2.8
20	2.7
21	4.3
22	2.0
23	€
24	2.2
25	1.5
26	1.5
27	3.3
28	3.4

APPENDIX 2

COMPUTER PROGRAM LISTING

THIS PRICEAM IS DESIGNED TO CORRELATE FOR COMMUNICATION WITH MIND DISCOTION, WIND SPEED, TEMPERATURE, OR STATEMENT DEVIATION OF TEMPERATURE.

1.0 FINT DATE

THE INPUT LATA COMBISTS OF 15 PCB CONCENTRATIONS, AND THE MET DATA FOR THE 28 DAYS FOR WHICH THERE ARE PCB DATA. THE MET DATA CONSISTS OF CEMPERATURE, WIND DIRECTION, AND WIND SPEED DATA DETAINED FROM MOE, ENERG, OR AES, AS APPROPRIATE.

2.0 SUBNOUTINES LIED

THE SUBROUTINES USED AND A BRIEF DESCIPTION OF THEIR USE IS SIVEN BELOW.

- A. DATA'EMTIR USED TO ENTER FOB OR MET DATA FROM TERMINAL
- P. CORRECT USED TO CORRECT OR CHANGE THE INPUT DATA
- C. ECHO PROVIDES FOR CUTPUT OF RAW DATA
- D. ANALYZE CONTROLS ANALYSIS OF DATA FOR CORRELATION CHARACTERISTICS
- E. STATE CALCULATES AVERAGE AND STD. DEV. OF DAILY TEMPS.
- F. DIRCLASS CLASSIFIES WIND DIRECTIONS INTO 14 POINTS OF COMPASS
- S. SPDCLASS CLASSIFIES WIND SPEED INTO 5 CLASSES
- H. CORRELATION CALCULATES CORRELATION COEFFICIENT AND SIGNIFICANCE
- I. DUTPUT OUTPUTS CALCULATED CORRELATION COEFFICIENTS AND ASSOCIATED STATISTICS
- J. GRAPH OUTPUTS HISTOGRAM PLOT OF CORRELATION COEFFICIENTS VS WIND DIRECTION CLASS
- K. CLOSE'FILE STORES CURRENT POB OR STATION DATA ON A DISK FILE
- L. RETRIEVE FETCHES PCB AND/OR STATION DATA FROM A DISK FILE

MAP1 WMI\$(15),8,15 MAP1 GRAPH†(31,80),8/1

FRINT TAB(-1,0)

DECISION1:

```
MAP1 PCSSTATE, S, SE
               MAP1 METETATA, E.SE
               MAP1 MENUA, 8, 109, "1. INTER DATAR 02. RETRIEVE DATAR 03. CORRECT&
DATAS 24. ECHO DATAS ST. ANALYZE DATAS 84. FIDILE® 97. END"
               MAF1 DELIM#, S, 1, "@"
               MAP1 NINETY4,3,5
               MAP1 MINETYFIVES, 5, 5
                MAP1 MINETYNINE*, 5,5
               MARI K#,S,SO
                DIM POPNAM$(2E),MFTNAM$(13),BIGNDIR$(16),BIGNSPD$(5)
                DIM TLINEWINDD(46), SWINDD(46), TLINEWINDS(5), SWINDS(5)
                DIM POB(28), STATION(29, 24, 3), AVTEMP(28), DEVTEMP(28), X(28)
                DIM Y(28), DIRCLAS(28,16), SPECLAS(28,5), WECOEFF(16)
                IIM WEDDEFF(E)
TATA N. N. N. W. N. W. W. N. W. W. W. S. W. S. W. S. S. W. S. S. S. E. S. E. E. E. E. E. E. N. E. N
DATA E, N. N. E
READ GRAPH$(32,1),GRAPH$(32,4),GRAPH$(32,5),GRAPH$(32,6),GRAPH$(32,9)
RIAD GRAFH$(32,10),GRAPH$(32,14),GRAPH$(32,15),GRAPH$(32,16),GRAPH$(32,20)
READ CRAPH¢(32,24),CRAPH¢(32,25),GRAPH¢(32,26),GRAPH¢(32,29),GRAPH¢(32,30)
READ GRAPH:(32,34),GRAPH:(32,35),GRAPH:(32,36),GRAPH:(32,45),GRAPH:(32,49)
READ GRAPH$(32,50), GRAPH$(32,51), GRAPH$(32,54), GRAPH$(32,55), GRAPH$(32,59)
READ GRAFH$(32,60),GRAPH$(32,61),GRAPH$(32,65),GRAPH$(32,69),GRAPH$(32,70)
READ GRAPH*(32,71), GRAPH*(32,74), GRAPH*(32,75), GRAPH*(32,78), GRAPH*(32,79)
READ GRAPH$ (32,80)
                DATA THU-S-U1, THU-S-R1, SUD-S-S1, SUD-S-R1, LON-S-U1
                ATA SAR-S-II, SAR-S-U1, MOR-3-U1, WIN-S-U1, HAM-S-I1
                DATA HAM-S-I2, HAM-S-U1, HAM-S-U2, STC-S-R1, NAN-S-R1
                DATA MAN-S-R2, FOR-S-U1, TOR-S-S1, OSH-S-U1, BUR-S-U1
                DATA MIS-S-U1, MIS-S-U2, MIS-S-U3, MIS-S-U4, KIN-S-U1
                DATA MCE-14016, MCE-12032, MCE-12034, AES- LOND, MCE-29026
                DATA MOE-27049, MOE-35033, MOE-33003, MOE-45025, AES- KING
                DATA MOE-77023, AES- TBAY, HYD- MANT
                      MASTER, DATA 'ENTER, CORRECT, ECHO, ANALYZE, STATS, DIRCLASS
                MATA
               DATA SPOCLASS, CORRELATION, OUTPUT, GRAPH, CLOSE'FILE, RETRIEVE
                FOR S=1 TO 25
                    READ POSMAKA(I)
                FOR I=1 TO 1S
                    READ METNAM¢(I)
                MEXT I
                TER I=1 TO 13
                    READ KMI$(I)
                MEXT I
                DECMUM=22
                CREN #1, "STATE. DAT", RANDOM, 15, RECNUM
                READ #1, MAXWEATHER
                CL03E #1
```

```
MOALL MENU, MENUG, DELIME, 6, 15
               PRINT TAP(4,15); "SELECT EPTION: ";
YOULL ASKIDT, "1284567", 21, 1
                FOINT TAD(-1,0)
               ON ERROR COTT ERRORI
               13/11=1
                ON O1 CALL DATA 'ENTER, RETROEVE, CORRECT, ECHO, ANALYZE, FIDDLE
                IF SIMP BOTO DECISION1
                FRINT TAB(-1.0)
               END
· 你我看到我们的我们的我们的我们就是我们的,你们们的人们的我们的人们的我们的,我们就是这些人的,我们就会会会会会会会会会会会会会会会会会会会会会会会会会会会会会
          SUDROUTINE DATA 'ENTER
<sup>17</sup>,只要我只要没有自己的。 你只要我看看这么多数,我也没有我的我看我我的我看我我的我看着我的,你就看到这种我的不会,你你看着我的我看着这一个。"
              INPUT "ENTER PGE (1) OR STATION (2) DATA, OR QUIT (3)", A1
DATA'ENTER:
               IF A1=3 RETURN
              WMI=2
              ON A1 GOTO FOR 'ENTR, STAT' ENTR
              GOTO DATA'ENTER
              INPUT "NUMBER OF NEW POP DATA FILE (1 - 16)? "" POENUM
    FOR SENTR:
               INPUT "STATION START TIME: ", START
               FOR I=1 TO MAXWEATHER-1
                   PRINT USING "ENTER FOD CONCENTRATION FOR DAY ###",I
                   INPUT PCS(I)
              MEXT I
               FLAGG=1
               DALL DLOSE'FILE
               GOTE DATA 'ENTER
    STATAENTR: INPUT "NUMBER OF NEW MET DATA FILE (1 - 13)? ", STATNUM
              INPUT "DAY TO START ENTERING TEMP DATA: ", STARTDAY
               IF STARTDAY>MAXWEATHER SOTO INWIND
               IF STARTDAY#1 FLAG2=8:A2=STATNUM:I=STARTDAY:CALL RETRIEVE
               FOR I=STARTDAY TO MAXWEATHER
                   FOR J=1 TO 24
                       PRINT USING "TAY ## - ", I;
                       PRINT USING "ENTER TEMPERATURE FOR HOUR ##: ", J-1;
                       INPUT " ", STATION(I, J, 1)
                       STATION(I, J, 1)=STATION(I, J, 1)/10.
                   NEXT J
                   PRINT CHR#(007)
              MEXT I
               FLAGG=2
               CALL CLOSE'FILE
              IF STARTDAY#1 INPUT "DAY TO START ENTERING SPEED DATA: ".STARTDAY
      INMIND:
               IF STARIDAY MAXWEATHER BOTO DIRIN
               IF STARTDAY#1 FLAG2=2:AG=STATNUH:CALL RETRIEVE
              FOR I=STARTDAY TO MAXWEATHER
                   FOR J=1 TO 24
                       PRINT USING "DAY ## - ", I,
                       PRINT USING "ENTER WIND SPEED FOR HOUR ##1 ", U-1;
                       INPUT " ",STATION(I,J,3)
                   MEXT J
                   PRINT CHR#(007)
              MEXT I
```

```
FLAGG=2
            CALL CLOSE'FILE
      DIRIN: IF STARTDAYES IMPUT "DAY TO START ENTERIND DIR DATAS ".STARTDAY
            IF STAR DAY>MAXWEATHER BOTE EKIRDIRU
            IF STARTDAYED FLACT - 2: A2=STATEUM: CALL RETRIEVE
            FOR J=1 TO 27
                   PRINT USING "DAY 5# - ". I;
PRINT USING "ENTER MIND DIRECTION FOR HOUR ##: ". U-1;
                   IMPUT "", STATION(I, J, C)
                MEXT J
                DRINT CHR#(007)
            MEXT I
SKIPDIRN:
            FLAGG=2
            CALL CLOSE'FILE
            GOTO DATA 'ENTER
SUBROUTINE CORRECT
MORRECT: INFUT "DO YOU WANT II MODIFY (1) THE DATA, OR QUIT (2) ",A
       IF A=2 RETURN
       WMI=3
        INPUT "DO YOU WANT TO LOAD DATA FROM DISK? ": A1$
        IF A1$[1,1]="Y" GOTO DISKDATA ELSE GOTO TYPE
 DIEKDATA:
          CALL RETRIEVE
            INPUT "MODIFY POD (1) OR STATION (2) DATA? "+ A1
  TYFE:
            INPUT "WHAT DAYS DATA DO YOU WANT TO MODIFY? ", DAY
 MODIFY:
            ON A1 GOTO POB'MOD, STAT'MOD
    POB'MOD: INPUT "ENTER NEW POB CONCENTRATION: ", POB(DAY)
            GOTO DATA'SAVE
    STAT'MOD: INPUT "MODIFY TEMP (1), DIRECTION (2), OR SPEED (3)? ", AS
            INFUT "TIME TO BE MODIFIED? ", TIMEDAY: TIMEDAY=TIMEDAY+1
            PRINT USING "CURRENT VALUE IS: ####. #", STATION(DAY, TIMIDAY, A3)
            INPUT "ENTER THE NEW DATA: ", STATION (DAY, TIMEDAY, AS)
            GCTG DATA'SAVE
   DATA'SAVE: IMPUT "BAVE THE DATA ON DISK? ", A2$
            IF A2$="Y" OR A2$="YES" CALL CLOSE'FILE
            GOTO CORRECT
【最高的《新兴的文学者的专家的专家的专家的《大学的的》(《大学的》)(《大学的》)(《大学的》)(《大学的))(《大学的专家的专家的专家的专家的专家的专家的专家
         SUBROUTINE ZONO
```

ECHO: INFUT "ECHO FOB (1) OR STATION (2) DATA, OR SUIT (3) ", A1 IF A1=3 RETURN

```
17 I = 4
             ON A1 30TO PCB'ENC. STAT'END
             SOTO ECHI
             IMPGT "PGD STATION NUMBER? (1 - 26): ", A2
    FOR'ENG:
             IF A2=POSMUM GOTO SIMOPOR
             FLA92::1
             DALL RETRIEVE
             PRINT CHR#(012)
    ECHOPORT
             FOR I=1 FO 9:PRINT " ":NEXT I
             PRINT TAB(85); "FOB DATA": PRINT " ": PRINT " "
             FRINT USING "
                               FOR STATION: \\#######\",FORMAM#(FORNUM)
             PRINT " ":PRINT " "
              TRINT TAD/101/"POB CONCENTRATION (na/ms/S)"
             FE3=「我的我。我#"
             FOR I=1 TO MAXWEATHER-1
                 PRINT USING " ###", I;
                 IF POB(I)#99 PRINT USING F8#, TAB(17):POB(I) ELSE PRINT &
                       TAS(20);"-"
             MEXT I
PRINT CHR$(012)
              TITI ESMO
    STAT'EKS: INPUT "MET STATION NUMBER? ", A2
             IF ALESTATNUM GOTO EKG'STAT
             FLAG2=2
             CALL RETRIEVE
    EKD'STAT: FOR I=1 TO MAXWEATHER
                 PRINT CHR$(012)
                 FOR I1=1 TO 5: FRINT " ": NEXT II
                 PRINT FAB(31); "MET STATION DATA"
                 FOR II=1 TO 4: PRINT " ": NEXT II
                FRINT USING " MET STATION: \########\", METNAM#(STATNUM)
                 FOR I1=1 TO 4:PRINT " ":NEXT I1
                 FRINT USING " DAY #50", I
                 FOR II=1 TO 4:PRINT " ":NEXT II
                 PRINT TAB(11); "TEMPERATURE" / TAB(24); "WINE SPEED"; &
                       TAB(37); "WIND DIRECTION"
                 FRINT TAB(18); "(DEG C)"; TAB(25); "(KM/HR)": TAB(37); &
                       "(DEG REL MORTH)"
                 FRINT "
                             HOUR"
                 FOR J=1 TO 24
                     FRINT USING "
                                      #ZOO
                                              ###.#
                                                            世春世。 林
                                                                          8
 dsd", J-1, STATION(1, J, 1), STATION(1, J, 2), STATION(1, J, 2)
             MEYT I
             FRINT CHR# (012)
              BOTE SCHO
SUITE STITIE
                          ANALYZE
【公司在中部内部的公司的企业的企业的企业。而且由于1、中国的企业工程的企业的企业的企业的企业和企业的企业的企业的企业的企业和企业的企业和企业的企业。
             WMI=5: N=114 XWEATHER-1
ANALYZE:
                 FLAG2-1
                  INPUT "FOR STATION TO AMALYZE: ", A2
```

```
(II)X,ib,il,"## ,### =(## , ##)SAUCCHS" EMISU TWIRR)
               FOR IT=I TO MAXUENTHELL
                            3 01 1=1F HOH
                                                       MIND VEREED:
                                  PLXEN DICO
                                    IP LXEN
                        FIDMETER (T. FELGMEIS
                        BADDS=(IP)GGNIMS
                    TLINEWINDD(J1)=TLINE
                      MODDELL(11)=VC.CELL
                        NOSERTEREDO TORO
               (II) X'IP'II'm ### =(## ' ##)SYTOHIC... OMISO 1912/2
                ()U.,11)?AUSRId=(11)X
                I-REHTAEWKARM OT I=II FOR
                              Al of 1=15 ApR
                                                        :MAIC'CVIW
                                   BOTO NEXT4
                           $SIBMELDISMEIS
                               SSIGTEMF=SLOPS
                          ENIBLE STREET STATEMENT OF STREET
                            SIGLCOELEHADOLGIS
                            NOITALERRO 1140
                                    II LXEN
                 (II) SMETUE: USING "DEVTEMP( 排作 # 4 14, 11, CEVTEMP(II)
                       X(II)=EZALEMB(II)
                    I-AEHTABWXAM OT [=1] FOR
                                                          BlBLE:S
                                   COLO NEXIG
                              $018=$aNELNOIS
                                  BEDTS=BWBLS
                              BMITL=ENSIBNITL
                               LCCEELE=WCGEELE
                            MOITALENGOS LLAS
                                      II LXEN
                   (II) SMING "ATEMP(44) = 444, 444, 441 (II) AVTEMP(II)
                       (II) ENEL/H=(II)X
                    I-RENTARIYAM OF I=11 ACR
                                                             LEWE
ON G SCIO LEWE, SIGTEMP, WIND'DIRW, WIND'SPEED
                                     t Ol Imp Mod
                                       STATE LIAD
                                          II TXEN
                          (DI) BOB 'TI' "## "### =(##) EDB( IT' BOB ( I C)
                               ([])=EEE(])A
                        FOR II=1 TO MAXMEATHER-1
                                    INTIBLEY ITSI
                                        こ ブール ごいくエニー
            EA." SECYLANA OT MOTTATE T
                                       15Ma 17 28.5
                                    SOLNUM- AS
POLNUM- ASTRIBUT
                       maie pastiffca, pecocos, to eninted on 9/10/80
```

TI LXEN

```
CALL CORRELATION

% SCHOOL TO LINE TO DEFF

TLINE (CINE CLIFT)

CONFORMATION

CONFORMA
```

HEXT JI

MEXIG.

WENT J

DALL OUTPUT PRINT CHEM (012) CALL DRAPH

RETURN

MEXT II

SUBROLTINE STATE

```
STATE:
             WHILE
             FOR I=1 TO MAXWEATHER-1
                 AVTEMP(I)=0
                 DEVIEWE(I)=0
                 CUMPEV=C
                 FOR 19=1 TC 14
                     DIRCLAS(I, IT) =C
                 FIR 17=1 TO 5
                     SFICLAS(I:IF:=0
                 NEXT IS
                 IF Y(I)=99 GOTO NXTI
                 FOR DIESTART TO 24
                     ANTEMP(I)=AVTEMP(I)+ STATION(I, I1.1)
                 MEXT II
                 FOR I1=1 TO START-1
                     AVTEMP(I)=AVTEMF(I:-STATION(I+1, I1, 1)
                 NIXT II
                 AVTEMP(I)=AVTEMP(I)/24.
IPRONT USING "AVTEMP(##)= ###.#", I.AVTEMP(I)
                 FOR II=START TO 24
                     SUMDEV=SUMDEV+(STATION(I, I1, 1)-AVTEMP(I))**2
                 MEXT I1
                  FOR II=1 TO START-1
                      OMDEV=SUMDEV-(STATION(I+1.J1.1)-AVTEMP(I))**2
                 NEXT II
                 DEVIEND(I)=SER(EU DE//24.)
                 FOR II=START TO 24
                     CALL DIRCLASS
                 MEXT I1
                  IAYFL J=!
                 TIR I1=1 TO STAFT-1
                     CALL DIRILASS
```

```
CAYFLG=0
                  FOR II=START TO DA
                      CALL EFFCLASS
                      I1
                  EAYFLC=1
                  TOR I1=1 TO START-1
                     CALL STEELASS
      MMTI:
              NEXT I
              FOR SHI TO MAXUEATHER-1
                  FOR J=1 TO 14
                   DIRCLAS(I, J)=(DIRCLAS(I, J)/24. 1*100
                  MEXT J
                  FOR J=1 TO 5
                     SPDCLAS(I, U)=(SPDCLAS(I, U)/24. ) *100
· 你是一个我们也要要要要要要要的,也是我们的,我们们的自己的,我们就会不会有什么。 "我们的,我们就会会会的,我们就会会会的,我们就会会会会会会会会会会会会会会
                  SUBROUTINE DIRCLASS
<sup>1</sup> "我我会我们也还会在这种的的是我的我们的我的我们的,我们就是我们的我们的我们的我们的,我们们们的我们的人们的是我们的人们的,我们们们们们的一个人们的人们的
DIRCLASS:
    WMI=7
    WIND-STATION(I+DAYFLG, I1, 2)
       WINDK = 11.25 OR WIND) 348.75 DIRCLAS(I,1)=DIRCLAS(I,1)+1:RETURN
    IF WIND> 11.25 AND WIND<= 33.75 DIRCLAS(I,2)=DIRCLAS(I,2)+1:RETURN
    IF WIND> 33.75 AND WIND<= 53.25 DIRCLAS(I,3)=DIRCLAS(I,3)+1:RETURN
    IF WIND> 56.25 AND WIND<= 76.75 DIRCLAS(I,4)=DIRCLAS(I,4)+1:RETURN
    IF WIND> 78.75 AND WIND(=101.25 DIRCLAS(I,5)=DIRCLAS(I,5)+1:RETURN
       WIND>101.25 AND WIND(=128.75 DIRCLAS(I,6)=DIRCLAS(I,6)+1:RETURN
                                   DIRCLAS(I,7)=DIRCLAS(I,7)+1:RETURN
       WIND>123.75
                  AND WIND<=146.25
                                   DIRCLAS(I,8)=DIRCLAS(I,8)+1:RETURN
       WIND>143.25 AND WIND<=168.75
    IF WIND>168.75 AND WIND<=191.25 DIRCLAS(I,7)=DIRCLAS(I,7)+1:RETURN
    IF WINDO191.25 AND WIND<=213.75 DIRCLAS(I,10)=DIRCLAS(I,10)+1:RETURN
    IF WIND>213.75 AND WIND(=236.25 DIRCLAS(I,11)=DIRCLAS(I,11)+1:RETURN
     IF WIND>286.25 AND WIND<=258.75 DIRCLAS(I,12)=DIRCLAS(I,12)+1:RETURN
    IF WIND>259.75 AND WIND<=281.25 DIRCLAS(I,13)=DIRCLAS(I,13)+1:RETURN
       WIND>281.25 AND WIND< =308.75 DIRCLAS(I, 14)=DIRCLAS(I, 14)+1:RETURN
    IF WIND>303.75 AND WIND<=326.25 DIRCLAS(I,15)=DIRCLAS(I,15)+1:RETURN
    DIRCLAS(I, 16) = DIRCLAS(I, 16) + 1: RETURN
SUBROUTINE SPECLASS
SPECLASS:
    WMI=8
    SPEED=STATION(I+DAYFLS, I1, 3)
       SPEEDK=5 SPECLAS(I.1)=SPECLAS(I.1)+1:RETURN
    IF SPEEDS5 AND SPEEDK=10 SPECLAS(I, 2)=SPECLAS(I, 2)+1:RETURN
```

IF SPEED>10 AND SPEED<=15 SPECLAS(I, 3)+SFECLAS(I, 3)+1:RETURN

```
or opeebble And speebk-20 specias(I,4)-specias(I,4) it.Return
    STEPLACIO, EXECTEDIASCO, EXPONENT
 SUBROUTINE CORRELATION
1"TT=9:N=MGX%TGTGTHER-1
CORRELATION:
            OUMX=0:SUMY=0:SUMXSQR=0:SUMYSQR=0:SUMXXX=0
            SKIPFED=0:5011/X2=0:5011/YC=0:VAR1=0:SDEV/FLOPE=0
              R Kai TO N
                OF MANY-OR SKIPPED-SKIPPED-1:SOTO MXTK
               CUMX=SUMX+X(M)
                CDYY=CLYY+Y(K)
               SUMMEDR-SUMMEDR+X(K)<*2
                CLNYSOR-SUNYSOR+Y(10) 442
               SUMMY+(X(K)*Y(M))
            IT SUMXSDR=0 SUMXSDR=.0001
 PRINT BURY, SURY, SUMYSOR, SUMYSOR, SUMYY
            SLOFE= (N*SUMXY-(SUMX-SUMY) 1/1N*CUMXSGR-(SUMX**2))
            PODERT= (SUMMY - ( (SUMM*SUMY), N) )/SQR( (SUMMSQR-(SUMM**2/N) )* 3.
                      (SUMYBOR- (SUMY* NO/N) 1)
 PRINT RODEFF, SLOFE
            TLINE=(ROSEFF*SGR(N-2))/SGR(1-ROSEFF**2)
 t VALUE LOOKED UP IN RANDOM FILE FROM DEGREES OF FREEDOM. DEGREES OF
 FREEDOM CALC. AS # DAYS-2 - # OF SKIPPED DAYS (-7 TO INDEX FILE)
!(NUMBER OF DAYS - NUMBER SKIPPED) CALCULATED AS N. ABOVE
            RECNUM-N-9
            OPEN #1, "DSKO:STATS. DAT", RANDOM, 14, RECNUM
            READ #1, MINETY$, MINETYFIVE; MINETYMINE$
            CLOSE #1
            MIMETY=VAL(MINETY*)
            NINETYFIVE=VAL(NINETYFIVE%)
            NIMETYNINE=VAL(NINETYNINE®)
!PRINT USING "90%: 希告. 往往年 , 95%: 恭恭. 告注并 , 99%: 告告. 并往往", NINETY, NINETYFIVE, &
ININETYNINE
            SIC5="
            IF APS(TLINE)>= NINETY AND ASSITLINE>KNINETYFIVE SIG4="POX":RETUR
            IF ASS(TLIME)>= NINETYFIVE AND ASS(TLINE) KNINETYNINE SIG$="95%":R
            IF ABS(TLINZ)>= NINETYNINE SIG#="99%"
            WMI=5: RETURN
SUPROUTINE DUTPUT
```

```
EMINI DRING ERP 1488(69): RMIND(10)
                                                                                                                                                                                                                                             MEXT I
                                                                                                                                              Y BRIND REMINDREDUED:
                                                                                                                                                                                                                SI O1 6=1 E02
                                                                                                                                                                                                          1. BUITS. INIUG
                                                                                                (91) BHEDOCMI(OZ) BHI 1, 中非特殊 184. SNICO INING
                                                                                                                                                                                                                                              I LXEN
                                                                                                                                         PRINT USING PICTUDESERVING
                                                                                                                                                                                                             5: C1 4=1 UC1
                                                                                                                                                                                                                                      n iniud
                                                                                                                                                                                                                                 n n 111751
  "ESE"; TAB(46); "E"; TAB(54); "ENE"; TAB(63); "NE"; TAB(72); "NNE"
                                       % :(98)d911,350;f(ZZ)j3914,358;f(81)2641;f(81)4(01)441 1NIV3
                                                                                                                                                                                                                                                 INIbai
                                                                                                                         (3)$MIGNSIS:(69)SWI '$bE SNISD ININE
                                                                                                                                                                                                                                              I LXEN
                                                                                                                                      FRINT USING FAA, SICKDIR$(I);
                                                                                                                                                                                                                    7 07 1=1 A07
                                                                                                                                                                                                          : DIS . LNINE
                                                                                                                (S)GGNIMERITL:(69)GFL:485 ENISA LNINC
                                                                                                                                                                                                                                              NEXT I
                                                                                                                              PRINT USING FEE, TLINEWINDD(I);
                                                                                                                                                                                                            Z O1 [ = I HO3
                                                                                                                                                                                                                     4
                                                                                                                                                                                                                                        " TWIRE
                                                                                                                                                                                                          źn.
                                                                                                                                 ($)CONING:(69)CVL'#85 DNISS INIUG
                                                                                                                                                                                                                                              I LXEN
                                                                                                                                              f(I) CONING '#EA ChiEn INTUA
                                                                                                                                                                                                                    Z CL I=I ECH
                                                                                                                                                                                                           1. BEOTS: INIBE
                                                                                                     (8) HEROCOM! (OZ) BYL + BYR # 188 . ENISC (NINC
                                                                                                                                          MINISSECONTAIN ENIET INING
                                                                                                                                                                                                                     7 07 1=1 RD3
                                                                                                                                                                                                                         , in INIUa
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                                                                                                                                                                                                                  林平谷も「せもかん=48三
                                                                                                                                                                                                                              u 林林林林 "林斯林u=季€出
                                                                                                                                                                                                                    n n LNISa
                           "WSS" : (SZ) EAT : "WS" : (E2) EAT : "USW" : (AZ) EAT : "W" : (AF) EAT
               % : MNM. : (98) Eg. : MNN. : (ZZ) EG. : MNN. : (SI) EG. : N. : (GI) EG. : N. : LEB. (ZZ) : MNN. : (SI) EG. : N. : LEB. (ZZ) EG. : LEB. (ZZ) 
                                                                                                                                             "NOTICERIC ENIN" (102) EAT TWIRR
               " " TNIST: "NOITOERIT CHING VE WIND DIRECTION": FRINT " "
                                                                                                                                                                                                                                                   LHITEL
                                                                                                    MA, FR ISAVE CITEM LC
                                                                                                                                                                                                                           INIES INIES
            (NEW ANDERSON AND THE PROPERTY OF THE PROPERTY
                                             (WINELS) #WANEDS, "VANSHIOSEV NODITATE BOS" DMISU TWIRP
                   " " TMIRE:" " TWIRE:"SIMEIDIFTEDD MOITA MERROD":(623)EAT TWIRE
                                                                                                                                                                                                           CTIDIESHO LNIES
                                                                                                                                                                                                                                              0.1=11.74
```

```
55747 " + N;
FIR 149 TO 15
    FRINT UZING FIRSTLINEWINDER(I)
MERT I
PRINT USING FSt. TAD(G7);TLIMENUNDE(14)
PRINT " SIG ";
TOT 1=5 TO 15
    TROM USING FAR, SIGNDIRA(I):
PRINT USING F4#, TAB(69); SIGNDIR$(16)
FOR I=1 TO SIFRINT " ":NEXT I
PRINT TAB(18): "POB CONCENTRATION VS WIND SPEED "
FEINT " "
PRINT TAB(21): "WIND SPEED (KM/HR)"
MRINT TAB(8); "0 - 5"; TAB(18); "5 - 10'; TAB(27); "10 - 15"; &
      TAB(37):"15 - 20";TAB(49);">20"
PELINT " "
F2$=" ##.####
PRINT " r ";
FOR I=1 TO 4
    PRINT USING F2+, WSCOSFF(I);
PRINT USING F2#, TAB(46); WEDGEFF(5)
PRINT "ELOPE ";
FOR I=1 TO 4
    FRINT USING F2$, SWINDS(I);
PRINT USING F5¢, TAB(46); SWINDB(5)
PRINT " c
FOR 1=1 TO 4
    PRINT USING F5$,TLIMEWINDS(I);
MEXT I
PRINT USING F5$, TAB(46); TLINEWINDS(5)
PRINT " SIG ";
FOR I=1 TO 4
    PRINT USING FA#, SICHSPD#(I);
NEMT I
PRINT USING F&+,TAB(46);SIGNSPD≢(5)
FOR I=1 TO S:FRINT " ":NEXT I
PRINT "POB CONCENTRATION VS AVERAGE TEMPERATURE:";
PRINT USING " r
                     ##.####",TAD(43);TCCEFF
PRINT USING "SLCPE
                    たお井、計劃的サ"、TAB(43); STEMP
PRINT USING " t #####", TA3(43); FLINETEMP
PRINT USING " SIG N#N ", TAD(43); SIGNTEMP#
FOR I=1 TO SIFRINT " ": NEXT I
PRINT "POB CONCENTRATION VS STD DEV TEMPERATURE:";
PRINT USING " r
                     お井。俳朴井井", TAB(43); SIGTCOEFF
PRINT USING "SLOPE ###.####", TAD(43); SBIGTEMP
PRINT USING " t
                    着きは、着きも非", TAB(43); TLINESIGTEMP
PRINT USING " SIG
                       N#N ", TAB(43); SIGNSIGTEMP#
RETURN
```

```
【你我有声言:"我是我有人的事情,我们就是我们的人们的,我们就是我们的人们的,我们就会会会说,我们就会会会,我们都会会会,我们就会会会会会会会会会会会会会会会会
              ELANGT=" ": LYMI=11
GRAFH:
              STARTHUM
              MINDS=":NTE DNIW"
              POD$="!NTS BOP "
              START#="START TIME"
               VALIDARIUALID DAYS"
              FOR I=1 TO 61
                   IF I=32 GOTO NXTIII
                    FOR J=1 TO 80
                         DRAFHA(I,J)=DLANKA
              NEXT I
   MXTIII:
                  I=1 TC CO
                    DRAPH#(01,I)=STAR®
              MEXT
              COUNTED. BO
              FOR I=1 TO 29 STEP 2
                    COUNT=COUNT-0.05
                    DRAFH#(I,SP)="+"
                    DRAPH≢(I,40)=STAR%
                    ORAPH#(I, 41)="0"
                    CRAPH*(I, 42)=". "
                     TRING$=COUNT USING "#.##"
                    GRAPH#(I,43)=STRING#[-2,-2]
                    GRAFH$(I, 14)=STRIMG$[-1, -1]
                    ]RAPH$(I+1,40)=3TAR#
              MEXT I
              GRAPH$(32,40)=STAR$
              COUNTED. 0
              FOR I=03 TO 60 STEP 2
                    COUNT=CCUNT-OLCS
                    ORAPH$(], 3?)="-"
                    SRAPH#(I,40)=STARW
                    ○RAPH#(I,41)="O"
                    GTAFH$(I, GI)="."
                   STRINGS-COUNT USING "#. ##"
                    ORAFH$(I,40) -STRING$[-2,-2]
                    CRAPH#(I,44)=STRING#I-0,-13
                    CRAPH&(I+1,40)=STAR¢
              GRAPH$(60,40)=STAR*
              GRAFRO(61,39)="-"
              CEAPH#(61,40)=STARM
              ORAFH: (61, 41)="0"
               연구4F년호(소1,42)=º."
              DRAFH$(61,43)="7"
              GRAPH#(61,44)="5"
              PRINT TAB(19); "CORRELATION COEFFICIENTS VS WIND DIRECTION"
              FOR I=9 TO 1 STEP -1
                    GRAPH#(1,I)=WIND#[-I,-I]
                    CRAPH*(2, I)=PCD*[-I,-I]
              MEXT I
              FOR 1=65 TO 74
                    CRAPH = (1, 1) = START = I(1-64), (1-64)
                    GRAPH#(2, I)=VALID#[(I-64), (I-64)]
```

```
MEXT I
             374FH+(1,75)=";"
384FH+(2,75)=";"
              70R I-1 TO 10
                 DRAPH# (D, J- 9) = FOINAM# (FOENLY) IJ: IJ
                 DRAFH# (1, I-9) = METNAM# (KEINUM) [1, I]
             NEXT
             STARTIS-START USING "NZ" - "08"
             VALIDIS=N USING "AZ"
             FOR J=1 TO 4
                 GRAPH#(1,I+76)=START1#[I,I]
                 GRAFH$(2, I+76)=VALID1$[I, I]
             OPHHST=INT(WDDOEFF(1)/0.025)
             IF ASS(SPHEST)>SC GPHEST=30*80N(GPHEST)
 DO FIRST DIRECTION A! DNE FOR SPACING REASONS
             INCR=SGN(GPHH37) >-1.
              IF GPHHGT=0 THEN GCTC SKIP1:
              IF GPHHGTKO GPHHGT=OFHHGT+1
             FOR J1=81 TO (S1+(ASS(GFHHGT)*INCR)) STEP
                                                         INCE
                   IF J1=32 THEN COTO NEXT1:
                  ORAFH¢(J1,1)=STAR$
             NEXT1: NEXT JI
                    CCUMT=0
       SKIP1:
                        COUNT=COUNT+5
                         IF COUNT=40 THEN COUNT=COUNT + E
                        SPHHST=INT(NDSCEFF(J)/0.025)
                         IF ABS(GPHHGT)>30 GPHHGT=30*8GN(GPHHGT)
                        INCR=SGN(GPHHGT)*-1
                        IF GPHHGT=0 THEN GO TO SKIP2:
                        IF GEHHOTKO GEHHOT=GEHHOT+1
                        FOR J1=31 TO (31+(ABS(GPHHGT)*INCR)) STEP
                             IF J1=32 THEN GOTO NEXT2:
                            GRAPH*(U1, COUNT)=STAR#
            MEXT2:
                        NEXT J1
            SKIP2: NEXT J
              FOR I=1 TO 61
                    FOR J=1 TO 79
                        PRINT USING "!", GRAPH#(I, J);
                   MEXT J
              FRINT USING "!", GRAFH#(I,80)
              MEXT I
              RETURN
!从我和心会会无法还要完全小学的的现在分词,我们的的一种的一种的一种的人,我们的一个人的一个人的,我们的一个人的,我们的一个人的,我们的一个人的人的,我们的一个人
                SUBROUTINE CLOSE'FILE
TLDSE'FILE: :MI=12
            ON AI GOTO FOB/OLS,STAT/CLS
  POB'CLS: IF FLASC=1 COTO DFN'FOB
            INPUT "POB FILE NUMBERS " PEBNUM
```

```
IDPN POR: PODETATOR DBK1: POB" + POBNUM+", DATE204, 13"
            LOCKUP POBSTATA, RESULT
            IF RESULT=0 AND 0182 FRINT CHR: $10071:1NPUT "MOUNT OTHER &
DATA DISK, OR TO CONTINUE...", DUMBY
            MCALL XNOUNTERDERISM
             PEN Gi, PESSTATO, OUTFUT
            TRINT #1,START
            FOR III=1 TO MAXWEATHER-1
                PRINT #1, III; FOD(III)
            FLAG5=0
            CLOSE #1:RETURN
   STAT/CLR: IF FLAGS=3 ENDWRITE=1 ELSE EMDWRITE=MAXWEATHER
IF FLAGS>=2 GOTO GFN/STAT
            INPUT "STATION FILE NUMBER? ", STATHUM
   OPN'STAT: METSTAT$="DSK1: MET"+STAFNUM+". DATE204, 13"
            LOCKUP METSTAT#, RESULT
            IF RESULT=0 AND Q102 PRINT CRR#(007):INPUT "MOUNT DTHER DATA &
DISK, OR TO CONTINUE...", DUMMY
            XOALL XMOUNT, "DBE1:"
            OPEN #1, METSTATS, CUTPUT
            FOR III=1 TO ENDURITE
               PRINT #1, III
               FCR JUJ=1 TO 24
                   PRINT #1, JUL, STATION(III, JUL, 1), STATION(III, JUL, 2), &
                         STATION([II, JUJ.3)
            MEXT III
            FLAGGEO
            CLOSE #1:RETURN
SUBROUTINE RETRIEVE
KMI=13
RETRIEVE:
            IF FLAG2=1 A1=1:PCBNUM=A2:COTO OFN1FCD
            IF FLAS2)=2 A1=2:STAINUM=A2:GOTO OPM2STAT
  RETRIEVE1: IMPUT "RETRIEVE POD (1) OR STATION (2) DATA, OR QUIT (3)? ", B1
            IF B1=3 RETURN ELSE A1=B1
            ON A1 GOTO POB'OFIG STAT'OPN
            GOTO RETRIEVE1
   PC3/SPK: INPUT "PCB FILE NUMBER? ", PCBNUM
   OPN1PCB: PCBSTAT$="DSK1:PCB"+PCBNUM+".DATC204,13"
            LODMUR POBSTATS, RESULT
            IF RESULT=0 AND G1#2 PRINT CHR$(007):INPUT "MOUNT OTHER DATA &
DISK, OR TO CONTINUE...", DUMMY
            XCALL XMOUNT, FDSK1:"
            OPEN #1, FOBSTAT# INFUT
            INPUT #1, START
            FOR III=1 TO MAXWESTHER-1
                INPUT #1, DUMMY, FCB(III)
```

```
CLOSE #1
           IF FLAGRED FLAGRACICETURM
           COTO RETRIEVES
   STATYOFW: IMPUT "STATION FILE NUMBER? ". STATNUM
   THISTAT: IF FLAG2=3 ENDWRITE=STARTDAY-1 ELSE ENDWRITE=MAXWEATHER
             TET: T#=" DEV1: MET"-STATMUM"". DATI204: 1j"
           LCOKUP METSTATA ASSULT
           IF FESULT#3 AND 01#2 PRINT CHR*(007):INPUT "MOUNT OTHER DATA &
DISK, OR TO CONTINUE...", DUMMY
          XCALL XMOUNT, "DESIL"
           CPEN #1, METSTAT$, INPUT
           FOR IDI=1 TO EMENSITE
              INFUT #1, DUM:TY
              FOR JUJ-1 TO 24
                  INPUT 84.DUMMY.STATION(III.JUL.1).STATION(III.JUL.2) &
    ,STATION(III.JUL.3)
              MEXT JUU
          MEXT III
           CLOSE #1
           IF FLAG2#0 FLAG2=0:DETURN
           GOTO RETRIEVE1
ERROR TRAPFING ROUTINE - CONTROL TO HERE DN ERROR, THEN GOES TO START
FRINT CHES(CO7)
ERROR1:
              PRINT USING "ERROR CODE ### ": ERR(C)
             PRINT USING "ERROR COURRED IN SUIROUTINE N#################### 24
                   NMI $ (WMI);
             PRINT "MEMORY: "; MEM(0)
             PRINT USING "I= 新作的。 ひゃ サボラ・ (C= 井舟井 ", I, J, K
              FRINT USING "I1= ### , d1= ###",II,J1
              FRINT UBING "FLAGI= ##, FLAG2= #%, FLAGB= ##",FLAG1,FLAG2,FLAGB
              FRINT "SANDY: "; SANDY
             FRINT USING "FOR FILE NAME: \###############", FORSTAT#
             PRINT CHR$(007)
              INPUT "OR TO CONTINUE...", DUMMY
             RESUME DECISION1
FILDLE:
                      CALL RETRIEVE
                     FOR I=21 TG 18
FOR J=1 TO 26
                         STATION(I, J. 1) = STATION(I, J. 1)/10
                     MEXT J
                     PEXT I
                     CALL CLOSE'FILE
```

RETURN

APPENDIX 3

COMPUTER PROGRAM OUTPUT

(Sampling Stations Listed in Alphabetic Order)

CONTRATION COSFFICIENTS

PER INCIDE BUS-8-14

MET. STATION: MOE-20028

MUMILI OF VALUE DAYS: 25

TO SERVICE TO STREET STREET

	* * * * *	ZVIZI		ETERTICA WMM	3.5	WBW	<u>೦</u> %	SCW
5L078 • 3.53		-0.3712 -0.0853 -1.7173 90%	-0.1387 -0.1080 -0.4829	0.4524 0.3622 2.2997 95%	0.3127 0.5763 6.8164 77%	0.7152	-0.0171 -0.0280 -0.0818	-0.040E
•	Ē	99E	35	ESE	Ε	EME	성표	NNÉL
SLOFE t 318		-0.2513 -0.0353 -1.2452	-0.0459		0.2071 0.0479 1.0153	0. (711	-0.0191 -0.0093 -0.0347	-0.04E1

POB CONCENTRATION VS WIND SPEED

	0 - 5	1000 Table	10 - 15	E0074 (E020)	>20
j -	0.2825	0.0594	0.0241	-0.0874	-0.2678
SLOPE	0.0626	0.0149	0.0116	-0.0305	-0.0546
Ť	1.4122	C. 2845	0.1156	-0.4209	-1.3032
SIC					

TEB CONCENTRATION	V3	AVEF	(AGE	TEMPERATURE:	r SLOPE t SIG	0.0515 0.0523 0.2475
FCB CONCENTRATION	VS.	STD	DEV	TEMPERATURE:	r SLOPE t sia	-0.0711 -0.3663 -0.3417

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			20	*			*							
			35	*			->0.50							
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#*** N NN *	W NW * *	***	* * * *	***		SSW	* S -*0.05 *	93 E * *	SE *					
#*** N NN * *	W NW * *	***	* * * *	***		SSW	* S -*0.05 * -~0.10	9 95 * * *	5E * * *					
XXXXX N NNI X X X	W NW # * * *	***	* * * *	***		SSW	* S -*0.05 * -~0.10	99 E * * *	SE * * * *					
N NNI *	W NW * * *	***	* * * *	***		SSW	* S -*0.05 * -*0.10 * -*0.15	99 E * * * *	5E * * *					
₩×××× N MNI * * * *	WN W * * * *	***	* * * *	***		SSW	* S -*0.05 * -*0.10 * -*0.15	99 9 * * * * *	SE * * * *					
AXXXX N NNI X X X X X X	W NW # * * *	***	* * * *	***		SSW	* S -*0.05 * -*0.10 * -*0.15 *	SSE * * * * * * *	SE * * * *					
**************************************	W NW	***	* * * *	***		SSW	* S -*0.05 * -*0.10 * -*0.15 * -*6.20	SS * * * * * * * * * * * * * * * * * *	SE * * * *					
**************************************	W NW * * *	***	* * * *	***		SSW	* S -*0.05 * -*0.10 * -*0.15 * -*0.20 *	SSE * * * * * * *	SE * * * *					
#*** N NNI * * * * *	W NW * * *	***	* * * *	***		SSW	* S -*0.05 * -*0.10 * -*0.15 * -*6.20 * -*0.25 *	SS * * * * * * * * * * * * * * * * * *	SE * * * *					
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#**** N NNI * * * * * * * * *	W NW * * *	***	* * * *	***		SSW	* S -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 *	SS * * * * * * * * * * * * * * * * * *	SE * * * *					
**************************************	W NW * * *	***	* * * *	***		SSW	* S -*0.05 * -*0.10 * -*0.15 * -*6.20 * -*0.25 * -*0.30 *	SS * * * * * * * * * * * * * * * * * *	SE * * * *					
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**************************************	W NW * * *	***	* * * *	***		SSW	* S -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.40 * -*0.40 * -*0.45	SS * * * * * * * * * * * * * * * * * *	SE * * * *					
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**************************************	W NW * * *	***	* * * *	***		SSW	* S -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.40 * -*0.45 * -*0.45 * -*0.50	SS * * * * * * * * * * * * * * * * * *	SE * * * *					
**************************************	W NW * * *	***	* * * *	***		SSW	* S -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.40 * -*0.45 * -*0.50 * -*0.50	SS * * * * * * * * * * * * * * * * * *	SE * * * *					
**************************************	W NW * * *	***	* * * *	***		SSW	* S -*0.05 * -*0.10 * -*0.15 * -*0.25 * -*0.30 * -*0.35 * -*0.40 * -*0.45 * -*0.50 * -*0.50	SS * * * * * * * * * * * * * * * * * *	(C) ************************************					
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-*0.75

CONNEL ATION COEFFICIENTS

FIR STAFION: NAM-S-II

MET. STATION: MGE-29026

NUMBER OF WALLS SAYS: 24

FOR DESCRIPTION OF SEER CARECTACH

			::I:::	CIRCIFIAN				
	. 14		4.37. 3		35 M (63%)	WEW.	(= 1 + 1 + 1 + 1 + 1 + 1 + 1 + 1 + 1 + 1	55.7
SLOPE t sid	0.1715	-0.0273	-6.0482 -0.0553 -3.1385	0.1148	0.1275 0.1769 0.7453	0,0755 0,0897 1,3955		:.0727 0.0420 0.0579
•	Ξ	ESE	35	ESE	Ξ	ENE	NE	NIVEE
SLOFE SİS		-0.1929 -0.0710 -0.9632	-0.0764 -0.0264 -0.4447	O. 0723		-0.1338 -0.0821 -0.6868		

POE CONCENTRATION VS WINE SPEED

		WIAE	EFEEL (KM.	(HR)	
	0 · 5	5 - 10	10 - 15	15 - 20	220
r	0.3116	0.1337	c. 2997	-0.2075	-0. 4517
SLOPE	0.0759	0.0461	0.1557	-O.OEOO	-0.110E
t	1.6066	0.8283	1.5390	-1.0392	-2.5499
5 I G					95%

PCE	CONCENTRATION	VΘ	AVERAGE	TEMPERATURE:	ŕ	0.0462
201						0.0712
					t	0.3248
					SIC	

= C.E.	CONSENTRATION	VΞ	STI	SEV	TEMPERATURE:	r	C. 0593
						SLOFE	0.3619
	8					Ī	0.2913
						953	

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CORRELATION COEFFICIENTS

FIR STATION: MARKS-12

MET. STATION: MOE-25024

TOS CONCENTRACION VS WIND DIRECTION

	M	MNA	NN KIND	DIRECTION	74	. 2 W	SW	# 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
SLOFS T	0.7521 0.3361 5.1535 29%	-0.0010 -0.0000 -0.0047	0.1681 0.1478 0.8179	0. 5098 0. 4594 2. 8384 27%	0.5299 0.4981 2.9065 PRX	0.1426 0.1107 0.6907	-0.0820 -0.0981 -0.3948	-0.1415 -0.1925 -0.7848
	S	ESE	ΞE	ESE	E	ENE	N E	NNEI
3107E T 813	0.0723 0.0228 0.3499	-0.1704 -0.0519 -0.8293	-0.3172 -0.0759 -1.6039	0.0062 0.0022 0.0295	-0.0012 -0.0764 -1.5147	-0.0321	0.1704 0.0855 0.9310	0.0726 0.0425 0.3490

FCB SCHOEMTRATION VS WIND SPEED

		MIND	BREED (MM)	~'-(구)	
	0 - 5	5 - 10	10 - 15	15 - 20	: 20
	0.6204	0.0764	-0.0818	-0.3373	-C. 3945
3L275		0.0189	-0.0321	-0.1245	-0.0770
t	3.7939	0.3676	-0.3935	-2.0301	-2.0591
* =	997			70%	90%

703	CONCENTRATION	VΞ	AVERAGE	TEMPERATURE:	ř	0.2656
					ELSPE	0.2337
						1.3212
					910	

703	CONCERTRATION	ΛΞ.	STD	DEV	TEMPERATURE:		0.1025 0.5093
			i i			t SIG	0.4941

*				7€
		COMMELATIO	N JOSFFICIENTS VS WIND DIRECTION	
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CONNER AN ION COEFFICIENTS

FOR CTASION: MAM-S-UI

MET. STATION: MOE-27026

CUMBER OF VALUE DAYE: 25

PCB CONCENTRATION VS WINE DIRECTION

	N	NNW	NW NW	DIRECTION WNW	L+ J	₩E! √	E₩	SSW
r SLOPE SIG	0.7217 0.3665 5.0143 99%	-0.1314 -0.0399 -0.6503	C. 1813 C. 1539 C. 7938	0.4599 0.3526 2.4941 95%	0.5436 0.4510 3.1062 79%	0.3327 0.3033 1.6917	0,1250 0,2716 0,6043	-0.0643 -0.0328 -0.3091
ψ _i	S	SSE	ŝΕ	SSE	Ξ	ENE	NE	MNET
r SLOPE	0.1052	-0.2781	-0.3450	-0.0412	-0.2122	-0.1047	0.1227	0.0470

POR CONDENTRATION VS WIND SPEED

	o - 5	WIND 5 - 10	SPEED (KM/	/HR) 15 - 20	>20
r ŞLOPE t SIG	0.6898 0.1517 4.5691 99%	-0.0453 -0.0132 -0.2174	-0.0038 -0.0017 -0.0181	-0.4231 -0.1478 -2.2375 75%	-0.3792 -0.0809 -1.9452 90%

FCB	CONCENTRATION	VS	AVER	RAGE	TEMPERATURE:	r SLOFE t SIG	0.2045 0.2040 1.0124
PCS	CONCENTRATION	VS	STD	ΓEV	TEMPERATURE:	r SLOPE t	0.0185 0.1057 0.0889

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				17-17-17	TO LET	TON	CHIFTT	CIENTO VE	:: 7 NT	7,75						Y A
						* ***		-40.7E	District Edition	3-10.40 V Stanto		100	TART	7 - 4	 •	05
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32								+÷0. <u>6</u> 0								
200																
47								÷<0.⊊								
P. 15				-2-				4								
144				**				-90 . 50								
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*				÷.												
4			-4	*				->C.45								
15			*	*				3.4								
			**	42				480,40								
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					*			-*5.Z0								
*			*	-35-												
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		*	÷	*	2-											
43-		*	24	*	*	-25		2.								
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*		*	*	*	*	13										8.0
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- TO THE RESERVE OF T																
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-24.	2000 PECUL	*	<u>s</u> .	*	*	*		* *			~~~~				*	. . .
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-24.	eese Milk	F & # 4 4							***** 385	65 85	**** ESE					*** NN
**		F & # 4 4		****	F ~ \$ # # #	\$86.		* 3	SSE					ŀΕ	***	
**	NAW	F & # 4 4		****	F ~ \$ # # #	\$86.	SSW	********* * 3 -*0.05	88 5 *	8E *		E	Et 3	!Ε	***	
**	MAN	F & # 4 4		****	F ~ \$ # # #	\$86.	SSW	********** * 3 -*0.05 *	33 5 * *	3E *		Ξ : *	E) ;	₹Ε •	***	
**	NAW	F & # 4 4		****	F ~ \$ # # #	\$86.	SSW	* 3 -*0.05 * -*0.10	88 5 *	8E *		E	E) *	!Ε	***	
**	MAN	F & # 4 4		****	F ~ \$ # # #	\$86.	SSW	********** * 3 -*0.05 *	33 5 * *	3E *		Ξ : *	E) *	₹Ε •	***	
**	MNU.	F & # 4 4		****	F ~ \$ # # #	\$86.	SSW	* 3 -*0.05 * -*0.10	38 5 * * *	3E * *		E * * *	E) 3	₹Ε •	***	
**	MNU.	F & # 4 4		****	F ~ \$ # # #	\$86.	SSW	* 3 -*0.05 * -*0.10 * -*0.15	565 * * * * *	3E * * * * *		E * * * *	E! * *	₹Ε •	***	
**	MNU.	F & # 4 4		****	F ~ \$ # # #	\$86.	SSW	********* * 3 -*0.05 * -*0.10 * -*0.15	555 * * * * * *	SE * * * * *		三 : * * * * * * * *	E) 3 4	₹Ε •	***	
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# #*	MNU.	F & # 4 4		****	F ~ \$ # # #	\$86.	SSW	********* * 3 -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25	535 * * * * * * *	S * * * * * * * * * * * * * * * * * * *		三 : * * * * * * * *	E) 3 4	₹Ε •	***	
# #*	MAN.	F & # 4 4		****	F ~ \$ # # #	\$86.	SSW	* S -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30	55 * * * * * * * * * *	EI * * * * * * * * * * * * * * * * * * *		三 : * * * * * * * *	E) 3 4	₹Ε •	***	
# #*	MAN.	F & # 4 4		****	F ~ \$ # # #	\$86.	SSW	* S -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30	55 * * * * * * * * * *	S * * * * * * * * * * * * * * * * * * *		三 : * * * * * * * *	E) 3 4	₹Ε •	***	
# #*	MAN.	F & # 4 4		****	F ~ \$ # # #	\$86.	SSW	********* * 3 -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30	55 * * * * * * * * * *	EI * * * * * * * * * * * * * * * * * * *		三 : * * * * * * * *	E) 3 4	₹Ε •	***	
**	MAN.	F & # 4 4		****	F ~ \$ # # #	\$86.	SSW	********* * S -*0.05 * -*0.10 * -*0.15 \$ -*0.20 * -*0.25 * -*0.30 * -*0.35	55 * * * * * * * * * *	E1 * * * * * * * * * * * * * * * * * * *		三 : * * * * * * * *	E) 3 4	₹Ε •	***	
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# #*	MAN.	F & # 4 4		****	F ~ \$ # # #	\$86.	SSW	********* * S -*0.05 * -*0.10 * -*0.15 \$ -*0.20 * -*0.25 * -*0.30 * -*0.35	55 * * * * * * * * * *	E1 * * * * * * * * * * * * * * * * * * *		三 : * * * * * * * *	E) 3 4	₹Ε •	***	
# #*	MAN.	F & # 4 4		****	F ~ \$ # # #	\$86.	SSW	******** * 3 -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.35 -*0.40	55 * * * * * * * * * *	E1 * * * * * * * * * * * * * * * * * * *		三 : * * * * * * * *	E) 3 4	₹Ε •	***	
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# #*	MAN.	F & # 4 4		****	F ~ \$ # # #	\$86.	SSW	********* * S -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.35 -*0.45 -*0.45	55 * * * * * * * * * *	E1 * * * * * * * * * * * * * * * * * * *		三 : * * * * * * * * * * * * * * * * * *	E) 3 4	₹Ε •	***	
# #*	MAN.	F & # 4 4		****	F ~ \$ # # #	\$86.	SSW	********* * 3 -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.35 * -*0.45	55 * * * * * * * * * *	E1 * * * * * * * * * * * * * * * * * * *		三 : * * * * * * * * * * * * * * * * * *	E) 3 4	₹Ε •	***	
# #*	MNU.	F & # 4 4		****	F ~ \$ # # #	\$86.	SSW	********* * S -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.40 -*0.45 -*0.45	55 * * * * * * * * * *	E1 * * * * * * * * * * * * * * * * * * *		三 : * * * * * * * * * * * * * * * * * *	E) 3 4	₹Ε •	***	
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# #*	MNU.	F & # 4 4		****	F ~ \$ # # #	\$86.	SSW	********* *	55 * * * * * * * * * *	E1 * * * * * * * * * * * * * * * * * * *		三 : * * * * * * * * * * * * * * * * * *	E) 3 4	₹Ε •	***	
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# #*	MNU.	F & # 4 4		****	F ~ \$ # # #	\$86.	SSW	********* * 3 -*0.05 * -*0.10 * -*0.15 * *0.20 * -*0.25 * -*0.30 * -*0.35 -*0.45 -*0.45 -*0.50	5 \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	E1 * * * * * * * * * * * * * * * * * * *		三 : * * * * * * * * * * * * * * * * * *	E) 3 4	₹Ε •	***	
# #*	MNU.	F & # 4 4		****	F ~ \$ # # #	\$86.	SSW	********* *	5 \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	E1 * * * * * * * * * * * * * * * * * * *		三 : * * * * * * * * * * * * * * * * * *	E) 3 4	₹Ε •	***	
# #*	MNU.	F & # 4 4		****	F ~ \$ # # #	\$86.	SSW	********* * S -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.40 -*0.45 -*0.50 -*0.50 * -*0.60	5 \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	E1 * * * * * * * * * * * * * * * * * * *		三 : * * * * * * * * * * * * * * * * * *	E) 3 4	₹Ε •	***	
# #*	MNU.	F & # 4 4		****	F ~ \$ # # #	\$86.	SSW	********* * S -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.40 -*0.45 -*0.50 -*0.55	5 \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	E1 * * * * * * * * * * * * * * * * * * *		三 : * * * * * * * * * * * * * * * * * *	E) 3 4	₹Ε •	***	
# #*	MNU.	F & # 4 4		****	F ~ \$ # # #	\$86.	SSW	********* * S -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.40 -*0.45 -*0.50 -*0.55	5 \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	E1 * * * * * * * * * * * * * * * * * * *		三 : * * * * * * * * * * * * * * * * * *	E) 3 4	₹Ε •	***	
** **	MNU.	F & # 4 4		****	F ~ \$ # # #	\$86.	SSW	********* * S -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.40 -*0.45 -*0.50 -*0.55	5 \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	E1 * * * * * * * * * * * * * * * * * * *		三 : * * * * * * * * * * * * * * * * * *	E) 3 4	₹Ε •	***	

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CORRECTION DESTRICIENTS

POB STATION: HAM-S-UI

MET. STATION: MDE-29026

MUMBER OF WALIE DAYS: 26

POD COMMENTRATION VS WIND DIFECTION

	N	5-16-11 J		DIFICTION WNW		4214	SW	SSN
SIC		-0.0631 -0.0450 -0.3123	-0.4119	-0.0139 -0.0300 -0.0382	-0.0129	-0.1437	-0.0977 -0.3606 -0.4811	-0.0617 -0.0988 -0.9029
	5	SSE	SE	ESE	Ξ	ENE	NE	NNE

POB CONCENTRATION VE WIND SPEED

		WIME	SPEED (KM/	(HR)	
	í - 5	5 - 10	10 - 15	15 - 20	>20
r	-0.0453	-0.2037	-c. 4222	-0.2502	0.5517
SLOPE	-0.0252	-0.1655	-0.5254	-C. 2548	0.3323
• •	-0.2220	-1.0352	-2.2819	-1.2661	3.2402
SIG			95 %		99%

FIE	CONCENTRATION	4,4	AVERAGE	TEMPERATURE:		0.3026
					ELCPE	O.8118
				*1	2	1. 5551

POB	CONCENTRATION	VΞ	STD	DEV	TEMPERAT	TURE:		
								-2.8560
							513	-0.9185

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N .	1.11	NW WINK		N. E.S.	SW	354	-*C.05 * ********* * S	*	* * *	ESE	E	ENE		##4 NN
				%2% ≉	5W *		-+0.05 # ******** * 8 -~0.05*	* * &< >< >& &	* * *	ESE *	E ∗	ENE *		
N .	1.11	NW WINK		N. E.S.	SW	354	-+0.05 * ******* *	* * &< >< >& &	* * *	ESE * *	E *	ENE *		
M ·	1.11	NW MNW * *		%2% ≉	5W *	354	-*0.05 * ******* * S0.05* * *	* * &< >< >& &	* * *	ESE * *	E * * *	ENE *		
M ·	1.11	NR ENK		%2% ≉	5W *	354	-*0.05 * ******* * S0.05* * * -*0.10* * *	* * &< >< >& &	* * *	ESE * * * *	E * * * *	ENE *		
M ·	1.11	NW MNW * *		%2% ≉	5W *	354	-*0.05 * ****** * 8 -*0.05* * * -*0.10* * * -*0.15	* * &< >< >& &	* * *	ESE * *	E * * * * *	ENE *		
M ·	1.11	NR ENK		%2% ≉	5W *	354	-*0.05 * * * * * * * * * * * * * * * * * * *	* * &< >< >& &	* * *	ESE * * * *	E * * * *	ENE *		
M ·	1.11	NR ENK		%2% ≉	5W *	354	-*0.05 * ******* *	* * &< >< >& &	* * *	ESE * * * *	E * * * * *	ENE *		
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M S	1.11	NR ENK		%2% ≉	5W *	354	-*0.05 * ******* *	* * &< >< >& &	* * *	ESE * * * *	E * * * * *	ENE *		
M ·	1.11	NR ENK		%2% ≉	5W *	354	-*0.05 * ***** *	* * &< >< >& &	* * *	ESE * * * *	E * * * * *	ENE *		
M ·	1.11	NR ENK		%2% ≉	5W *	354	-*0.05 * * * * * * * * * * * * * * * * * * *	* * &< >< >& &	* * *	ESE * * * *	E * * * * *	ENE *		
M ·	1.11	NR ENK		%2% ≉	5W *	354	-*0.05 * -*0.05* -*0.10* -*0.15 * -*0.20 * -*0.25 * -*0.30 *	* * &< >< >& &	* * *	ESE * * * *	E * * * * *	ENE *		
M ·	1.11	NR ENK		%2% ≉	5W *	354	-*0.05 * * * * * * * * * * * * * * * * * * *	* * &< >< >& &	* * *	ESE * * * *	E * * * * *	ENE *		
M ·	1.11	NR ENK		%2% ≉	5W *	354	-*0.05 ******** * S -~0.05* * * -*0.10* * * -*0.20 * -*0.25 * -*0.30 * -*0.35	* * &< >< >& &	* * *	ESE * * * *	E * * * * *	ENE *		
M ·	1.11	NR ENK		%2% ≉	5W *	354	-*0.05 * ****** * -*0.05* * -*0.10* * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.35 * -*0.40	* * &< >< >& &	* * *	ESE * * * *	E * * * * *	ENE *		
M ·	1.11	NR ENK		%2% ≉	5W *	354	-*0.05 * * * * * -*0.10* * * * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.35 * -*0.40 *	* * &< >< >& &	* * *	ESE * * * *	E * * * * *	ENE *		
M ·	1.11	NR ENK		%2% ≉	5W *	354	-*0.05 * * * * * * * * * * * * * * * * * * *	* * &< >< >& &	* * *	ESE * * * *	E * * * * *	ENE *		
M ·	1.11	NR ENK		%2% ≉	5W *	354	-*0.05 * * * * * * * * * * * * * * * * * * *	* * &< >< >& &	* * *	ESE * * * *	E * * * * *	ENE *		
M ·	1.11	NR ENK		%2% ≉	5W *	354	-*0.05 * * * * * * * * * * * * * * * * * * *	* * &< >< >& &	* * *	ESE * * * *	E * * * * *	ENE *		
M ·	1.11	NR ENK		%2% ≉	5W *	354	-*0.05 ******** *	* * &< >< >& &	* * *	ESE * * * *	E * * * * *	ENE *		
M ·	1.11	NR ENK		%2% ≉	5W *	354	-*0.05 ********* * S -~0.05* * * * -*0.10* * -*0.15 * -*0.20 * -*0.25 * -*0.35 -*0.35 -*0.45 -*0.55	* * &< >< >& &	* * *	ESE * * * *	E * * * * *	ENE *		
M ·	1.11	NR ENK		%2% ≉	5W *	354	-*0.05 ******* * 8 -*0.05* * * -*0.10* * * -*0.15 * -*0.20 * -*0.25 * -*0.35 * -*0.40 * -*0.45 * -*0.55 * -*0.55	* * &< >< >& &	* * *	ESE * * * *	E * * * * *	ENE *		
M ·	1.11	NR ENK		%2% ≉	5W *	354	-*0.05 ******* * 8 -*0.05* * * -*0.10* * * -*0.15 * -*0.20 * -*0.25 * -*0.35 * -*0.40 * -*0.45 -*0.55 -*0.55 -*0.60	* * &< >< >& &	* * *	ESE * * * *	E * * * * *	ENE *		
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M ·	1.11	NR ENK		%2% ≉	5W *	354	-*0.05 ******* *	* * &< >< >& &	* * *	ESE * * * *	E * * * * *	ENE *		

CLAMBUATION COEFFICIENTS

PGB STATEON: KIN-S-U1 MET. STATEON: RES- KIND

NUMBER OF VALID DAYS: 24

FOR DOWNENTRATION WE WIND DIRECTION

	N	\$ 15 mg	WINE IN	IIREITION UAN	λ	₩Ē.	SM	SSM
2L3PE * 233	0.2596 0.0963 1.2410	-0.1219 -0.0284 -0.5741	0.1512 0.0472 0.7174	-0.2005 -0.0654 -0.9597	0.1957 0.0578 0.8471	-C.0708 -0.0859 -0.3331	0.0359 0.0531 0.1483	0.1261 0.0384 0.5962
	S	SSE	SE	Ξ7 Ξ	Ξ	ENE	NE	ME
r DLOPE Sig	0.1135 0.0131 0.5359	0.0483 0.0195 0.2047	0.0778 0.0258 0.3659	-0.1389 -0.0384 -0.8577	-0.2572 -0.0474 -1.2485	0.1907 0.0349 0.9110	-0.2087 -0.0841 -1.0008	-0.2162 -0.0925 -1.0387

FC3 CONCENTRATION VS WIND SPEED

		HIND	SPEED (KM.	(HR)	
	୍ - ଅ	E - 10	10 - 15	15 - 20	>20
۳	0.3978	-0.0379	-C.3995	-0.2705	0.0970
QLIPE	0.0850	-0.0121	-0.0399	-0.1148	0.0099
14	2.0335	-0.3192	-2.0442	-1.3180	0.4571
813	90%		70%		

FOR	CONCENTRATION	VE	AVERAGE	TEMPERATURE:	•	C. O404
					SLOPE	0.0066
					-	(. Z839
					303	

FCE	CONCENTRACION	$V\Xi$	272	EEV	TEMPERATURE:	<i>*</i> -	-0.0734
						SLOPE	-0.2512
						t	-O.S491
						7.7.	

		vert.	- [-:2:]:3		ELAT	77.7	I-EFF	ICIENTS VS	WIND	CIREC	TION		TINE:	P 1
.	T 57	. KIN-	-5-U1					** 5. 7 0				VALID	DAYS:	24
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5.00														
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	NNW	-≠≈≠≠ NW	WNW		MEN			-\$&>> \$ \$\\	***** 335	****	EEE	ΞΞ	NE NE	1 NN
根据				***		***	****	*****		****				414
根据	NNW ∗		WNW * *	***	MEN	***	****	******** * E -*0.05 *		****	ESE * *	E	NE NE * *	1M :
根据	NNW *		WNW * *	***	MEN	***	****	********* ! * E -*0.05		****	ESE *	= = * *	EN ENI * *	11/4 C
根据	NNW *		WNW * * *	***	MEN	***	****	********* * E -*0.05 * -*0.10 * -*0.15		****	ESE * *	5	SA BAI * * * * * *	414
根据	NNW *		WNW * * * *	***	MEN	***	****	********* * E -*0.05 * -*0.10 * -*0.15 *		****	ESE * *	5 8 * * *	NE NE * * * *	414
根据	NNW *		WNW * * *	***	MEN	***	****	********* * E -*0.05 * -*0.10 * -*0.15 * -*0.20 *		****	ESE * *		SA BAI * * * * * *	414
根据	NNW *		WNW * * *	***	MEN	***	****	********** * S -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25		****	ESE * *		SA BAI * * * * * *	414
根据	NNW *		WNW * * *	***	MEN	***	****	********* * E -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30		****	ESE * *		SA BAI * * * * * *	414
根据	NNW *		WNW * * *	***	MEN	***	****	********** * E -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.05		****	ESE * *		SA BAI * * * * * *	414
根据	NNW *		WNW * * *	***	MEN	***	****	********* * E -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30		****	ESE * *		SA BAI * * * * * *	414
根据	NNW *		WNW * * *	***	MEN	***	****	********** * E -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.30 * -*0.35 * -*0.40 * -*0.40		****	ESE * *		SA BAI * * * * * *	414
根据	NNW *		WNW * * *	***	MEN	***	****	********** * E -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 -*0.30 * -*0.35 * -*0.35		****	ESE * *		SA BAI * * * * * *	414
根据	NNW *		WNW * * *	***	MEN	***	****	*********** * E -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 -*0.30 * -*0.35 * -*0.45 * -*0.45		****	ESE * *		SA BAI * * * * * *	4/4
根据	NNW *	NW .	WNW * * *	***	MEN	***	****	*********** * E -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 -*0.30 * -*0.35 * -*0.35 * -*0.35 * -*0.55 * -*0.45 * -*0.50 * -*0.55		****	ESE * *		SA BAI * * * * * *	414
根据	NNW *	NW .	WNW * * * * * * * * * * * * * * * * * *	***	MEN	***	****	************** * -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 -*0.30 * -*0.35 * -*0.45 * -*0.45 * -*0.50		****	ESE * *		SA BAI * * * * * *	414
根据	NNW *	NW .	WNW * * * * * * * * * * * * * * * * * *	***	MEN	***	****	************* * E -*0.05 * 0.10 * 0.15 * 0.20 * 0.25 * 0.30 * 0.30 * 0.40 * 0.45 * 0.45 * 0.50		****	ESE * *		SA BAI * * * * * *	414
根据	NNW *	NW .	WNW * * * * * * * * * * * * * * * * * *	***	MEN	***	****	*********** * * * * * * * * * * * * *		****	ESE * *		SA BAI * * * * * *	414
根据	NNW *	NW .	WNW * * * * * * * * * * * * * * * * * *	***	MEN	***	****	********** * E -*0.05 * 0.10 * 0.15 * 0.20 -*0.25 -*0.30 * 0.35 -*0.40 * 0.45 -*0.45 -*0.50 * 0.55 -*0.50 * 0.55 -*0.50 * 0.55 -*0.50 * 0.55 -*0.50 * 0.55 -*0.50		****	ESE * *		SA BAI * * * * * *	414
根据	NNW *	NW .	WNW * * * * * * * * * * * * * * * * * *	***	MEN	***	****	*********** * * * * * * * * * * * * *		****	ESE * *		SA BAI * * * * * *	414

DISJUE AFION COSEFICIENTS

FOS STITION: LOM-S-UT

MIT. STATION: AES- LOND

NUMBER OF VALID DAYS: 15

PCE CONCENTRATION VS WIND DIRECTION

	N	NNW	NN NN	DIRECTION WNW	¥.	WSM	'S \	SSW
. 828 . 6 87012	0.5325 0.2450 1.5557	0. 24 2 4 0. 2475 0. 7972	0.2469 0.5234 1.0276	0.3447 0.9293 1.4687	0.1954 0.0522 0.7970	0.3747 0.2197 1.8245	-0.0370 -0.0478 -0.1479	-0.0106 -0.0053 -0.0423
	ş	SSE	95	ESE	E	ENE	NE	NNÉ
F BLOFI	0.14 87 0.0491	0.0438 0.0112	-0.2044 -0.0695	-0.0770 -0.0193	-0,2976 -0,0973	-0.3086 -0.0891	0.0429 0.0545	-0.0840 -0.1247

PCD COMMENTRATION VS WIND SPEED

		WIND	SPEED (KM/	HR)	
	0 - 5	5 - 10	10 - 15	15 - 20	>20
1-	0.0740	0.3131	0.1910	-0.0953	-0.3011
SLOPE	0.0176	0.0776	0.0623	-0.0429	-0.0456
	0.2967	1.3423	o.7735	-0.5330	-1.2630

PCB	CONCENTRATION	VS	AVER	AGE	TEMPERATURE:	r SLOPE t SIG	0.4046 0.3377 1.7696 90%
PCB	CONCENTRATION	VS	STD	DEV	TEMPERATURE:	r SLOPE t	-0.1239 -0.4967 -0.4996

			OWNERS OF BERNING THESE	
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DURNELATION COEFFICIENTS

FILE STAFION: MIS-S-U1

MET. BIATION: MOE-35033

MINITER OF VALIE PAYS: 24

FOD CONCENTRATION VS WIND DIRECTION

	N		WINE NW	DIRECTION NAM	**	11 T.V	ΞW	EVEC 1
BLIFE t sig	0.2094 0.0638 1.0044	-0.0125 -0.0074 -0.0588	0.0424 0.0429 0.1990	0.0008 0.0006 0.0037	-0.2945 -0.0625 -1.4954	0.0122 0.0046 0.0570	0.1261 0.1000 0.5964	0.7304 0.4902 5.0199 99%
	S	EEE	ΞE	EBE	Ξ	ENE	ME	NNE
r SLOPE	0.5133	-0.0455	-0.2863	-0.1774	-0.0137	-0.0471	-0.0998	0.0729

POB CONCENTRATION VS WIND SPEED

		MIND	SFEED (KM.	/HR)	
	2 - ₹	5 - 10	10 - 15	15 - 20	>20
r	0.2650	-0.1669	-0.0348	-0.2510	0.0317
SLIPE	0.0471	-0.0369	-0.0100	-0.0946	0.0205
t	1.2059	-0.7738	-0.1633	-1.2151	0.1485
BID					

FCB	CONCENTRATION	VΞ	AVE:	RACE	TEMPERATURE:	r SLOPE t SIG	0.3772 0.3566 1.9103 90%
PCB	CONCENTRATION	VS	STD	DEV	TEMPERATURE:		0.0824 5.3375 6.3890

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	COSTRUCTION	COLFFI	CIENTE VE WIND	DIRECTION			
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COURT ATION COSFFICIENTS

FIR STATION: MIS-S-US

MIT. ITATION: MOERCEOSA

NUMBER OF VALID DAYS: 20

FIR ICHOENTRATION VS WIND DIRECTION

		NNW	WIKE Nij	DIRECTION UNW	EN EX	WED.	700	58: <i>1</i>
: SLOPE • t • SIG	0.3722 0.0579 6.8385	-0.1291 -0.0760 -0.6294		-0.0338 -0.0241 -0.1624	1.07.0	-0.1594 -0.0624 -0.7745	-0.1238 -0.1005 -0.5905	0.5298 0.3623 2.9956 99%
	5	SEE	<u> </u>	ESE	E	ENE	NE	NNE

PCB CONCENTRATION VS WIND SPEED

		WIND	SPEED (KM/	(HRI)	
	0 - 5	5 - 10	10 - 15	15 - 20	>20
100	0.0648	-0.0576	0.0533	-0.1168	0.0129
SLOPE	0.0112	-0.0126	0.0174	-0.0417	0.0098
• 0	0.3112	-0.1738	C. 2816	-0.5639	0.0616
SIG					

P 33	CONCENTRATION	VS	AVE	RAGE	TEMPERATURE:	SLOPE t SIC	0.3819 0.3435 1.9818 90%
PCB	CONCENTRATION	VS	STD	DEV	TEMPERATURE:	r SLOPE t	0.1799 0.7478 0.8772

		CIRCLATION	COEFFICIENTS VS LIND	DIRECTION			
I.E	TT::::::::::::::::::::::::::::::::::::		440.75			TIME:	
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	*	**		*	*	*		*		*	*				30
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CIMPATION COSTFICIONTS

PCD ETATION: MIB-E-UD

MIT. STATION: MOE-SECSE

NUMBER OF VALID DAYS: 25

POP DINGENTRATION VS WIND DIRECTION

	1. I.		WINE NW	DIFECTION WILL	119 22	MEN	SW	SSW
r 913P5 t	0.2654 0.1165 1.3203	0.1981 9.1547 8.9720	0.2539 0.3614 1.2591	0.0018 0.0018 0.0084	-0.3110 -0.0978 -1.5393	-0.1617 -0.0905 -0.7857	0.1084 0.1260 0.7241	0.5492 5.4884 3.3205 99%
	8	SEE	SE	ESE	Ξ	ENE	NE	MAZE
SLUPE t SIG	0.5517 0.4077 3.1724 99%	-0.0146 -0.0065 -0.0701	-0.2070 -0.1473 -1.0145	-0.2442 -0.1310 -1.2076	0.0494 0.0494 0.8300	0.0133 0.0129 0.0333	-0.1703 -0.0609 -0.9287	-0.0785 -0.0511 -0.3775

POB CONCENTRATION VS WIND SPEED

		HIND	SPEED (KM/	(日尺)	
	O - E	5 - 10	10 - 15	15 20	>20
i-	0.2094	0.0517	-0.1781	-0.2142	0.0377
SLOPE	0.0555	0.0166	-0.0740	-0.1754	0.0394
• t	1.0270	0.2453	-0.8678	-1.5971	0.1906

FCD	CONCENTRATION	VΞ	AVERAGE	TEMPERATURE:	r	0.4115
					SLOFE	0.5668
					+	2.1656
					818	75%

PCE	CONCENTRATION	VE	STD	DEV	TEMPERATURE:	96	-0.0360
						SLOFE	-0.2207
						T	-0.1765
						SIG	

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* **	***	*	****	W * * * * * *	WSW * * *	****	* ******	* * ********* * S -*0.05 * -*0.10 * -*0.15 *		3E * * *	ESE * * *	* *****		NE *	
* **	***	*	****	X	WSW * * *	****	* ******	* * ********* * S -*0.05 * -*0.10 * -*0.15		3E * * * * *	E * * * * * * * * * * * * * * * * * * *	* *****		NE *	
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* **	***	*	****	W******	WSW * * *	****	* ******	* * * * * * * * * * * * * * * * * * *	SSE	3E * * * * *	ESE * * * * *	* *****		NE *	
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DOW OF ATIOM COEFFICIENTS

POD STATION: MIS-S-U4

KET. STATION: MCE-95037

NUMBER OF VALIE DAYS: 27

PCD CENCENTERTION VO WINE DIFECTION

	14	1	KIME NG	DIRECTION WNW	W	WSW	€ ₩	SEW
; SL3FE • t	0.0261 0.0082 0.1307	-0.2145 -0.1175 -1.0983	-0.2132 -0.1959 -1.0911	-0.0110 -0.0074 -0.0551	-0.3529 -6.0128 -0.3153	-0.0466 -0.0165 -0.2334	-0.0662 -0.0468 -0.3319	0.2137 0.1347 1.0938
	s	SSE	8 E	E9E	Ξ	ENE	ΝE	NNE

PCD CONCENTRATION VS WIND SPEED

		WIMD	SPEED (KM/	(HR)	
	0 - 5	5 - 10	10 - 15	15 - 20	>20
7	-0.1752	-0.0267	o. 1475	-0.0303	0.5189
SLOPE	-0.0270	-0.0053	0.0404	-0.0101	0.3256
τ	-0.8903	-0.1995	0.7456	-0.1515	3.0350
212					99%

500	CENCENTRATION	VS	AVE	RAGE	TEMPERATURE:	r SLOPS t SIG	0.0541 0.0480 0.2810
PCB	CONCENTRATION	VS	STD	DEV	TEMPERATURE:	r SLCPE t SI3	0.4323 1.6051 2.3972 95%

### ### ##############################					COR	A		COEFFE	SIENTS VS	WIND	DIREC	OT E SIM				
VALID DAYS: 27	1.1-	-	N: ME	-35033			E 151072	100 m					STAR	T T	IME:	10
### 10, 60	I i m	- 7														
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* +0.10 * * * * * * * * * * * * * * * * * * *								*								
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* + *0.05 * * * * * * * * * * * * * * * * * * *								<u>N</u> .	St						*	
# +0.05								12	-×0.10×						*	
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N NNW NW UNW W WSW SW SSW S SSE SE ESE S ENE NE NR * * * * * * * * * * * * * * * * * * *								×	-*O.05*					*	*	
N NNW NW UNW W WEW SW SSW * S SSE SE SE S ENE NE NN * * * * * * * * * * * * * * *	*							*	* *				2	*	*	
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* * * * -*0.20	N	*	*	UNW		lv a'W		5,5%	-×0.05 *	994	*	*	Ξ.	ENE		
* * -*0.20	N	**	*	DNW		NEW .		5.54	-*0.05 * -*0.10	952	* *	* *	=	=N=	. 1/=	•
* -*0. 25 * -*0. 30 * -*0. 35 * -*0. 40 -*0. 50 * -*0. 55 -*0. 65 * -*0. 65 * -*0. 70 * * -*0. 65	N	* * *	* *	SNR		N EW		534	-*0.05 * -*0.10 *	952	* * *	* * *	2	=1/10	. 1/2	•
* -*0. 25 * 0. 30 * 0. 35 * 0. 40 -* 0. 45 -* 0. 50 * 0. 55 -* 0. 65 * 0. 65 * 0. 70 * 0. 70	N	* * * *	* * * * *	SNR		NSW		534	-×0.05 * -*0.10 * -*0.15	2512	* * *	* * * *	2	=1,7=	. 1/3	•
* -*0.30 * -*0.35 * -*0.40 -*0.50 * -*0.50 * -*0.60 * -*0.60 * -*0.65	N	* * * * * * * * * * * * * * * * * * * *	* * * * *	SNK		%≥W		534	-*0.05 * -*0.10 * -*0.15	255	* * *	* * * * * *	5	ENE.		•
* -*0.30 * -*0.35 * -*0.40 -*0.50 * -*0.50 * -*0.60 * -*0.60 * -*0.65	N	* * * * * * * * * * * * * * * * * * * *	* * * * *	SNR		WEW		534	-*0.05 * -*0.10 * -*0.15 * -*0.20	355	* * *	* * * * * * * * * * * * * * * * * * * *	5	= N=		•
-*0.30 * -*0.35 * -*0.40 -*0.65 * -*0.65 * -*0.65 * -*0.70 *	N	* * * * * * * * * * * * * * * * * * * *	* * * * *	SNR		WEW		534	-*0.05 * -*0.10 * -*0.15 * -*0.20	255	* * *	* * * * * * * * * * * * * * * * * * * *	5	<u> </u>		
* -*0.35 * -*0.40 -*0.45 * -*0.50 * -*0.55 -*0.65 * -*0.70	N	* * * * * * * * * * * * * * * * * * * *	* * * * *	SNR		₩SW		D 20 A	-*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25	355	* * *	* * * * * * * * * * * * * * * * * * * *	2	= N=		•
-*0.35 * -*0.40 -*0.45 -*0.50 * -*0.65 * -*0.65	N	* * * * * * * * * * * * * * * * * * * *	* * * * *	SNR		₩SW		534	-*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25	355	* * *	* * * * * * * * * * * * * * * * * * * *	2	= N=		•
* -*0. 40 -*0. 45 -*0. 50 * -*0. 55 -*0. 65 * -*0. 65	N	* * * * * * * * * * * * * * * * * * * *	* * * * *	SNR		₩SW		534	-*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 *	355	* * *	* * * * * * * * * * * * * * * * * * * *	<u> </u>	=1%=		•
-*0.40 -*0.45 -*0.50 * -*0.55 -*0.60 * -*0.65	N	* * * * * * * * * * * * * * * * * * * *	* * * * *	SNK		WEW		534	-*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 *	355	* * *	* * * * * * * * * * * * * * * * * * * *	<u>J</u>	=1%=		
-*0.45 -*0.50 * -*0.55 -*0.60 * -*0.65	N	* * * * * * * * * * * * * * * * * * * *	* * * * *	SNK		WEW		034	-*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 *	255	* * *	* * * * * * * * * * * * * * * * * * * *	<u>J</u>	= 1 1 1		·
-*0.50 * -*0.55 -*0.60 * -*0.65 * -*0.70		* * * * * * * * * * * * * * * * * * * *	* * * * *	SNK		WEW			-*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.35 *		* * *	* * * * * * * * * * * * * * * * * * * *	J1	=.1%=		•
-*0.50 * -*0.55 -*0.60 * -*0.65 * -*0.70	N	* * * * * * * * * * * * * * * * * * * *	* * * * *	SNK		WEW			-*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.35 * -*0.40		* * *	* * * * * * * * * * * * * * * * * * * *		=./\=		•
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-*0.55 -*0.60 * -*0.65 * -*0.70	N	* * * * * * * * * * * * * * * * * * * *	* * * * *	SNK		WSW.			-*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.35 * -*0.40 * -*0.40 *		* * *	* * * * * * * * * * * * * * * * * * * *		= 1/1=		· ·
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* -*0.70 *	N	* * * * * * * * * * * * * * * * * * * *	* * * * *	SNK		WSW.			-*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.35 * -*0.40 * -*0.55 * -*0.50 * -*0.55		* * *	* * * * * * * * * * * * * * * * * * * *				
-*0.70 *	N	* * * * * * * * * * * * * * * * * * * *	* * * * *			WEW.			-x0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.35 * -*0.40 * -*0.50 * -*0.55 * -*0.50 * -*0.55		* * *	* * * * * * * * * * * * * * * * * * * *				in the second se
•		* * * * * * * * * * * * * * * * * * * *	* * * * *			WEW.			-x0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.35 * -*0.40 * -*0.40 * -*0.55 * -*0.60 * -*0.65		* * *	* * * * * * * * * * * * * * * * * * * *				in the state of th
		* * * * * * * * * * * * * * * * * * * *	* * * * *			WEW.			-x0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.35 * -*0.40 * -*0.45 * -*0.60 * -*0.65 * -*0.65 *		* * *	* * * * * * * * * * * * * * * * * * * *				
200 Mg - 200 Mg		* * * * * * * * * * * * * * * * * * * *	* * * * *			WEW.			-x0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.40 * -*0.45 * -*0.55 * -*0.65 * -*0.65 * -*0.70		* * *	* * * * * * * * * * * * * * * * * * * *				NI.

-*0.75

CORRELATION COEFFICIENTS

FOR STATISMA MODIFICALS

MET. STAITION: MCE-12034

MUNDER OF VALUE DAYS: 21

POB CONCENTRATION VS WIND DIRECTION

	M	MAN	NW MIND	DIRECTION WNW	ω	WSW	sw	SSW
r SLIPE 500	0.0073 0.0034 0.0333	-0.1259 -0.1447 -0.6216	0.0521 0.0217 0.2582	-3.0448 -0.0118 -0.2189	0.2403 0.1773 1.2124	-0.070& -0.0760 -0.3468	0.0871 0.0597 0.4284	0.4312 0.4607 3.9865 99%
•	S	SSE	SE	ESE	Ε	ENE	ΝΞ	NNE

DOE SINCENTRATION VS WIND CREED

		WIND	SPESS (KM/	YHR)	
	o - 5	5 - 10	10 - 15	15 - 20	>20
r	0.1761	-0.0703	0.0207	-0.1090	-0.0907
SLIFE	0.0277	-0.0113	0.0054	-0.0233	-0.0323
t 579	0.8743	-0.3452	0.1013	-0.5370	-0.4549

. T	CONCENTRATION	VĐ	HVER	HUE	TENTERH!URE:	SLOPE t BIG	0.0429 0.3041
POS	CONCENTRATION	VΞ	ETC	DEV	TEMPERATURE:	r SLOPE t SIG	-0.1325 -0.4170 -0.4551

DORRELATION COEFFICIENTS VS WIND DIRECTICA WIND STM: MCR-12034 **0.75 POB STM: MCR-9-U1 **0.70

START TIME: 12 Valid Days: 25

N

--0.65

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+>0, ≥0 #

+*0. EI

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10

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* -<0.45* * * *

+×0.40*

* * -*0.35%

* * *

+*0.30* * * +*0.25*

+*0, 15%

+>0.20×

* * +*0.10*

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· (1) 中心部外的大學學院的學術學院學院學院學院學院學院學院學學學學院學院教育學學學學學學院與實際原理學院與與學院與與學療學院與實際學療養

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1	NNR	NW	WINW	W	WEW	ΞW	398	*	3	EEE	ΞE	ΞΞΞ	Ξ	ENE	NE
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	4							-*0.1	0	4-	*		*	쑞.	
	*							+%-		25-			*		
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-80.75

DIRECT ATION COEFFICIENTS

POD STAFION: MAN-3-R1

MET. STATION: MYD- NANT

NUMBER OF VALID CAYS. AT

FOR CONCENTRATION WE WAND BIRSOTICH

	r.i	Wiel	WIND NJ	DIRECTION WNW		WENT.	ΞW	55.7
SLOPE * BIC	0.2730 0.2565 1.5322	6.1346 0.0556 0.6792	0.1011 0.0207 0.5079	0.0714 0.0459 0.3580	-6.0267 -0.0327 -0.1336		-0.0903 -0.0907 -0.4534	-0.1094 -0.0551 -0.5508
2	3	SSE	SE	ESE	Ξ	ENE	1:5	NME
2127E		-0.1478 -0.0295 -0.7316	-0.1309 -0.0340 -0.4602	0.0047 3.0010 0.0236	-0.0026 -0.0004 -0.0120	-0.0529 -0.0214 -0.2648	-0.0489 -0.0354 -0.3455	0.1810 0.0796 0.9200

POS INMOSKIRATION VS WIND SPEED

		MIND	SPEED (KM)	(HR)	
	0 - 5	5 - 10	10 - 15	15 - 20	>20
r	0.0100	0.1790	-0.0555	-0.2350	-0.3278
SLOFE	0.0399	1.0348	-0.0134	-0.0696	-0.0468
• •	2. 2529	0.9097	-C. 277&	-1.2070	-1.7349
319	95%				90%

FCE	CONCENTRATION	$\vee \Xi$	AVESA3E	TEMPERATURE:	/ *	0.2734
					SLUFE	0.1591
					t	1.4213
					空正位	

FCI	COMMENTRATION	VΞ	STD	DEV	TEMFERATURE:	r	0.0477
						SLUFE	0.2236
						t	0.2386
						515	

CORRELATION COEFFICIENTS VS WIND DIRECTION KIND CTM: AYE- NANT RDE STN: NAN 3-31 --0.75 START TIME: VALID DAYE: 27 - :0.70 -*O.65 ++0. (4) 381 1 ---0. E0 ++0.45 --0.40 250 -*O.35 4 +*O.30 -*0.25 -44 +*0.20 -33-35 10 +÷0.15 -5-44 +*O. 10 15 35 35 432 1 -*O.05* 35 * S SSE SE ESE E ENE NE NA NES DE DEW W WAN NA WAY NE -*0.05 * 125 434 - 14 25 * * * 2 44 34 -÷0.10 * 5 -85 -8-* -*0.20 -*0.25 6. -*0.30 24. -#0.35 -87 -∻O.40 -24--40.45 * -∻0.∃0 -*0.55 - 4 -+0.60 × --0.35 -5 -≠0.70

* -÷0.75

STREE ATION COEFFICIENTS

FOR STATICAL CARASTA

MET. STATION: HYD- MANT

NUMBER OF VALUE DAMES IN

POS CONCENTRATION VE WIND DIRECTION

	M	NNW	NM MIND	DIRECTION WAW	L.	ИSИ	SW	EEW
STOUS STOUS STOUS	0.1684 0.1724 0.9351	0.2678 0.1291 1.8872	0.4245 0.1141 2.3443 95%	0.2540 0.2062 1.7047 90%	0.1329 0.1904 0.3703	0.0539 0.0661 0.2697	0.0779 0.0915 0.3907	0.0091 0.0054 0.0456
	S	SSE	85	EEE	Ξ	ENE	NE	NNE
r SLIPE	0.1301 0.0536	-0.0329 -0.0198	-0.3787 -0.1218	-0.1546 -0.0343	-0.2362 -0.0436	-0.2168 -0.1027	0.0602 0.0354	C.1918 O.0785

POB CONCENTRATION VS WIND SPEED

		WIND	SPEED (KM)	(HR)	
	0 - 5	5 - 10	10 - 15	15 - 20	>20
r	0.3120	0.3333	-0.1066	-0.2508	-0.3408
SLOPE	0.0593	0.0729	-0.0317	-0.0849	-O. OE49
• -	1.6421	1.7976	-0.5340	-1.2954	-1.8123
SIG		90%			90%

FCB	CONCENTRATION	VΞ	AVERAGE	TEMPERATURE:	r	0.2593
					SLOPE	0.2048
					=	1.3415
					SIG	

FCB	CONCENTRATION	VS	STD	DEV	TEMPERATURE:	r	0.3069
						SLIPE	1.6277
						45	1.6125
						808	

				F. (7)	ERTI AT	7.53		CIENTS VE	17 - 17	FITEFI	7-60				
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茶	*	**	**					+#C.15							
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47	**	45	*	20				-*C.10#							
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9.0	74.5	(2)		(6.5)	100									-055	
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홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****	4-4-5		· 중 중 중 중 중 중 중 중 중 중 중						***	
							::::::::::::::::::::::::::::::::::::::	* S	88888 88E	**** 3E	**** E3E	E *****	ENE		sse: Ni
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****	4-4-5		· 중 중 중 중 중 중 중 중 중 중 중						***	
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****	4-4-5		* S	SSE	SE	ESE	Ξ	ΞXΞ	***	
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****	4-4-5		******* * S -*0.05 *	99E *	3E *	ESE	E *	ΞΝΞ *	***	
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****	4-4-5		* S -*0.05 * -*0.10	99E *	SE * *	ESE * * *	₩ * *	ENE * *	***	
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****	4-4-5		* * * * * * * * * * * * * * * * * * *	99E *	SE * * *	ESE * * *	Ε * * * *	ENE * *	***	
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		* * * * * * * * * * * * * * * * * * *	99E *	SE * * * * *	ESE * * *	E * * * * * *	EXE * * * *	***	
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		* * * * * * * * * * * * * * * * * * *	99E *	3E * * * * * *	ESE * * *	U * * * * *	ENE * * * * *	***	
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		************* * S -*0.05 * -*0.10 * -*0.15 * -*0.20	99E *	0 * * * * * * * *	ESE * * *	E * * * * * *	EXE * * * *	***	NI
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		********** * S -*0.05 * -*0.10 * -*0.15 * -*0.20	99E *	3E * * * * * *	ESE * * *	U * * * * *	ENE * * * * *	***	NI
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		********** * S -*0.05 * -*0.10 * -*0.15 * -*0.20	99E *	0 * * * * * * * *	ESE * * *	U * * * * * * *	ENE * * * * *	***	NI
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		********** * 9 -*0.05 * -*0.10 * -*0.15 * -*0.20 *	99E *	(i)	ESE * * *	U * * * * * * *	ENE * * * * *	***	NI
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		************ * 9 -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 *	99E *	60 * * * * * * * * * * * * * * * * * * *	ESE * * *	U * * * * * * *	ENE * * * * *	***	NI
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		************** * S -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30	99E *	EU * * * * * * * * * * * * * * * * * * *	ESE * * *	U * * * * * * *	ENE * * * * *	***	NI
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		************** * S -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.30	99E *	00 * * * * * * * * * * * * * * * * * *	ESE * * *	U * * * * * * *	ENE * * * * *	***	NI
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		************** * S -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.35	99E *	EI * * * * * * * * * * * * * * * * * * *	ESE * * *	U * * * * * * *	ENE * * * * *	***	NI
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		********** * S -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.35	99E *	00 * * * * * * * * * * * * * * * * * *	ESE * * *	U * * * * * * *	ENE * * * * *	***	NI
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		************** * S -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.35	99E *	EI * * * * * * * * * * * * * * * * * * *	ESE * * *	U * * * * * * *	ENE * * * * *	***	NI
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		************* * S -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.35 * -*0.40	99E *	EI * * * * * * * * * * * * * * * * * * *	ESE * * *	U * * * * * * *	ENE * * * * *	***	NI
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		************* * S -*0.05 * -*0.10 * -*0.20 * -*0.25 * -*0.30 * -*0.35 * -*0.40 * *	99E *	EI * * * * * * * * * * * * * * * * * * *	ESE * * *	U * * * * * * *	ENE * * * * *	***	NI
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		*********** * S -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.35 * -*0.40 * -*0.45	99E *	EI * * * * * * * * * * * * * * * * * * *	ESE * * *	U * * * * * * *	ENE * * * * *	***	NI
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		********** * S -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.35 * -*0.40 * -*0.45	99E *	EI * * * * * * * * * * * * * * * * * * *	ESE * * *	U * * * * * * *	ENE * * * * *	***	NI
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		*********** * S -*0.05 ** -*0.10 * -*0.15 * -*0.20 * -*0.30 * -*0.35 * -*0.40 * -*0.45 -*0.50	99E *	EI * * * * * * * * * * * * * * * * * * *	ESE * * *	U * * * * * * *	ENE * * * * *	***	NI
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		********** * S -*0.05 ** -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.40 * -*0.45 -*0.50 *	99E *	EI * * * * * * * * * * * * * * * * * * *	ESE * * *	U * * * * * * *	ENE * * * * *	***	NI
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		*********** * S -*0.05 ** -*0.10 * -*0.15 * -*0.20 * -*0.30 * -*0.35 * -*0.40 * -*0.45 -*0.50	99E *	EI * * * * * * * * * * * * * * * * * * *	ESE * * *	U * * * * * * *	ENE * * * * *	***	NI
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		********** * S -*0.05 ** -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.40 * -*0.45 -*0.50 *	99E *	EI * * * * * * * * * * * * * * * * * * *	ESE * * *	U * * * * * * *	ENE * * * * *	***	NI
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		*********** * S -*0.05 **0.10 * 0.20 * -*0.25 -*0.30 * 0.35 * -*0.40 * -*0.45 -*0.50 * -*0.50	99E *	EI * * * * * * * * * * * * * * * * * * *	ESE * * *	U * * * * * * *	ENE * * * * *	***	NI
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		********** * S -*0.05 ********* ********* ********* *****	99E *	EI * * * * * * * * * * * * * * * * * * *	ESE * * *	U * * * * * * *	ENE * * * * *	***	NI
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		********** * S -*0.05 * -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.40 * -*0.45 -*0.50 * -*0.50 * -*0.50 * -*0.50 * -*0.50 * -*0.60 * -*0.60	99E *	EI * * * * * * * * * * * * * * * * * * *	ESE * * *	U * * * * * * *	ENE * * * * *	***	NI
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		********** * S -*0.05 **0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.40 * -*0.45 -*0.50 * -*0.55 -*0.55	99E *	EI * * * * * * * * * * * * * * * * * * *	ESE * * *	U * * * * * * *	ENE * * * * *	***	NI
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		********** * S -*0.05 -*0.10 * -*0.15 * -*0.20 * -*0.30 * -*0.35 * -*0.40 * -*0.45 -*0.50 * -*0.55 -*0.60 * -*0.65 * -*0.65	99E *	EI * * * * * * * * * * * * * * * * * * *	ESE * * *	U * * * * * * *	ENE * * * * *	***	NI
홍 홍 .	5 4 4 4 4	****	FK 1440	\$ 1 K \$1.	****** W3W	4-4-5		********** * S -*0.05 **0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.40 * -*0.45 -*0.50 * -*0.55 -*0.55	99E *	EI * * * * * * * * * * * * * * * * * * *	ESE * * *	U * * * * * * *	ENE * * * * *	***	NI

-÷0.75

CONTRACTION DESTRICTS

PCI CLATION: GEM-E-U1

MET. STATION: MOE-45025

MUMBER OF MALIE DAYS: 24

FOR COMPENTABLION VE WINE DIRECTION

N	NNW	NW NW	DIRECTION WNW		* * * * * * * * * * * * * * * * * * *	E.,	SCN
-0.0337 -0.0162 -0.1663	0.1694 0.1271 0.8422	0.1031 0.1041 0.5079	C. 2262 C. 1880 1. 1876	0,3041 0.1603 1.5340	-0,1369 -0,0509 -0,6789	-0.0831 -0.0274 -0.4083	-0.0417 -0.0158 -0.2050
S	88 5	ΞΞ	ESE	Ξ	EME	NE	NNE

FOR CONCENTRATION VS WIND SPEED

		WINI	EPEED (KM)	/ F.≅)	
	0 - E	5 - 10	10 - 15	15 - 20	> 30
je.	0.1502	-0.1700	-0.0590	-0.0259	-0.0495
SLOPE	0.0227	-0.3414	-0.0165	-C.CZ:C	-0.1741
513	0.7443	-0.8452	-0.9397	-0.1414	-0.2543

FCS	CONCENTRATION	VS	AVERAGE	TEARERATURE:	r SLOPE t SIS	0.3630 0.3539 1.9095 90%
SIE	CONSENTRACION	VS	STE CEV	TEMPERĄTURE:	SIS	0.0234 0.0915 0.1147

						TITAL (TEFFI	CIENTS VS	MIND	DIREC	7754				
G 1	-		-4502	=				480.75				977	DT -	INE:	17
	rain in			-										DAYS:	26
	er jaar	ALL COLOR (MATERIAL COLOR						+*0.70							
								3							
								-×0.65							
								4							
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	-X-	**	**	*				+*0.05		14	- 32	*			
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			V-950C							30	100	7.			
45-35-3					554454	****	****		* * * * * * * *				****	****	***
	****	*****	* * \$ \$ \$	\$ 8.8 \$				水水水水水水水水		***		****	**** ENE		
⊹÷: N		*****			WEW	SW	88% 88%	* 3	: 24243 53E						
	****	*****	* * \$ \$ \$	\$ 8.8 \$	WEW *	SW *		******* * 3 -*0.05%		***		****			
	****	*****	* * \$ \$ \$	\$ 8.8 \$	WEW	SW		******* * 3 -*0.05* * *		***		****			
	****	*****	* * \$ \$ \$	\$ 8.8 \$	WSW *	SW *		******* * S -*0.05* * * -*0.10*		***		****			
	****	*****	* * \$ \$ \$	\$ 8.8 \$	WEW *	SW *		******** * S -*0.05* * * -*0.10*		***		****			
	****	*****	* * \$ \$ \$	\$ 8.8 \$	WSW *	SW *		******** * S -*0.05* * * -*0.10* * * -*0.15*		***		****			
	****	*****	* * \$ \$ \$	\$ 8.8 \$	WSW *	SW *		******** * S -*0.05* * * -*0.10* * * -*0.15* * *		***		****			
	****	*****	* * \$ \$ \$	\$ 8.8 \$	WSW *	SW *		******** * S -*0.05* * * -*0.10* * * -*0.15* * * -*0.20*		***		****			
	****	*****	* * \$ \$ \$	\$ 8.8 \$	WSW *	SW *		******** * S -*0.05* * * -*0.10* * * -*0.15* * * -*0.20* * *		***		****			
	****	*****	* * \$ \$ \$	\$ 8.8 \$	WSW *	SW *		******** * S -*0.05* * * -*0.10* * * -*0.15* * * -*0.20* * *		***		****			
	****	*****	* * \$ \$ \$	\$ 8.8 \$	WSW *	SW *		******** * S -*0.05* * * -*0.10* * * -*0.15* * * -*0.20* * * -*0.23*		***		****			
	****	*****	* * \$ \$ \$	\$ 8.8 \$	WSW *	SW *		******** * S -*0.05* * * -*0.10* * * -*0.15* * * -*0.20* * * -*0.25* * *		***		****			
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COMMENTION COEFFICIENTS

PIR STATION: STORE RI

MIT. OTAFICK: MCE-27047

MINIER OF VALUE CAME: 26

POD CONSENTRATION VE WIND DIRECTION .

	N	N	WA WA	DIRECTION WWW		WEW	5 %	SSN
. 313 37132 37132	0.4671 0.4216 2.5373 95%	0.2050 0.1590 1.0263	0.0226 0.0086 0.1108	0.0103 0.0079 0.0529	-0.2917 -0.2203 -1.4382	0.3928 0.3874 2.0923 53%	0.4268 0.3691 2.8131 95%	0.1035 0.0038 0.5094
	3	SSE	SE	ESE	Ε	ENE	NE	NNE
SILOPE	0.0291 0.0128 0.1425	0.0174 0.0059 0.0852	-0.2176 -0.1317 -1.3920	0.0129 0.0059 0.0427	-0.2502 -0.0548 -1.2459	-0.0728 -0.0320 -0.3574	0.0045 0.0070 0.0218	-0.2394 -0.4024 -1.2082

POB CONCENTRATION VS WIND SPEED

		WINE	SPEED (KM.	/HR)	
	0 - 5	5 - 10	10 - 15	15 - 20	>20
r	0.4558	-0.3894	-0.3383	-0.2015	-0.0820
SLOPE	0.0954	-0.1549	-0.1044	-0.1353	-0.1/21
· +	2.5096	-2.0709	-1.7614	-1.0077	-0.4031
313	95%	95%	90%		

PCE	CONCENTRATION	VS	AVERAGE	TEMPERATURE:		0.1142 0.1250
					τ	0.5630
					SIS	

200	CONCENTRATION	VΞ	STD	DEV	TEMPERATURE:		-0.4103
				tri		SLOPE	-1.9534
						t	-2.2043
						313	95%

CORRELATION COSFFICIENTS US WIND DIRECTION START TIME: 14 VALID DAYS: 25 WIND STY: NOE-27049 +40.75 %705 STM:STC-9-R1 4°0.70 2.5 ~중이**.** 상당 ->0.3O **0.55 -27-+*O.50 - 15-+*0.45 4 ĸ. +*0.40 -14 ≯ ¥. -*O.35 ÷ × × -3-×-35 4*0.30 -5-* -≃-≾ * +<0.25 * * 4. -32 +*O.20 * * .× × ÷ * * *-4*O.15 -5-Ψ. 4 * ÷-× * -*C.10 # * 42 χ. -24 13 ÷. * +*0.05 35 ¥-× × * * * 송 중 · .\$-* Handa de de maria de la compansión de la N NNW NW WNW W WSW SW SSW * S SSE SE ESE E ENE NE NN

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INRIELATION COEFFICIENTO

FOD STATION: SAR-S-I1

KET. STATICKE MOE-14016

"INTER OF VALCE DAYS: 24

FOR CONCENTRATION VS WIND DIRECTION

	N	HNW	MIND	DIFICTION:		NBM	9k'	350
31.3PE • : • :	0.1560 0.1749 0.7407	0.6392 0.4134 3.3982 79%	0.5531 0.6093 3.1218 99%	0.1033 0.0763 0.4872	0.1003 0.4074 0.9105	-0.1124 -0.0767 -0.5806	-0.0309 -0.0534 -0.3805	0.1460 0.0916 0.4922
	8	SSE	85	ESE	_	ENE	NE	NNE
•		See See See			_	=:==	. 4.	

PCB COMMENTRATION VS WIND SPEED

		WIND	SPEED (KM/	(HR)	
	0 - 5	5 - 10	10 - 15	15 - 20	>20
٠	0.1303	0.2478	0.2160	-0.1676	-0.2769
SLOPE	0.0494	0.0654	0.0649	-0.0743	-0.0439
t	0.6165	1.1996	1.0378	-0.7975	-1.3514
SIC					

FCE	CONCENTRATION	VS	AVEF	RAGE	TEMPERATURE:		0.4574 0.5093 2.4124 95%
=	CONCENTRATION	VE	675	SEA	TEMPERATURE:	r SLOPE t SIG	-0.0701 -0.4604 -0.4241

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CONSCRIPTION COEFFICIENTS

DOD STAFION: SAF-8-11

MET. STATISM: MOE-18016

MUMBER OF MANIE DAYS: 24

POB CONCENTRATION VS WIND DIRECTION:

	N	NNU	::\\ ::\\	DIRECTIC:: WNW		JEN	8%	551
71 ITE * * 510	5.1710 6.3394 6.9127	0.8904 1.0518 4.4840 99%		-0.0738 -0.1175 -0.0311		H S STREET STATE	-0.2020 -0.2247 -0.9672	
	3	SSE	āΞ	ESE	Ξ	ENE	ΝΞ	MNE
· ILIFE		-0.1657 -0.0833 -0.7883		-0.1832 -0.2496 -0.9487	-0.1395	-0.0423	-0.0309 -0.0161 -0.1449	0.3026 0.3447 1.4893

POB CONCENTRATION VS WIND SPEED

		HIND	SPEED (KM)	(HR)	
	0 - 5	5 - 10	10 - 15	15 - 20	>20
i de la companya de l	-0.0028	C. 1159	0.4367	-0.0339	-0.2549
SLIPE	-0.0019	0.0573	0.2436	-0.0441	-O.O696
	-0.0133	0.5619	2.2769	-0.3003	-1.2358
2; 7 13			93%		

PCB	CONCENTRATION	VS.	AVERAGE	TEMPERATURE:		0.1988
					SLUME t	0.3431 0.9470
					SIG	
FOE	CONCENTRATION	·y.c.	STD DE:	' TEMPERATURE:	~	0.0720

SLCPE 0.8219 t 0.3394 SIG

CIRCLATION COEFFICIENTS VO WIND DIRECTION -- VO. 75 BIART TIME: 22 WallD Days: 25 645.70 -40.55 -----55. 2 way, Ed. +*O.45 $-i - i \sum_{i} \left(\frac{1}{2} \right) \cdot \sum_{i} \left(\frac{1}{2} \right) \cdot \left(\frac{1}{2$ ~ 2.5 +*0.35 2. -\$--5-+*0.30 20 * * -×0.25 46-.50 +*O.20 4-× -2-**O.15 * * -**≯** ∻ 37 4 -*O.10× ---4º × ÷≈0.05* 15 1 * 35 M NNW NN UNW W WEXT SW BEN * S SEE SE ESE E ENE NE MN

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DOMNELATION COEFFICIENTS

POB STATIONS SUD-S-31

MET. STATION: MGE-77025

NUMBER OF VALID DAYS: 24

PCS CONCENTRATION MS WIND DIRECTION

	V	€ (5.11.1 1.1.40°)	WIND NW	DIRECTION WANT	×	WSW	<i>Ξ</i> .	SSW
3L2PE 5 * SI3	0.8011 0.0727 1.6012	6.2831 6.1176 1.2792	0.2359 0.1041 1.8942 90%	0.2370 0.0925 1.1448	0.0435 0.0303 0.2135	0.2379 0.1412 1.1485	0.0488 0.0240 0.3209	-0.2234 -0.0638 -1.0749
	:	SSE	S E	E3E	Ξ	ENE	NΞ	MME
ELEPE : :	-0.3493 -0.0174 -1.7402 TOX	-0.2118 -0.0275 -1.0113	-0.1939 -0.0651 -0.9271	0.0419 0.0094 0.1967	-0.1029 -0.0464 -0.4851	-0.1478 -0.0791 -0.7010	0.0441 0.0121 0.2071	0.0706 0.0105 0.3322

FOR CONCENTRATION WE WIND SPEED

		1.1742	THEEL CAMP	(- 1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	
	0 - 5	5 - 10	10 - 15	15 - 20	20
i.	-0.2911	0.2502	0.2330	0.1466	-0.1300
SLOFE	-0.0481	0.0563	0.0456	0.0334	-0.0139
	-1.4274	1.2123	1.1392	0.6953	-0.6151
5.55					

FOB	CONCENTRATION	V∃	AVE:	RAGE	TEMPERATURE:	r SLOPE SIG	0.0247 0.0119 0.1159
FCB	CONCENTRATION	VΞ	375	DEV	TEMFERATURE:	r SLOPE	0.4341 1.2042 2.2601

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CON ELATION COEFFICIENTS

FOE STATION: SUD-S-RI

MET. STATION: MOE-77025

NUMBER OF VALID DAYS: 23

HOS CONCENTRATION VE WIND DIRECTION

	M	$N_i N_i$	NW	DIRECTION With	7.0	WEW	≘₩	3514
TLIFE • 252	-0.1342 -0.0505 -0.1335	-0.0731 -0.0277 -0.3593		-0.0150 -2.0097 -0.0739		-0.0415 -0.0377 -0.2035	-0.2562 -0.1229 -1.2985	-0.2158 -0.1020 -1.0900
	3	EEI	SE	ESE	E	ENE	NE	NNE
					_		313500	

PCE CONCENTRATION VS WIND BREED

		WIND	SPEED (KM)	(HR)	
	0 - 5	5 - 10	10 - 15	15 - 20	2.20
je.	-0.3425	-0.4082	-0.3532	5. 2445	0.5320
QLOFE	-0.0970	-0.1397	-0.1069	0.0905	C. 0935
	-1.9057	-2.1906	-1.8496	1.2352	3.0780
. SIB	70%	9E1	90%		7.712

PCB	CONSENTRATION	VS	AVES	RAGE	TEMPERATURE:	r SLOPE t SIG	0.2400 0.1913 1.2113
705	CONCENTRATION	VS	STD	DEV	TEMPERATURE:	r SLOPE t	-0.0087 -0.0453 -0.0434

- %(), TE MINI STONEST-77025 -- 2. 70 -0.2T 40°0° .×. - xO. ES ٠Ä٠ 4*0.30 7.25 -×0.45 .⊗--*O.40 4 25 -*0.35 .g**c** * ±∻0.30 4. 494 ---· -0.25 · ** 2. 뀾

START TIME: 07 VALID DAYS: 26

- 18. 4¢	****	***	·*****	(***)	****	* > * * *	美安尼亚安宁	***	·* > + + -	·*****	1145 Pr Pr Pr 1	· * * * * * *	K # # # #	****	****	***
N		NU	WNN	74	WEW		COM			335		SEE	Ξ	ENE		131
#	-8			-52		-5-	*	-*O.	<u></u> 55			*	*	*	*	
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CONTRACTION COEFFICIENTS

TOD STATION: THU-5 FG

MET. STATION: AES- TEAY

NUMBER OF VALID DAYS: IN

FIS STATEMERATION VS WIND DIRECTION

	**	1000 100 to	WIME NA	IIRECTION WNW	W	พรพ	SW	5.5.M
ILIPE t	0.0403 0.0094 0.1975	-0.0242 -0.0027 -0.1187		-0.2391 -0.0551 -1.3148	-0.5231 -0.1001 -3.007: 79%		-0.2781 -3.2703 -1.4181	0.0676 0.0420 0.3017
	£.	332	32	ZZE	Ε	ENE	NE	NNE
5.126Z	0.4745 0.2969 2.3404 95%	0.8700 0.2841 1.7518 90%	0.4168 6.1396 2.9461 95%	0.3393 5.1313 1.7669 90%	0.1710 0.0425 0.7532	0.5284 0.1818 0.0488 96%	0.1518 0.0694 0.7524	0.3323 0.0700 1.7259 90%

POB CONCENTRATION VS WIND SFEED

	0 - 5	(40.000	10 - 15		>20
r SLOPE t SIG	0.4329 0.0533 2.3518 95%	0,2115 0,0323 1,0402	-0.3900 -3.0677 -2.0750 95%	-0.3583 -0.0832 -1.8802 90%	-0.2129 -0.3427 -1.0375

FILE	CONCENTRATION	VΈ	AVERAGE	FEMFERATURE:	r	0.0257
					SLCPE	0.0140
					15	0.1262
					513	

7-13	CONCENTRATION	VΞ	STE	DEV	TEMPERATURE:	₹	-0.0042
						SLOFE	-3.0099
						T.	-0.0211
				01		RITIN	

				0.07	7FL AT	T = \!	COEFFI	DIENTS VS	WIND	DIREC	TIBN				
		MARIO.	- TD:NY					-> 1.75				STA	RT TI	:E:	0.5
		ii. 7 Fizi	=-=-					30					ID DA		26
	190	para a a seri	(A) (10) (B)					0.70							
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								* *	**	*		2%	*		
								+*0.15*	-5-		2.	×	*	*	
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								+>0.10>	3		*	*	Ť	*	
								** *	*	*	44	*	*	*	
							2.5	+*O.05*	*	*	*	**	*	*	
26							- 4	* *	斧	*	*	*	*	*	
Z 3-25	x	医医性皮肤	*****	* * * * }	****	***	. K K K K K K K	*****	84844	****	****	****	****	****	***
N P	MADA	51.1	WNIV	1.0	W8W	ΞW	8814	÷ 8	ESE	35	ESE	Ξ	ENE	NΞ	NN
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		C4.74	*												
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		*	*	* * *	*	* *		* -÷0.19 *							٠
		* *	* *	* * * *	* * * *	* * *		* -*0.10 * -*0.15							•
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		*	* * * *	* * * * * *	* * *	* * * * *		* -*0.10 * -*6.15 * -*0.20							•
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		* * * *	* * * * * * *	* * * * * * *	* * * * *	* * * * * *		* -*0.10 * -*6.15 * -*0.20							
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		经股份 医骨头 医牙头虫	* * * * * * *	* * * * * * * * * * * *	* * * * * * * * * * * * * * * * * * * *	* * * * * *		* -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 *							* ************************************
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		经股份 医骨头 医牙头虫	* * * * * * *	* * * * * * * * * * * * * * * * * * * *	* * * * * * * * * * * * * * * * * * * *	* * * * * *		* -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 *							
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		**************************************	* * * * * * *	* * * * * * * * * * * * * * * * * * * *	* * * * * * * * * * * * * * * * * * * *	* * * * * *		* -*0.10 * -*0.15 -* -*0.20 * -*0.25 * -*0.30 * -*0.95 * -*0.45							
		**************************************	* * * * * * *	*****	* * * * * * * * * * * * * * * * * * * *	* * * * * *		* -*0.10 * -*0.15 * -*0.20 * -*0.25 * -*0.30 * -*0.65 * -*0.45 *							
		**************************************	* * * * * * *	* * * * * * * * * * * * * * * * * * * *	* * * * * * * * * * * * * * * * * * * *	* * * * * *		* -*0.10 * -*0.15 -* -*0.20 * -*0.25 * -*0.30 * -*0.05 * -*0.40 * -*0.45 * -*0.50							
		**************************************	* * * * * * *	*****	* * * * * * * * * * * * * * * * * * * *	* * * * * *		* -*0.10 * -*0.15 -*0.20 * -*0.25 * -*0.30 * -*0.55 * -*0.40 * -*0.45 * -*0.50							×
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		**************************************	* * * * * * *	*****	* * * * * * * * * * * * * * * * * * * *	* * * * * *	,	* -*0.10 * -*0.15 -*0.20 * -*0.25 * -*0.30 * -*0.55 * -*0.40 * -*0.45 * -*0.50							· X
		**************************************	* * * * * * *	*****	* * * * * * * * * * * * * * * * * * * *	* * * * * *	,	* -*0.10 * -*0.15 -*0.20 * -*0.25 * -*0.30 * -*0.95 * -*0.45 * -*0.45 * -*0.50 * -*0.55							* X
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--0.65 *

--0.70 ---0.75

The section descriptions

PER STRIBUTE THE FIRST

BET. STATETM: BES- TEAM

NUMBER OF WALLE BOYS: 27

THE DEMORPHRATION WE WIND DIRECTION

	(wide) 19-10	T BELLA TO K. Brown 186	5 H	DESTRUCTION	48	West	MARK K STARK	
51.785 *	0.3078 0.1077 1.6281	-1.6784 -0.0156 -1.3734	-0.01186 -0.1267 2.1091	-3.8173 3.1039 -1.0498 7.54	-0.0007 -0.1657 -0.6019 75%	-1. 2217 -0. 1272 -0. 1749	-0.0303 -0.0364 -0.1651	6.2053 0.3348 1.0483
	2	医曼因	EE	Les and the second	Ξ	ENE	Ξ.:	1/1/20
ore ore	0.4027 6.3732 3.3361 75%	0.2071 0.2917 1.5101	7. 1.72 1. 1511 1. 1111	6.2400 6.1078 1.2340	0.0511 0.0302 0.1065	0.30 4 4 0.1339 1.733	0.3747 0.3005 0.007 73%	0.2421 c.0649 t.2477

FOR TOUCHTRATION VS WIND SPEED

		11111	EREZE (KM)	(RR)	
	G - 5	5 - 10	10 - 15	:5 - 20	3.20
2 to 1	0.4799	-1.0227	-0.4141	-1.2086	-0.0101
	0.1001	.o. 0952	-0.1185	-0.1244	-0.0059
* t	2.7270	-1,1137	-2.2740	-1,5071	-0.0904
813	95%		7 - 10		

FCD	CONCENTRATION	VE.	AVER	RAGE	TEMPERATURE:	919 919	0.3449 3.9767 1.9533 96%
PIE	CONCENTRATION	7/8	STE	DEV	TEMPERATURE.		0.1211 0.3544 0.4097

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				23		10.0			5 0.3	MINI	DIRE	TION				
	27	11 4.23	- 717	1				5,	TE				STA	ST TI	MF.	10
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		NK	ADU.	1.3	W35	ΞW	EEW			EEE				ENE	NΞ	M
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DAR BY ANDEN COEFFEDIENTS

POB STATION: TOR-5-01

MET. STATION: MSE-SSSSS

NUMBER OF VALID DAYS: 25

FOR COMPONIESTION WE WIND DIRECTION

	N	* 150.1	V. I I	DIRECTION		1, 10m, 1 1, 10m, 11	SW	SEM
SLOPE • SIG	0.5794 0.2727 2.2581 87%	0.4280 0.1924 2.1703 EX	0.3632 0.2494 1.9146 90%	-0.0724 -0.0416 -0.3329	-0.0075 -0.0013 -0.0092	0.5295 0.2395 2.7031 95%	0,1704 0,1239 0,7027	0.2720 0.1105 1.4031
	Comp.	FBE	SE	EEE	豆	三九二	KE	NNE
91075 t 518	0.1021 1.0332 3.4701	0.1051 -0.0251 -0.4840		-0.4061 -0.1011 -2.0207 75%	-0.1750 -0.0744 -0.0147	- 3. 1572 -0. 0477 -0. 8/14	-0.1701 -0.0327 -0.8220	5.6504 6.6214 6.2311

POS DINGENTRATIEN VS KIND DPEED

			SEELD (KW.)		
14	· - 5	5 - 10	10 - 15	1T - 20	120
ş	0.3130	4,0217	-0.1559	-0.2261	-1.1774
TLIFE	0.0410	-0.0037		-0.0497	-0,0702
• 5	1.5100	1.0773	-0.7239	-1.0000	-0.7237

775	CONDENTRATION		AVER	ASE	TEMPERATURE:	016 1716 1716 1816	0.3371 0.1974 1.6520
PCB	CONCENTRATION	125	STI	DEV	TEMPERATURE:	r SLOPE t	0.0233 0.1094 0.1137

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		THE STATE OF THE S	[18. 2] - [2.1] [2.1] [2.1] [2.1] [2.1] [2.1] [2.1]

START TIME: ATCHE STAUNTT-55003 F DE STAUTE -0-81 ---O. <u>--</u>-~ 80.80 440. SE -40.50 2 34 ---O.4E 100 er. Sta +>0.40 44-34 42 -~0.85 4 25 -×0.30 10 2. *39 3----0.27 5 35 14 -12-4 8. Series. 1.00 -*O.20 100 * * 2 2 -×0.15 2 4 4. 2. -24 * * -22 , 4 -54 -÷0.10* 44 4 . 4 -34 24 +40.05* * * * * * 8. 8 44 540 e de

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							43-		*	*	3	*	20	
							-×0.20		75-	12				-
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CERULATION COEFFICIENTS

POR CRATION: TOP-6-01

MET. STATION: MOE-SECO

MUNEER OF VALID DAYS: 25

* POR DINCENTRATION WE WIND LIRECTION

	N	N.S.W.	MINT NO		Ŵ	WSW	(Ξ:/∞)	BEW
# 81.075 * \$IG	0.1983 0.2159 0.9701	0, 1952 0, 2033 0, 9544	0.4853 0.3979 2.6638 95%	6.0277 0.3143 2.3350 95%	0,1239 0,0659 0,5984	0.8509 0.4038 1.7971 90%	-0.0417 -0.0478 -0.2000	0.4360 0.3776 2.3234 95%
	5	33E	ΞΞ	ESE	Ξ	ENZ	A. F. Com. F. V. Same	NE
21252	-0.0578 -0.0419	-0.2679 -0.1471	-0.3805 -0.2783	-0.2770 -0.1800	~0.0070 -0.0032	-0.1297	-0.2752 -0.1173	0.0204 0.0199

FOR CONCENTRATION WE WIND SPEED

		MIND	SPEEL (KY/	(-IF-)	
	? - E	5 - 10	10 - 15	15 - 20	>20
ş [®]	C. E177		-C. 2795	- 1. 2325	-0.3187
SLIFE			N. Z141		
	2.9011	-0.0051	-1.9349	-1.6907	-1.55
E I G	5°774		デクル		

PCD	CONCENTRATIO	WS	AVERAGE	TEMPERATURE:		0.3219 0.4245 1.6273
₽C∃	CONCENTRATION	VS	SID DEV	TEMPERATURES	r 3LOPE 3	-0.1267 -1.3504 -0.7136

															•
					^-		COEFFC	11177 5 11	WIND	DIRE	ITE DAI				
			1010	-	A-17			79. 7E					ART TI		11
		CITOR-	E-11										10 DF	YΞ:	
								7.75							
								0.45							
								2.4 (=1.2)							
								5, 4.0							

		-84						+÷0.50							
		79						-×0.45							
		4	45				4	4							
			2				45	40							-
		-31	*				***	4							
		-12-	-:-		7		+	3E							
		4"	*		*		-24	S = %							-
		48	*		*		** &								
		24	45				3	4×5. 35							
		410	*		4		-3-	3							
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	*	4-	*				25.	÷.							
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	45	**	*		*		4-	* * * ^							
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COMPLATING COEFFICIENTS

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MET. STATION: MOD-1203%

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POP CONCENTRATION VE WIND SIRECTION

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	₹.	335	SE	ESE	Ε	ENE	NE	NNE
SLOPE	0.0054 0.0010 0.0239	-0.2850 -0.0433 -1.4833	-0.2889 -0.0750 -1.5090	-0.1910 -0.0518 -3.8203	-0.0759 -0.0299 -3.3799	-0.0729 -0.0245 -0.3652	0.0330 0.0077 0.1901	-0.0943 -0.0266 -0.4738

PCD CONCENTRATION VS WIND SPEED

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310	0.5%		92%	95%	

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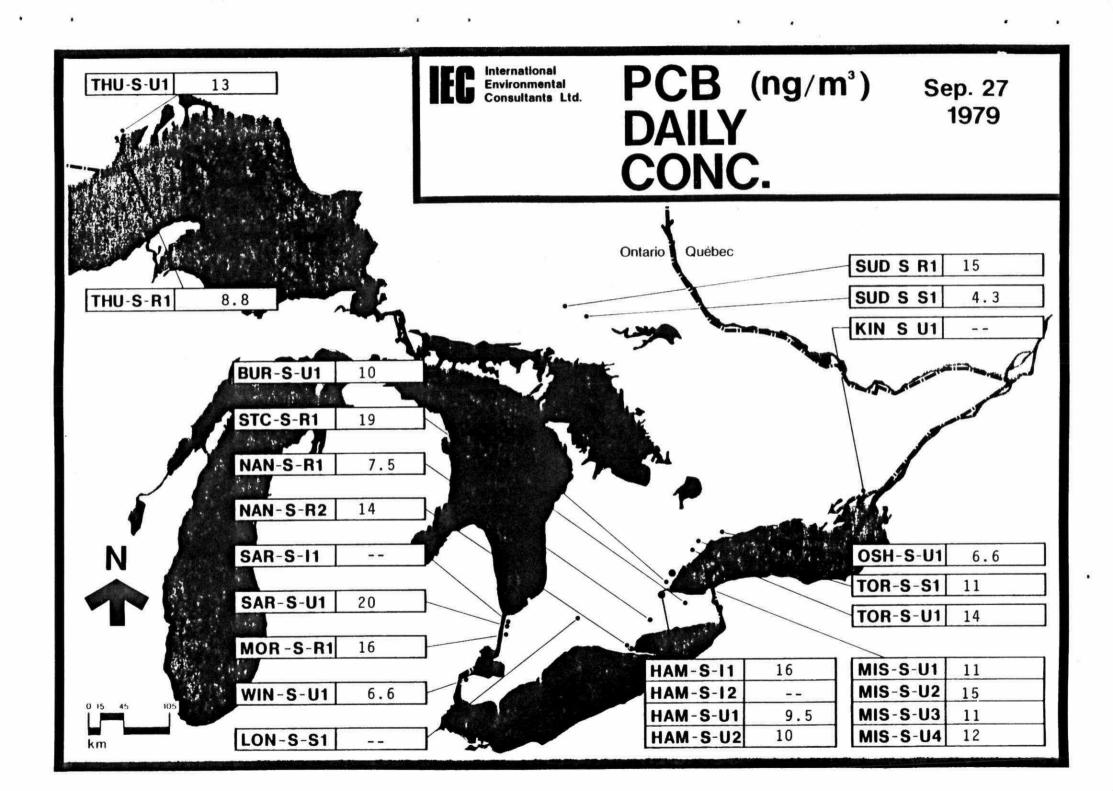
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						ELDEE	0.0070
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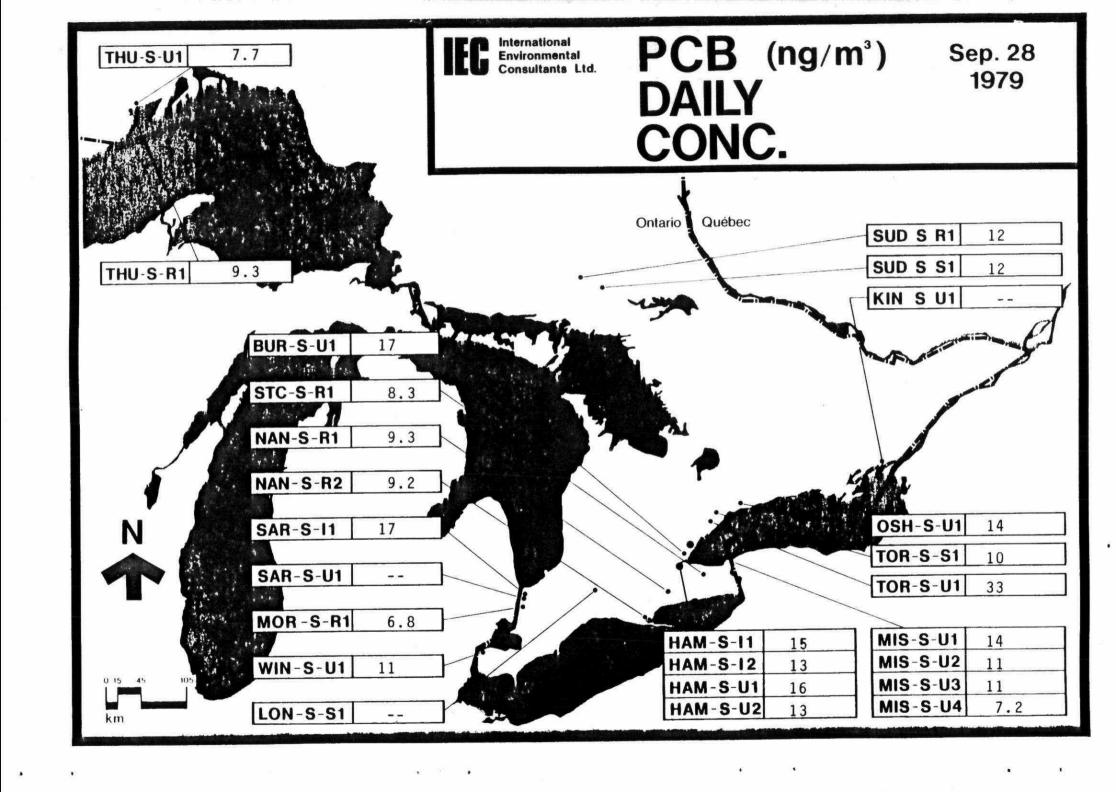
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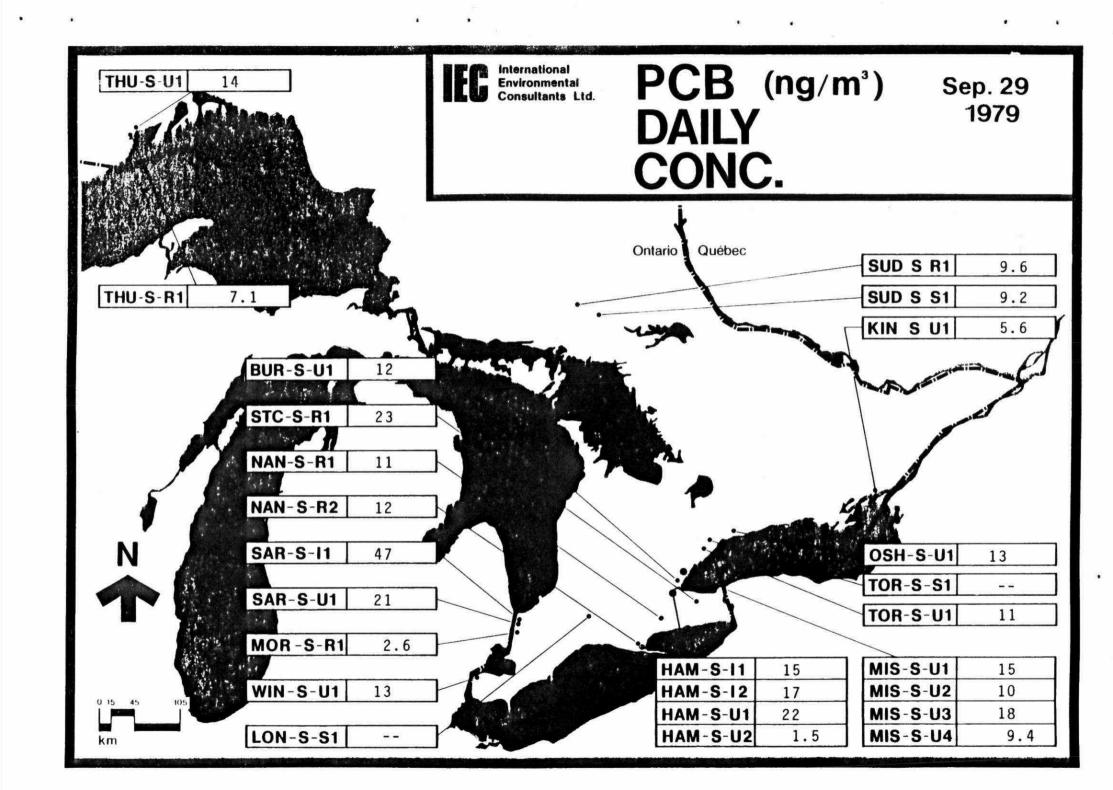
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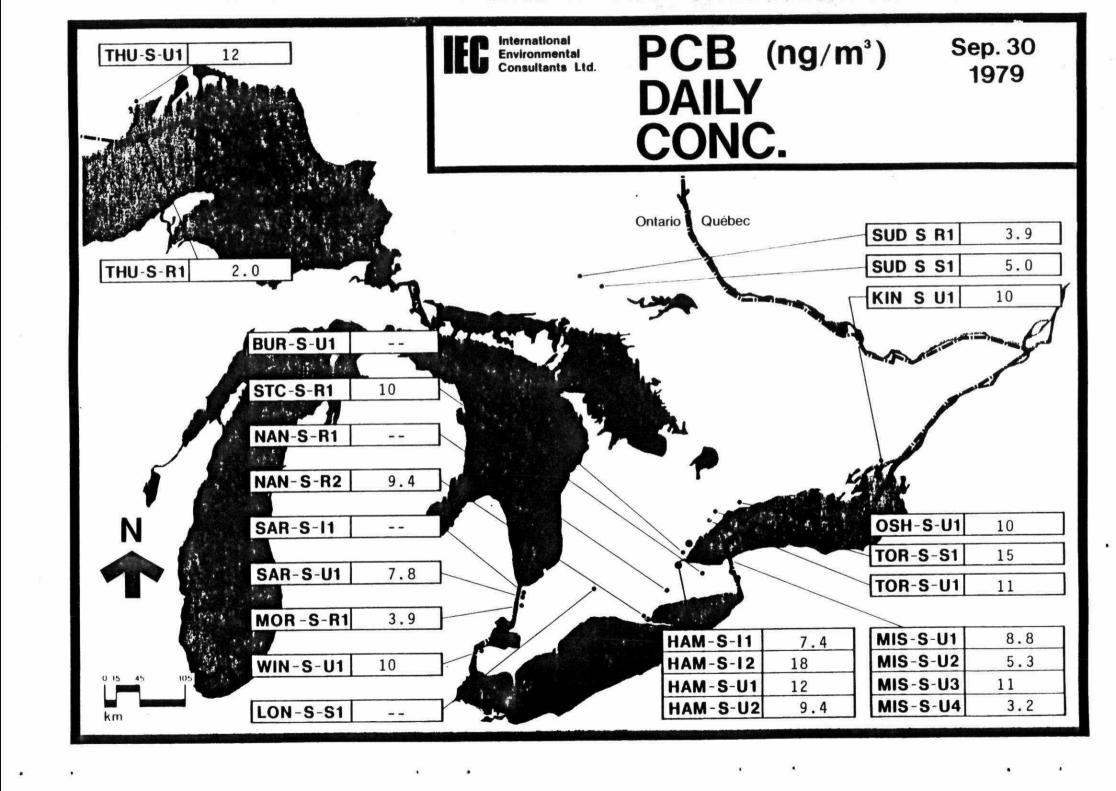
APPENDIX 4

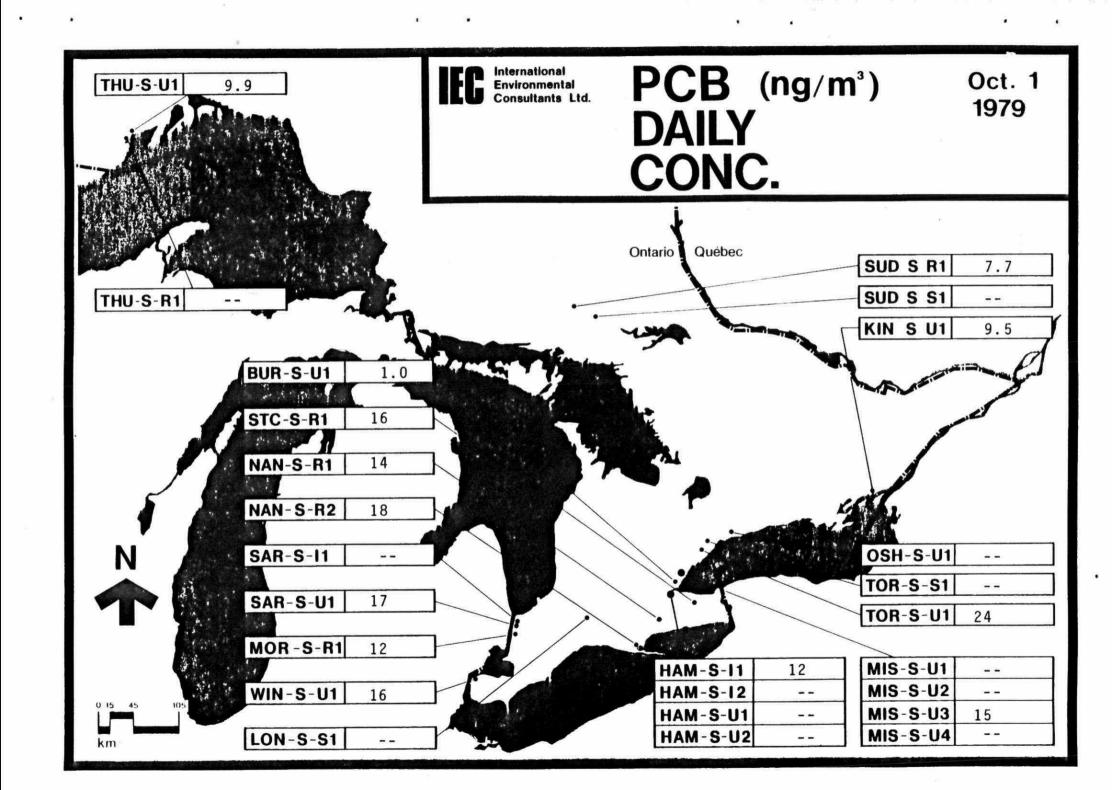
MAPS OF DAILY PCB CONCENTRATIONS

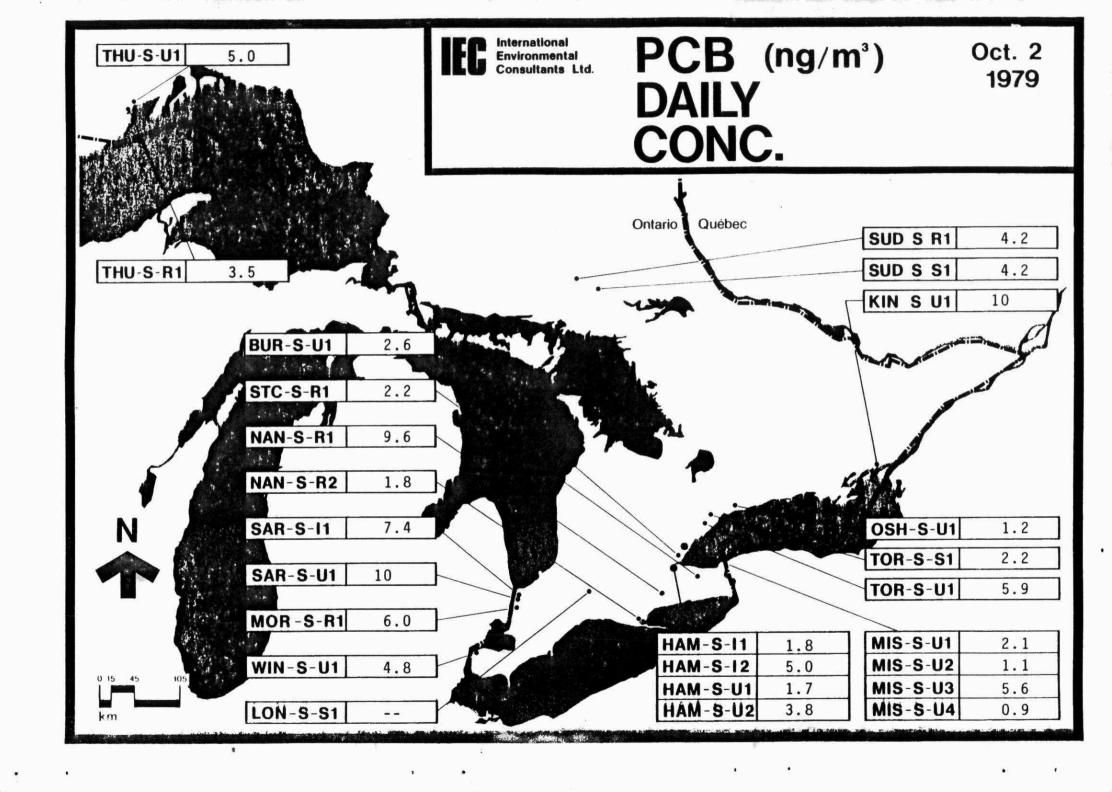


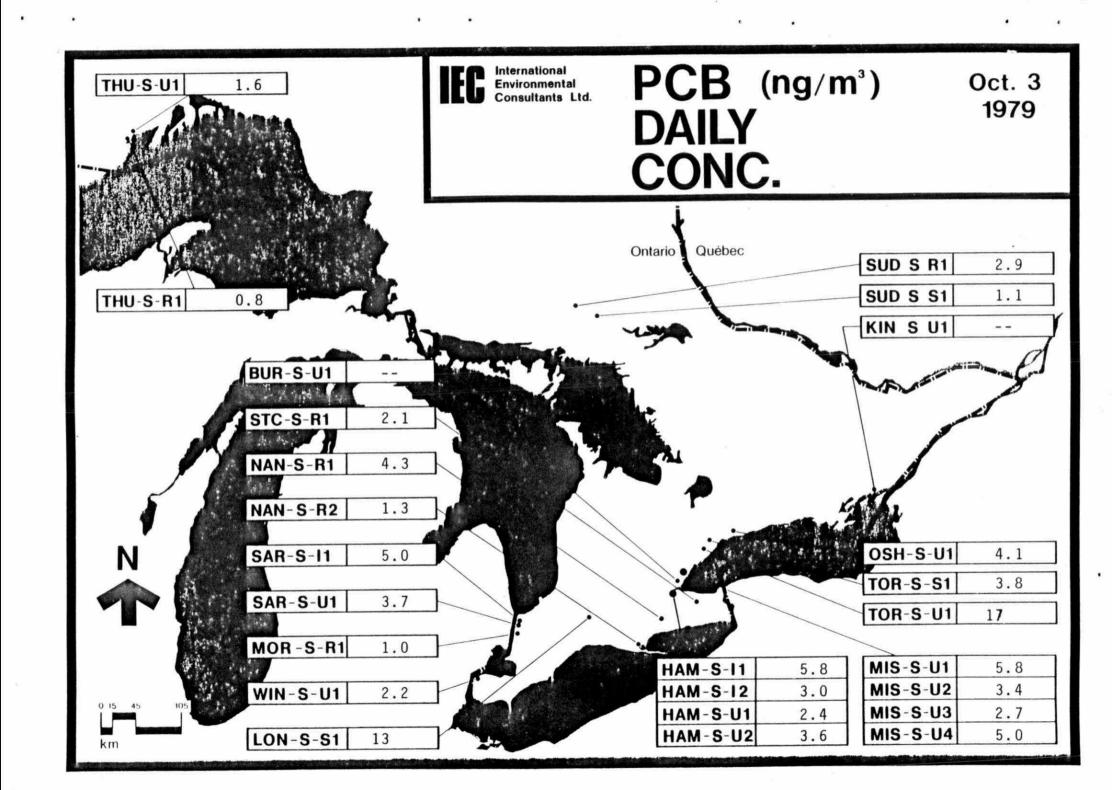


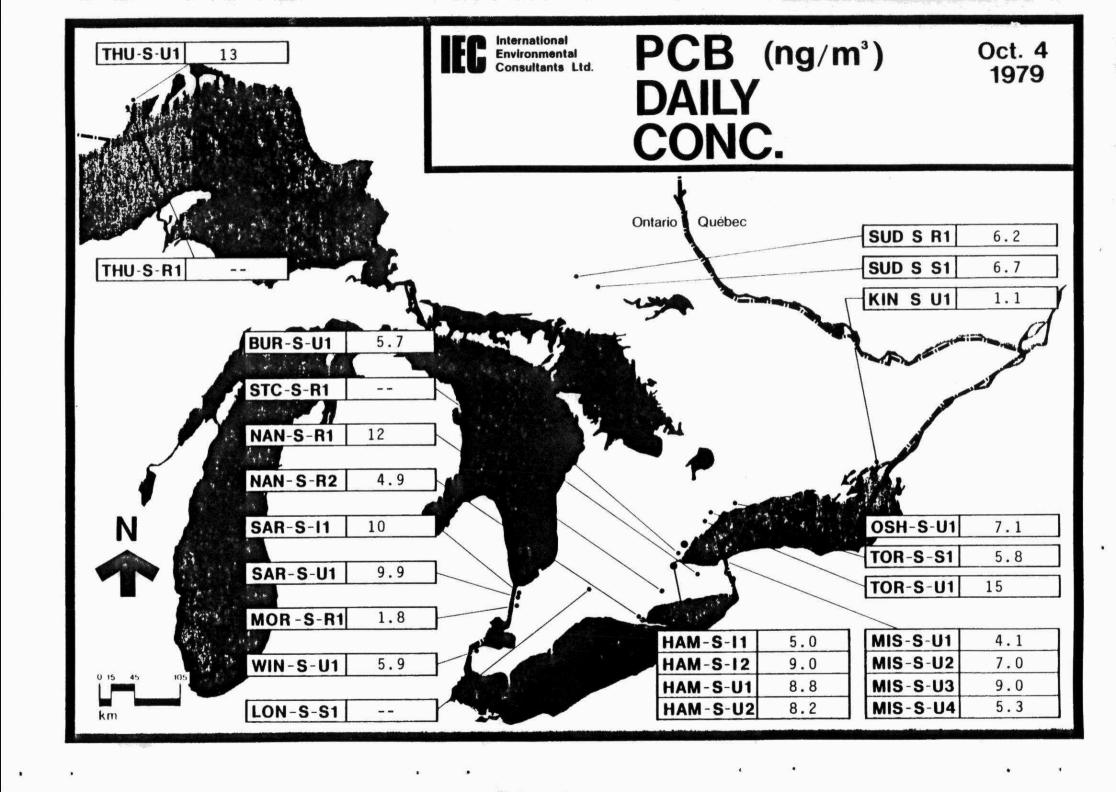


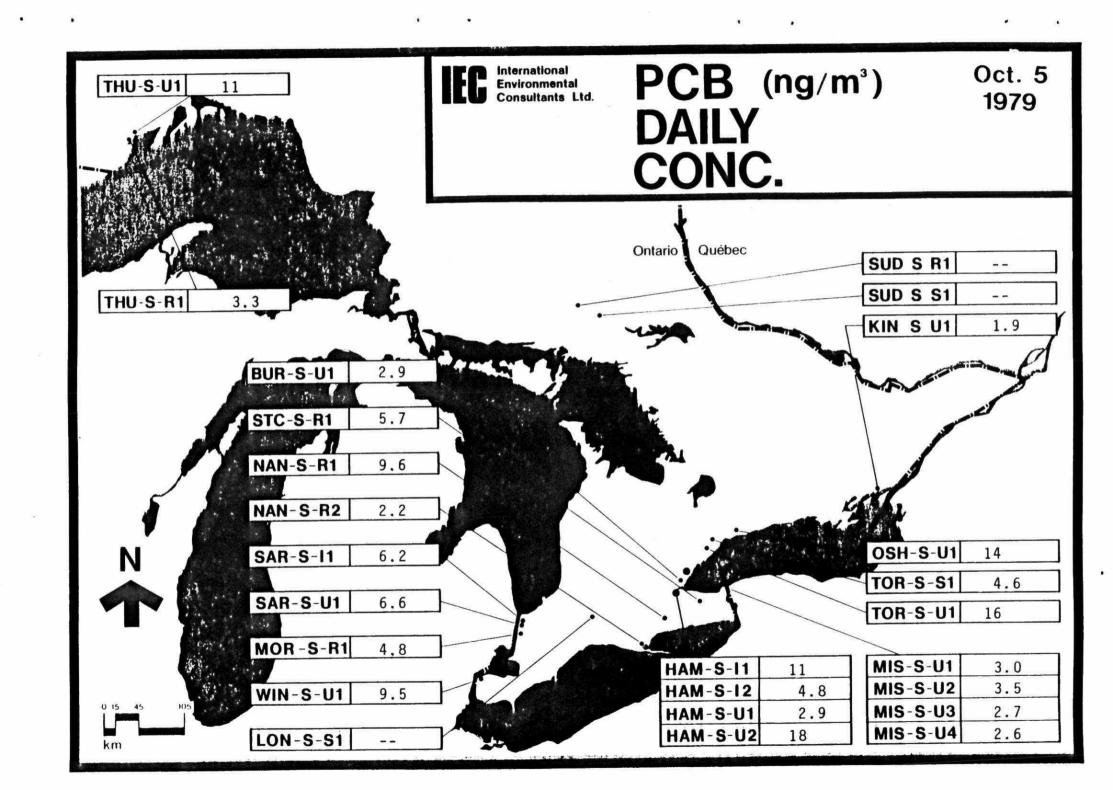


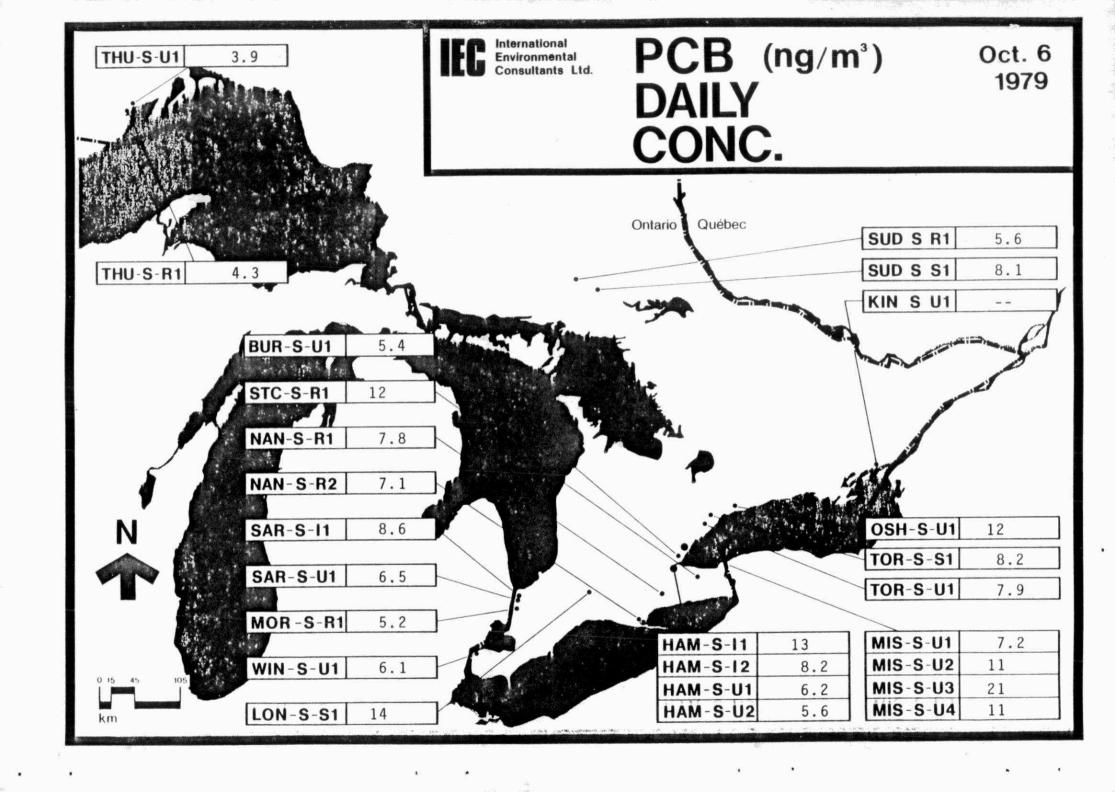


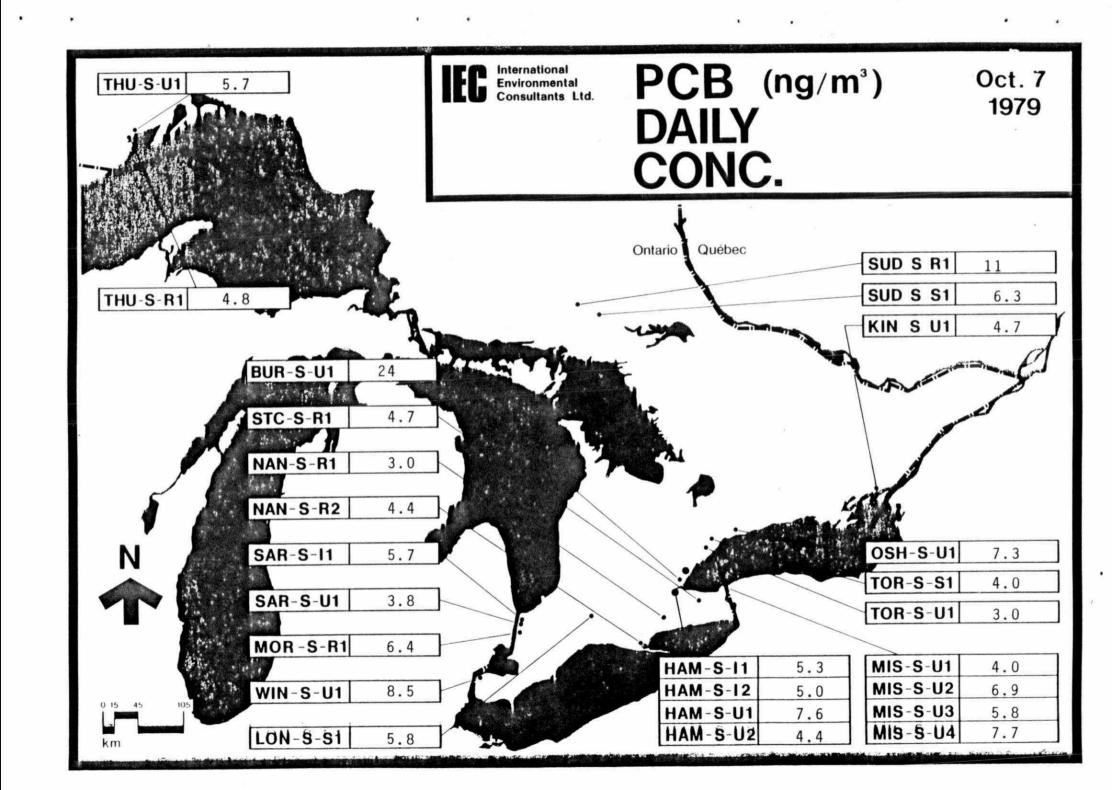


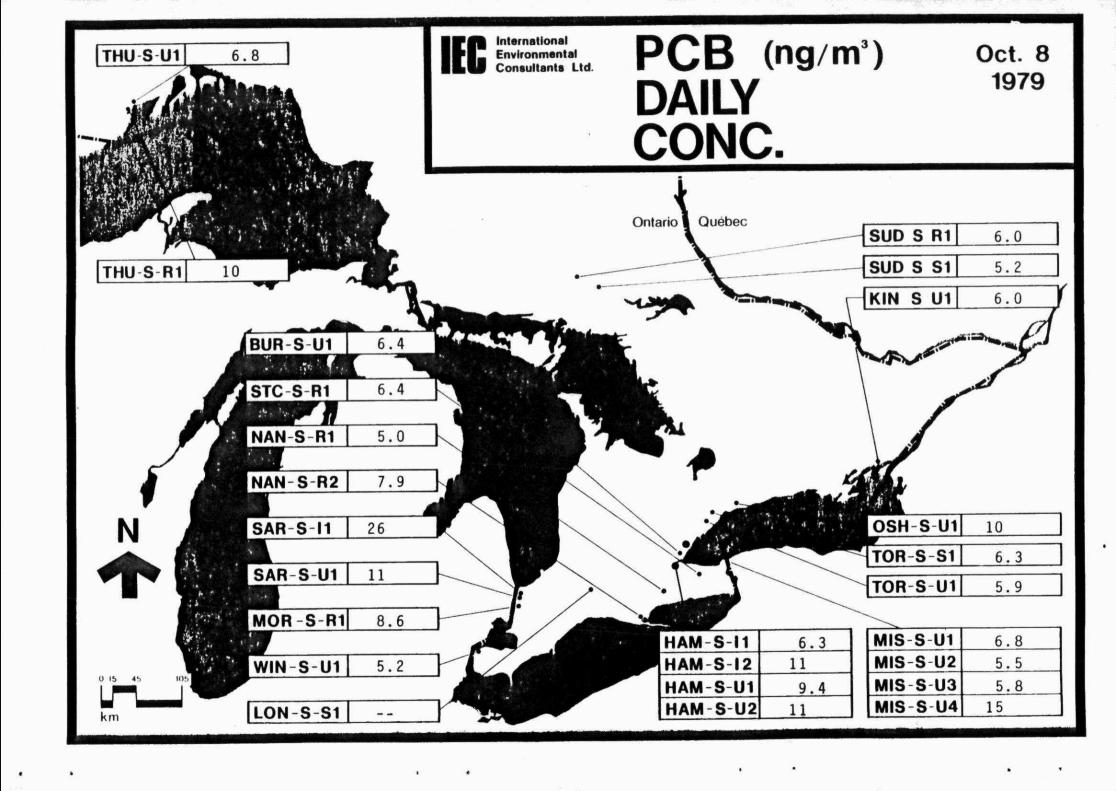


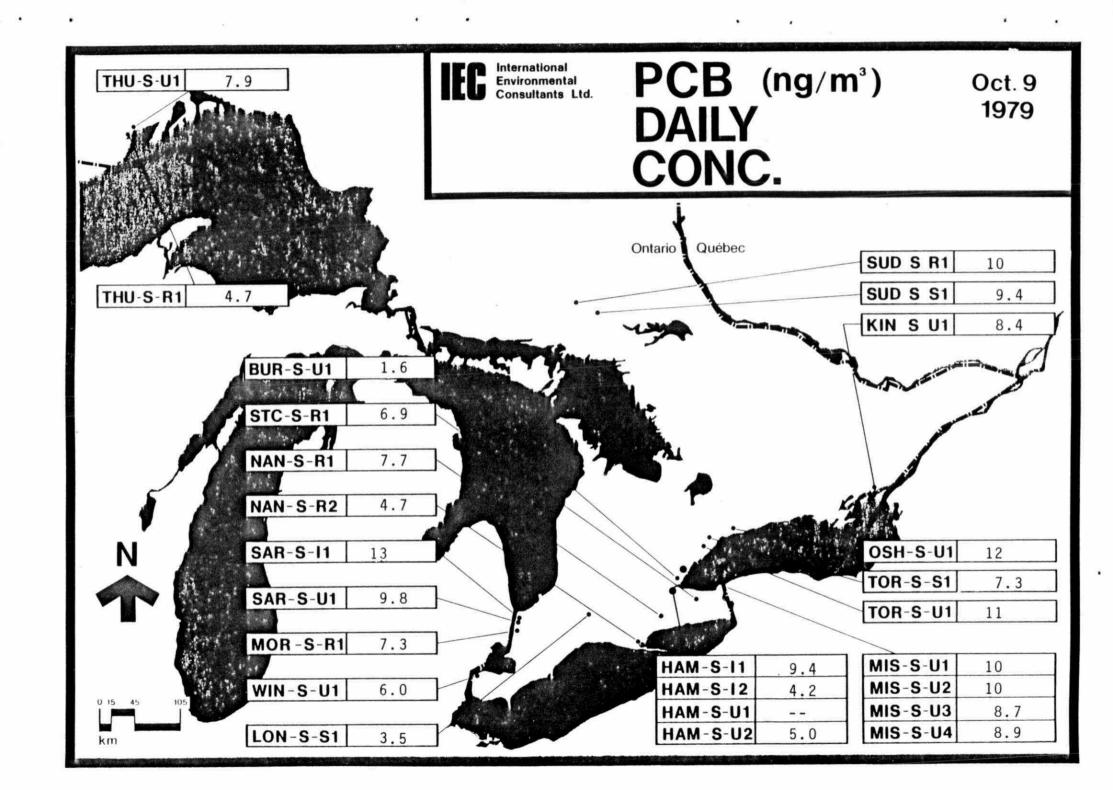


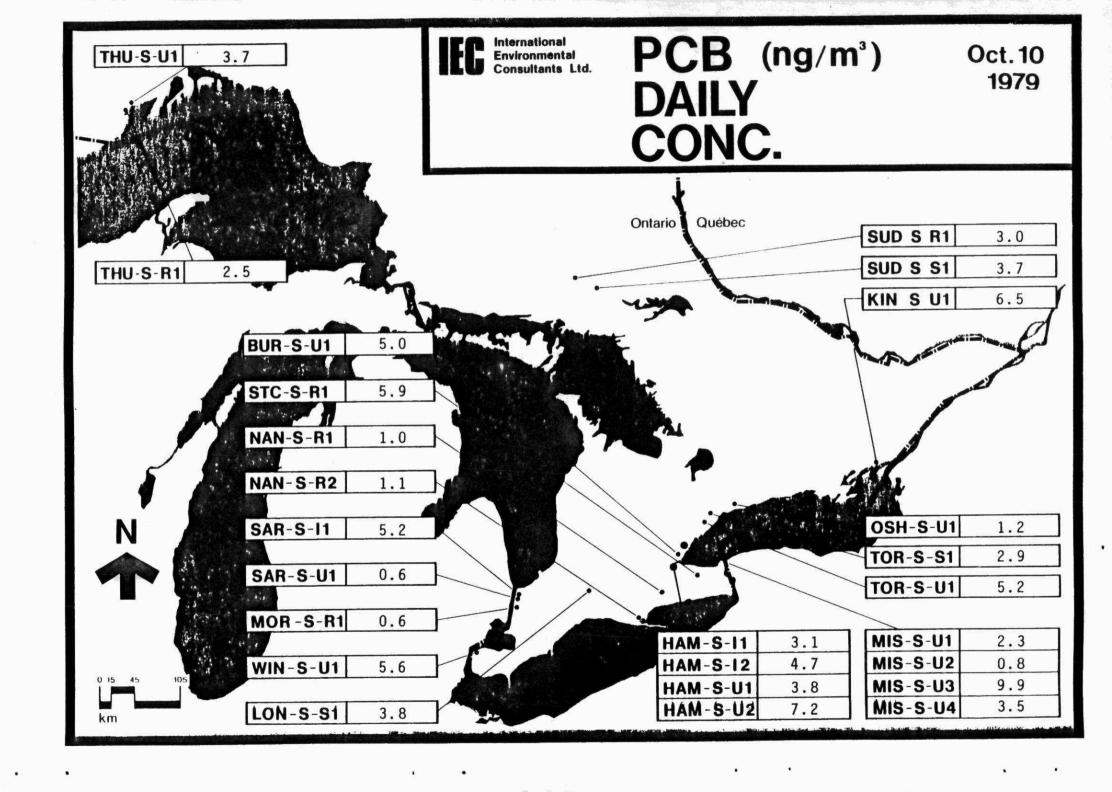


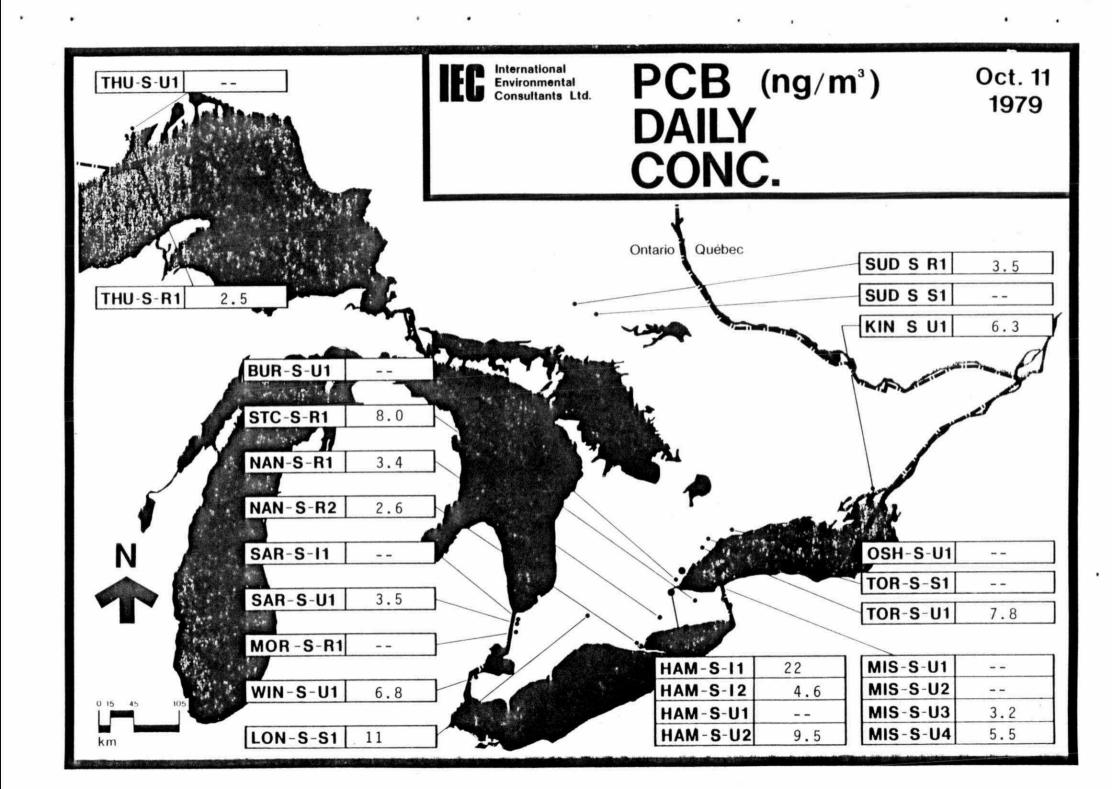


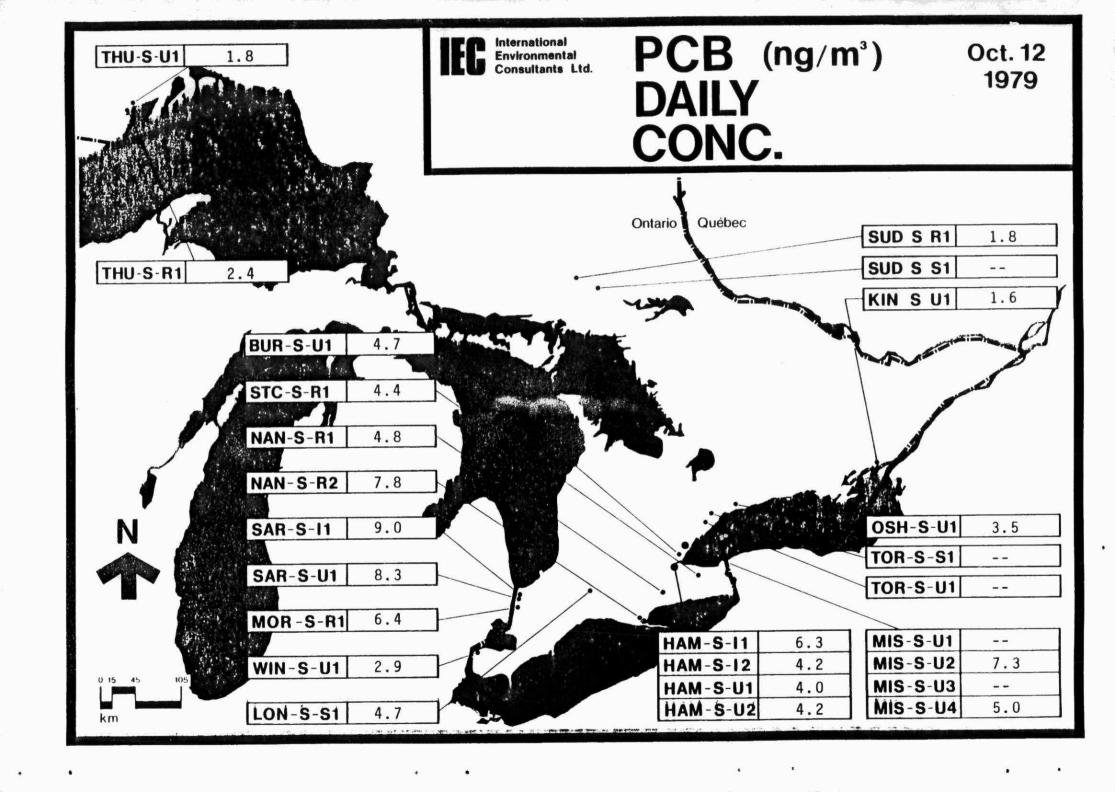


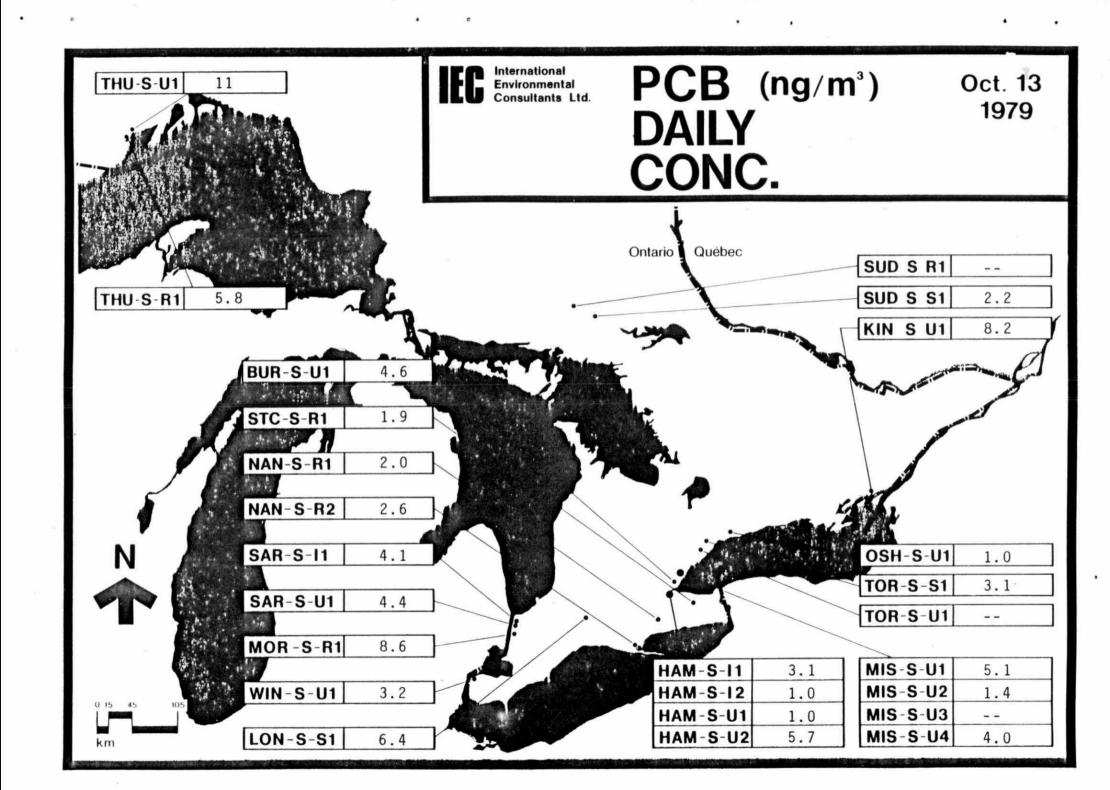


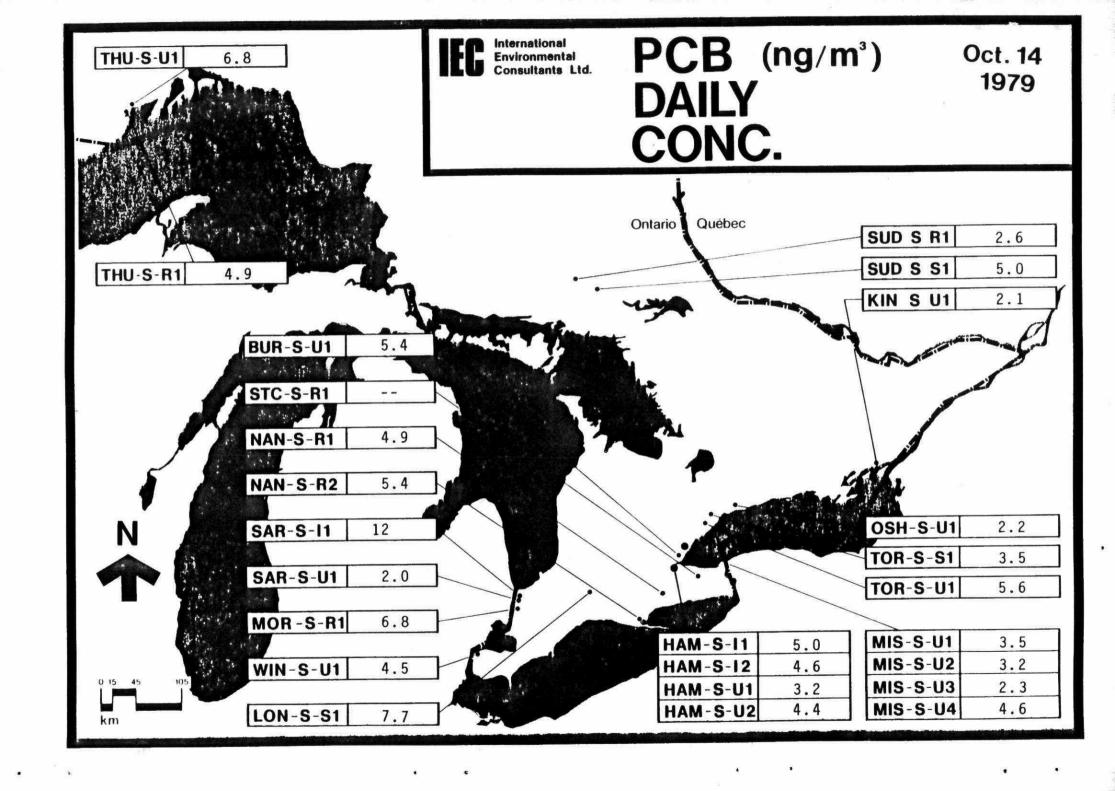


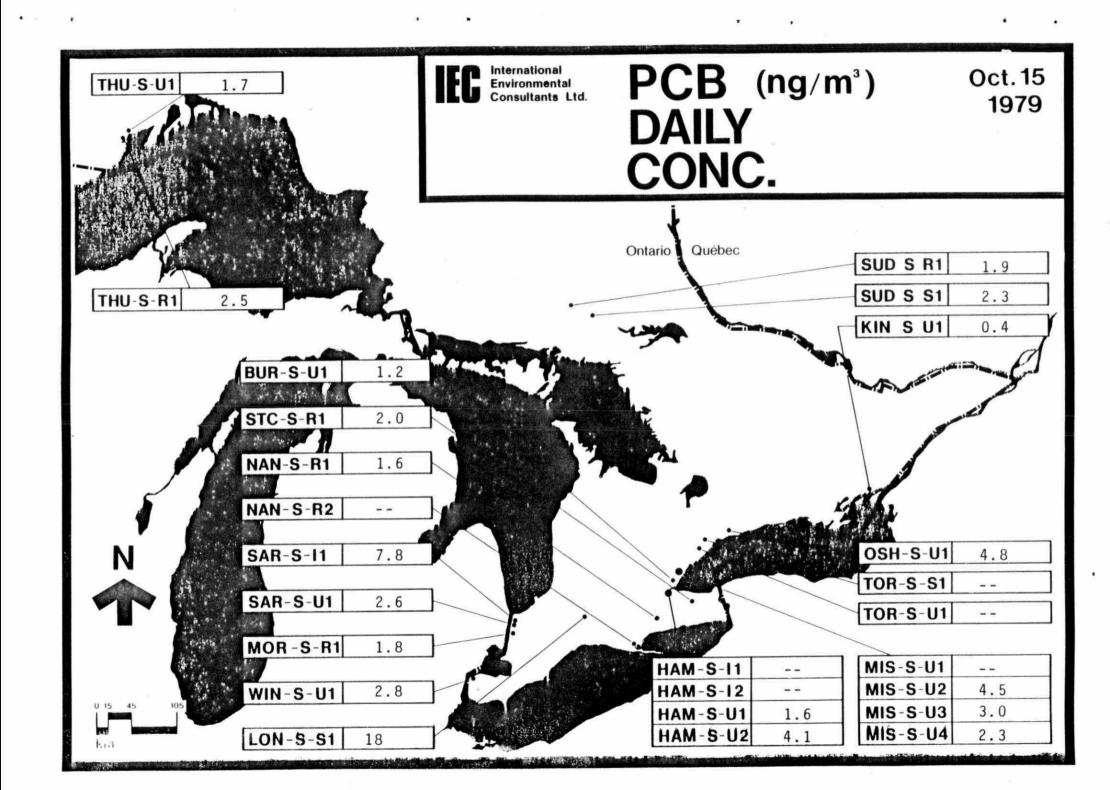


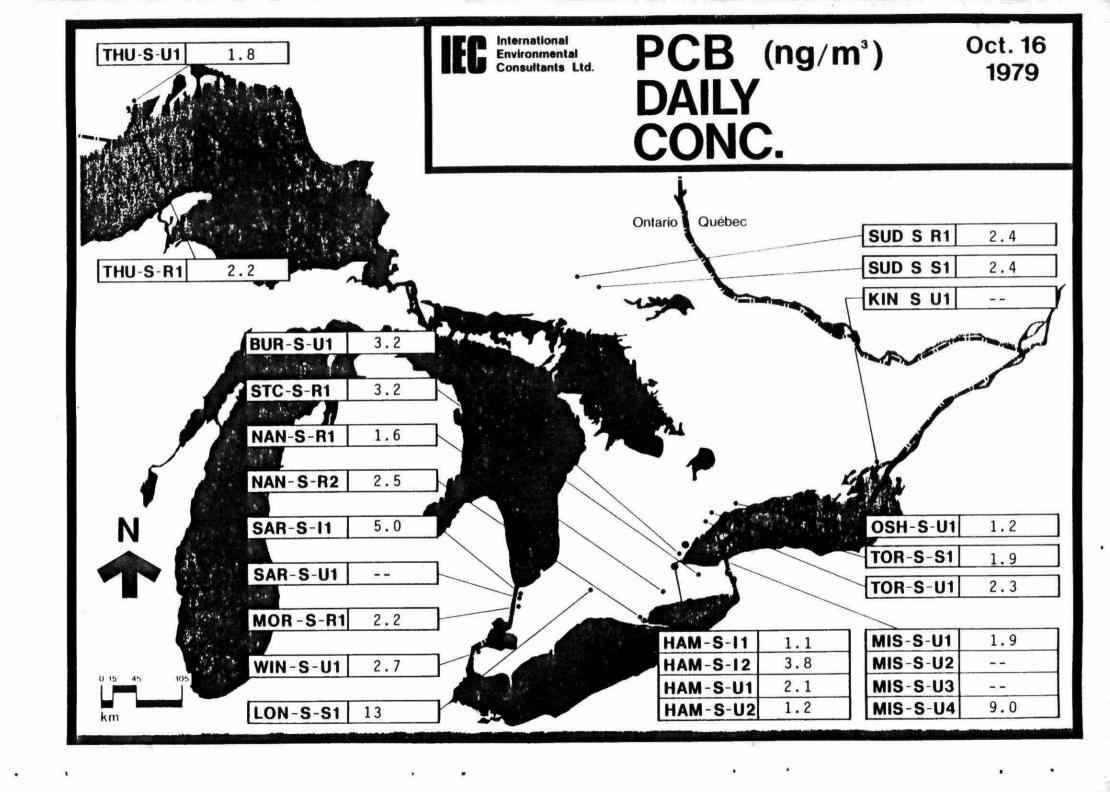


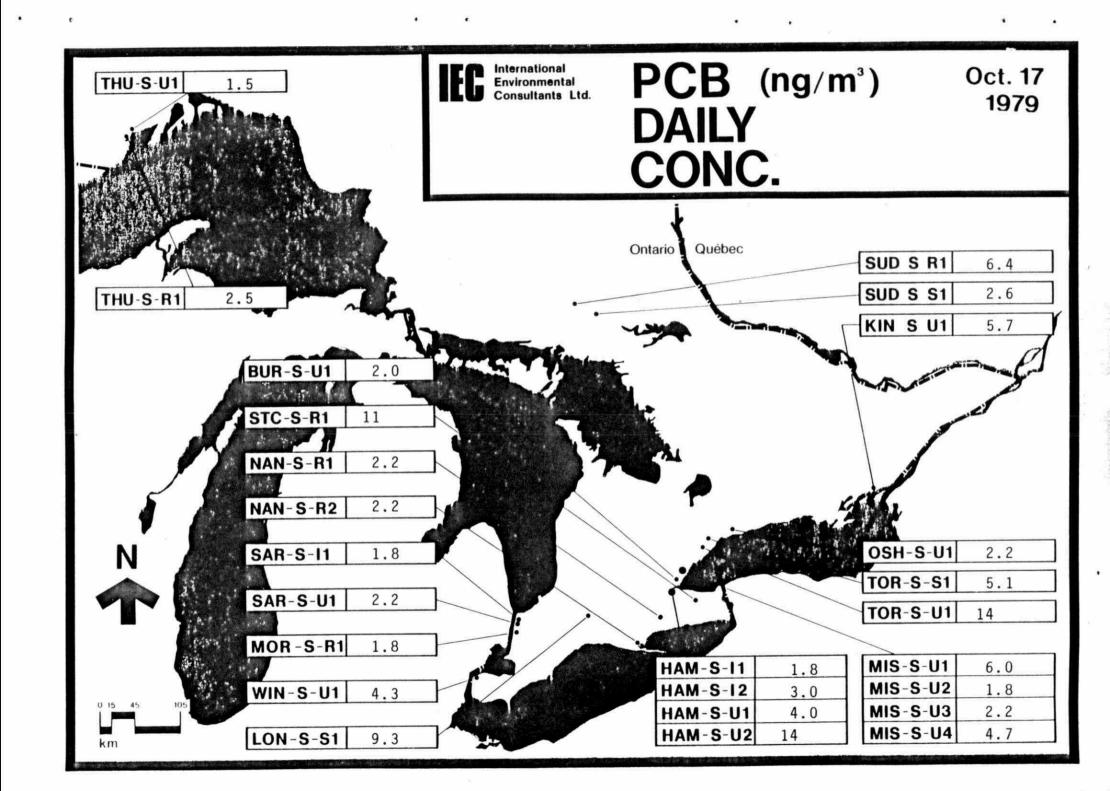


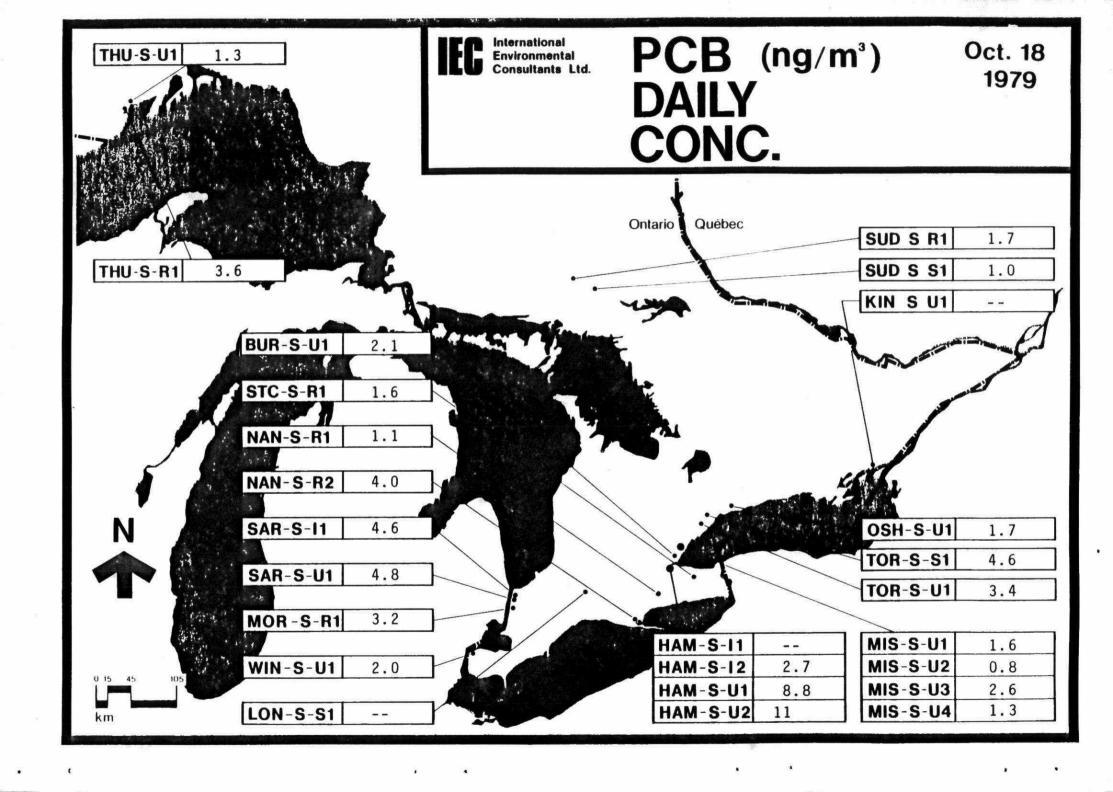


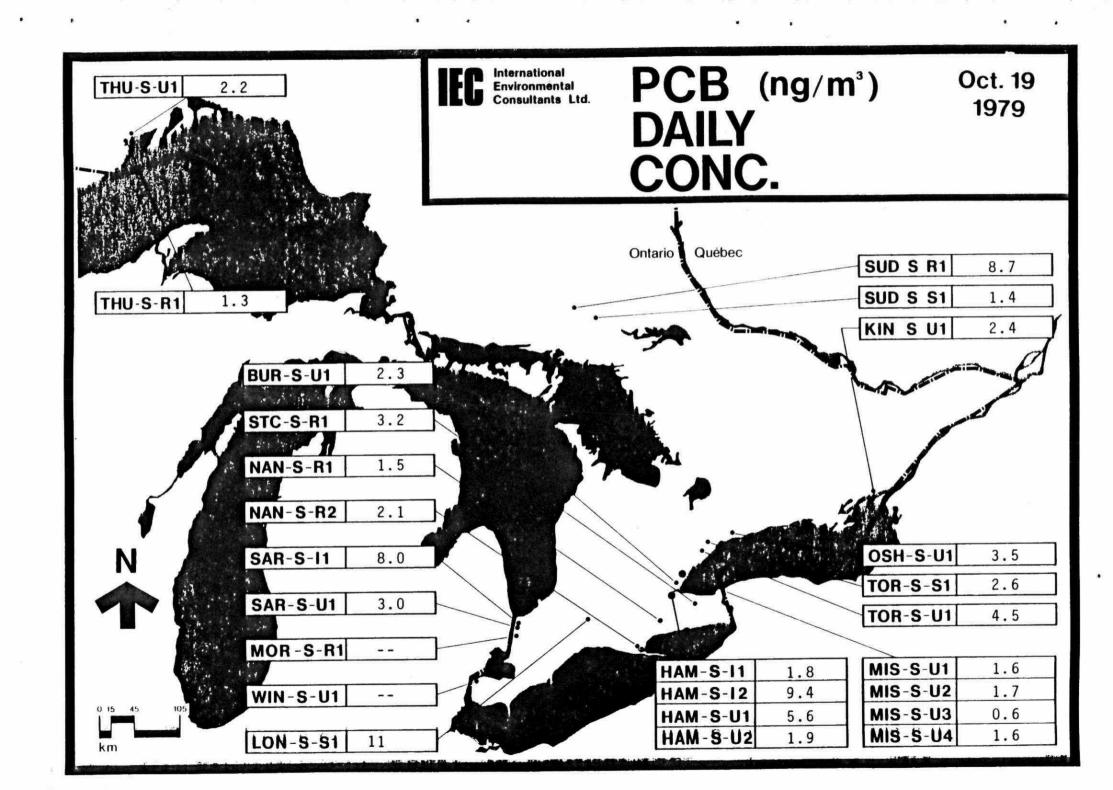


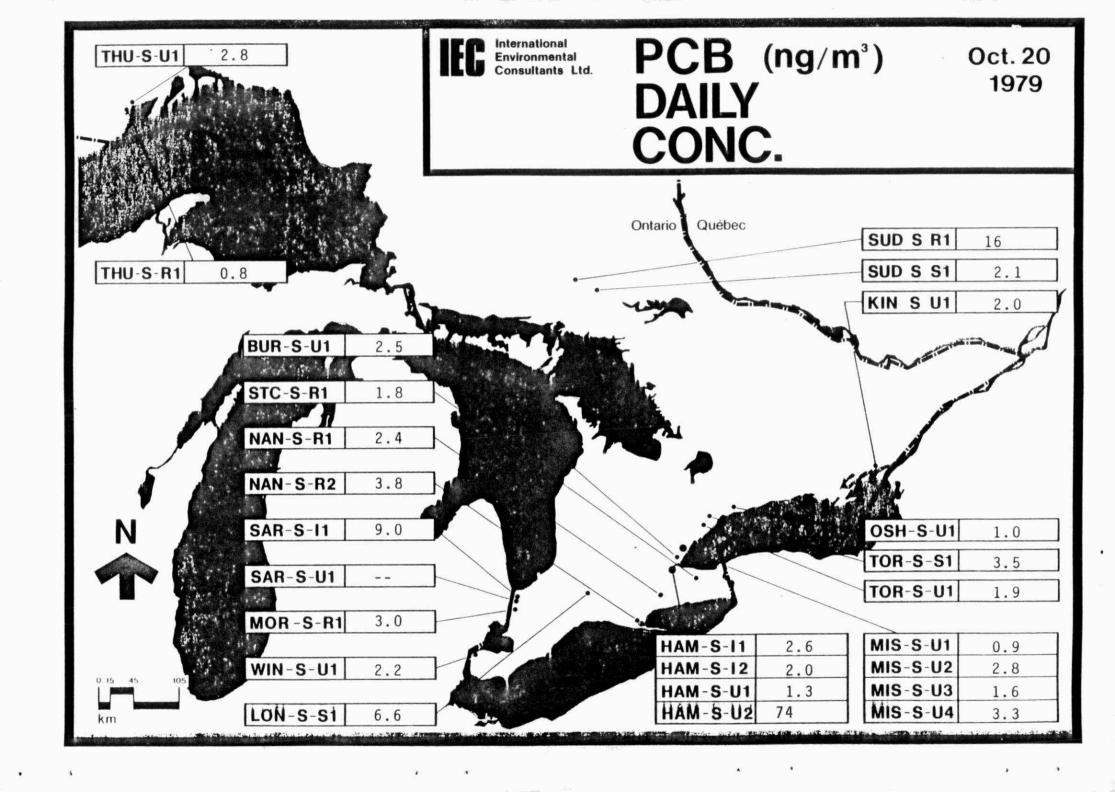


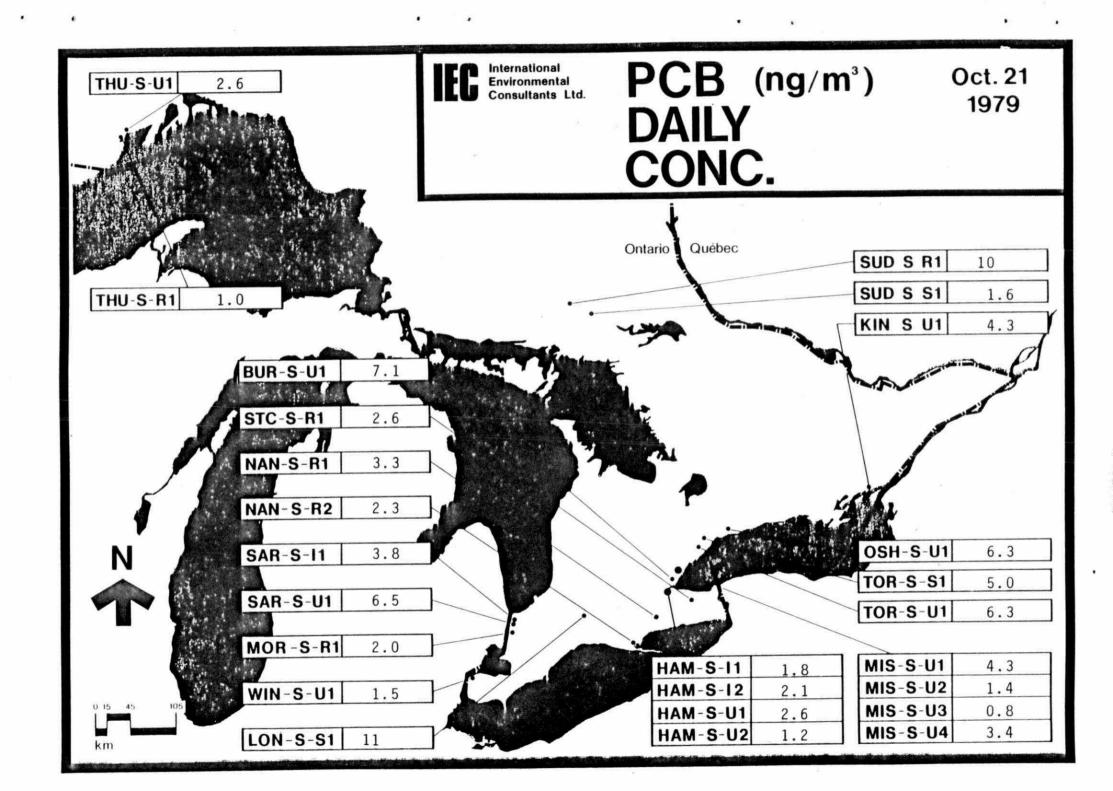


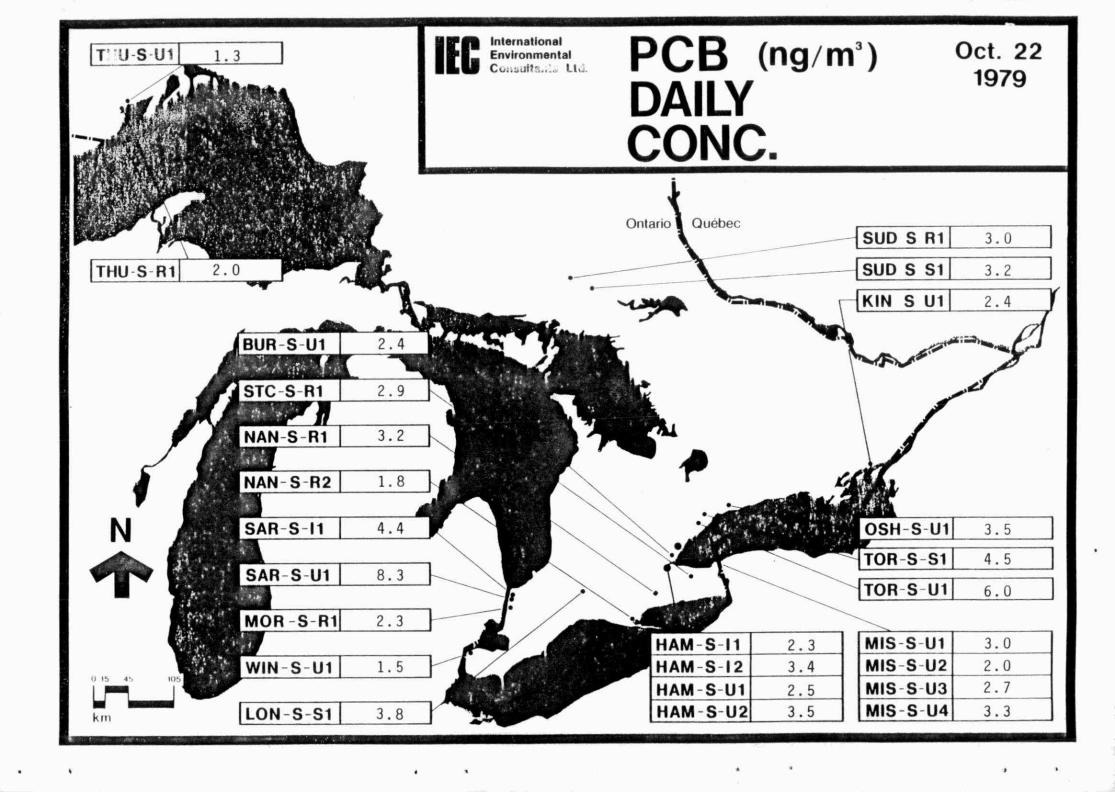


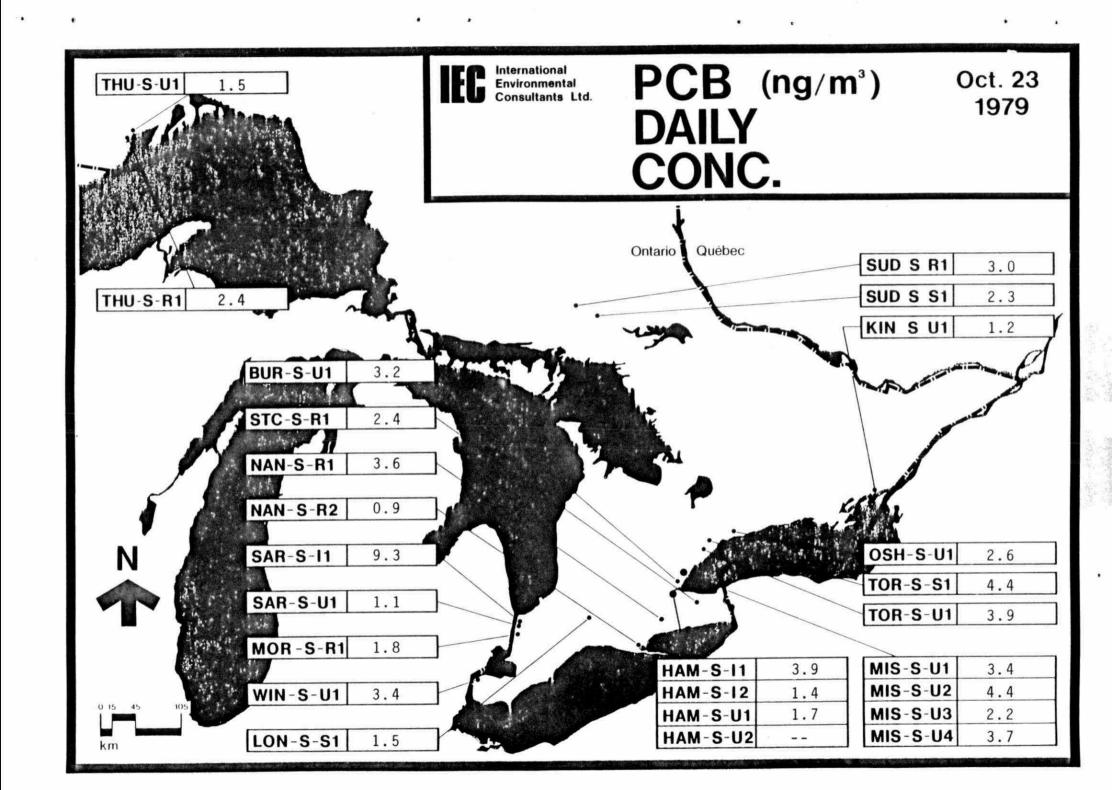


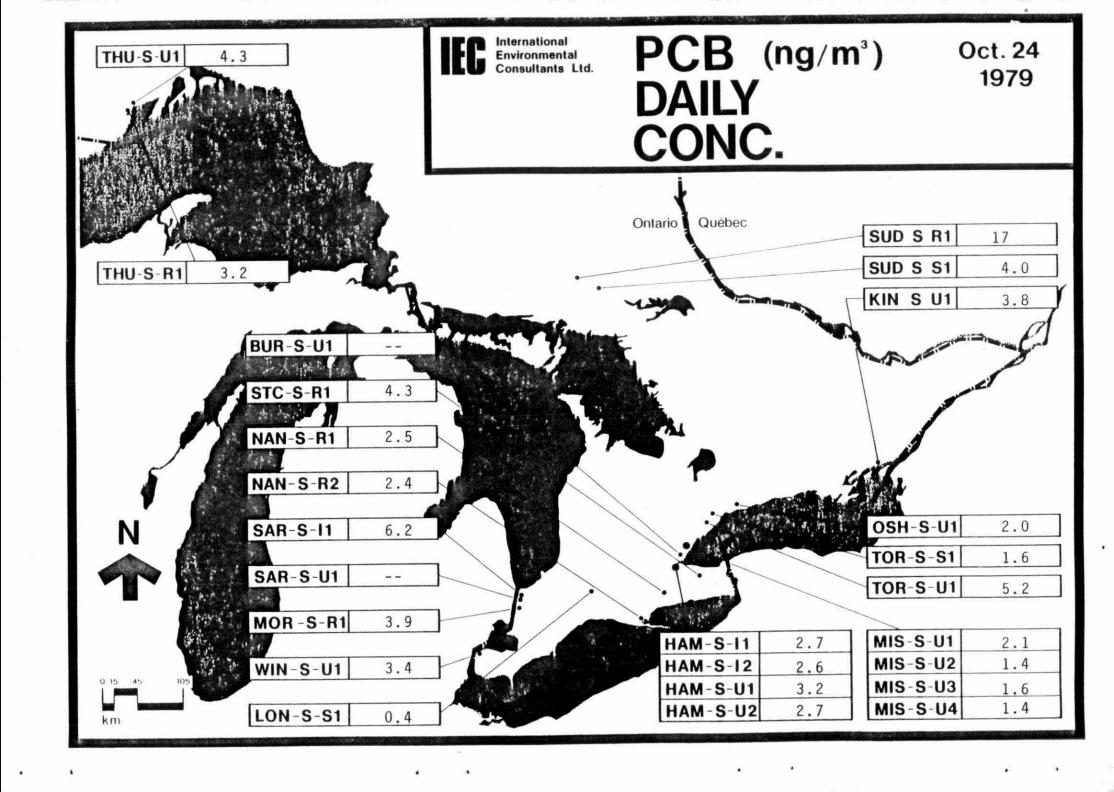










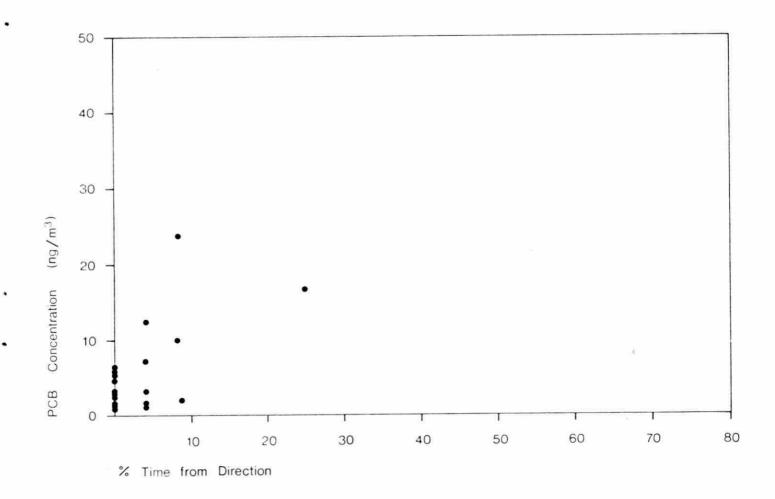


APPENDIX 5

PLOTS OF SIGNIFICANT CORRELATIONS

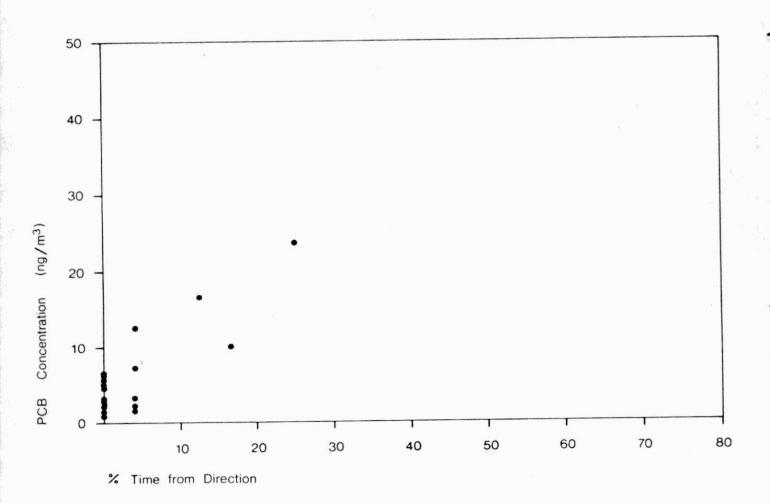
PCB Concentration vs Wind Direction Class

Station BUR-S-U1
Direction W



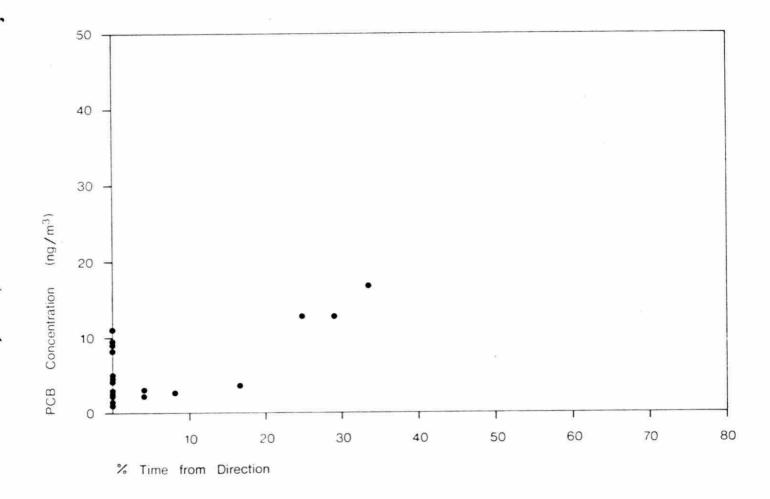


Station BUR-S-U1
Direction WSW



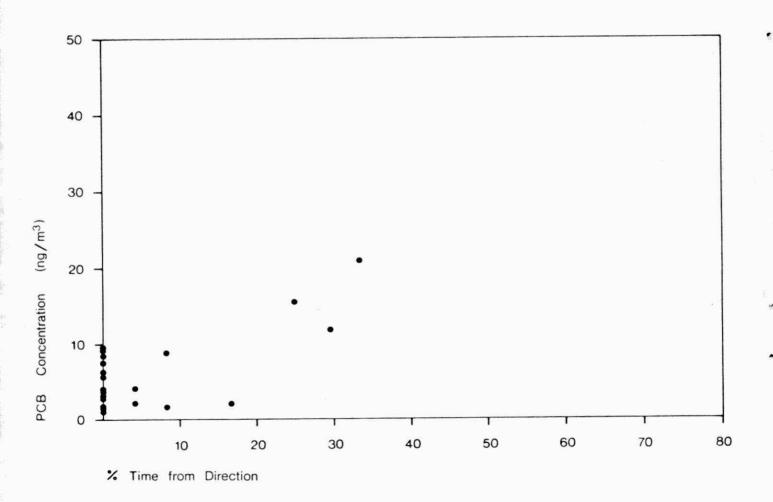


Station HAM-S-I2
Direction N



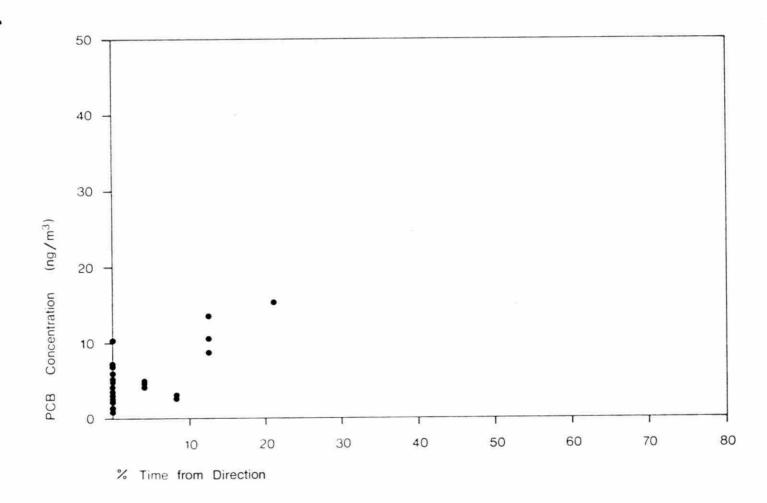


Station HAM-S-U1 Direction N



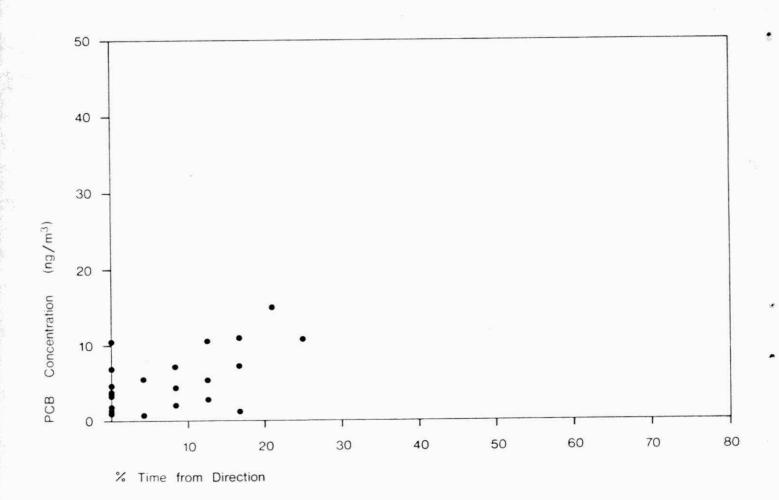


Station MIS-S-U1
Direction SSW



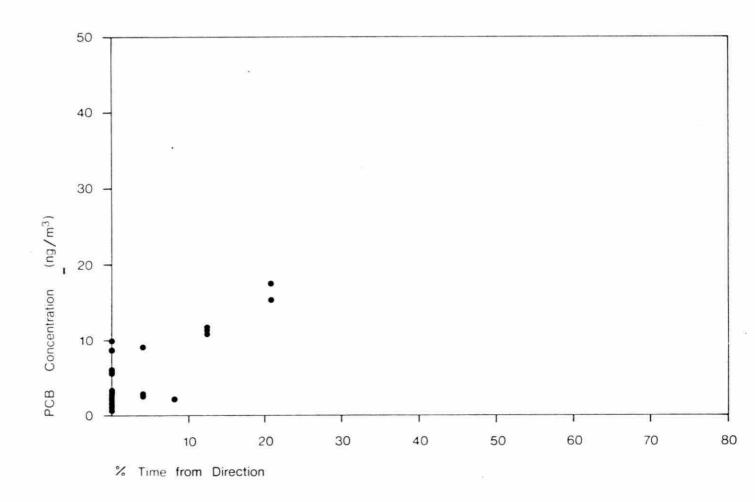


Station MIS-S-U2 Direction S



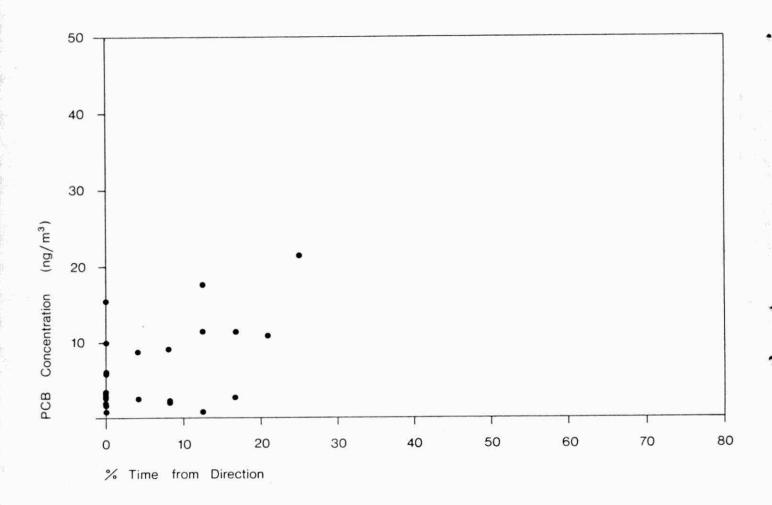


Station MIS-S-U3
Direction SSW



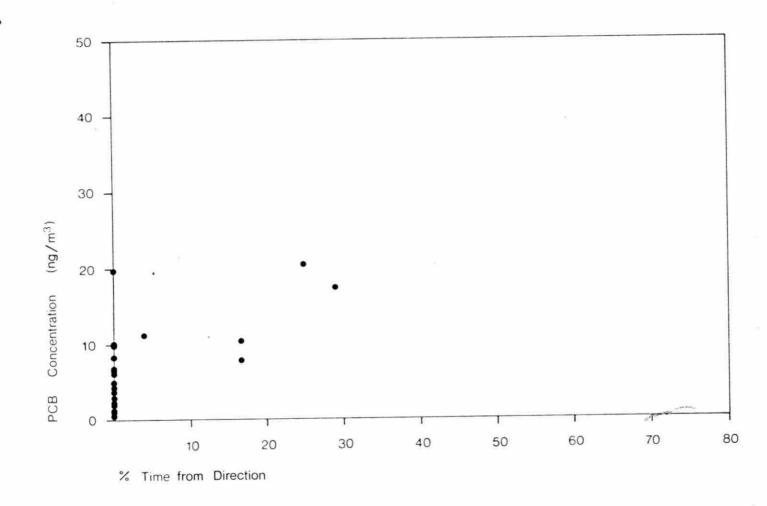


Station MIS-S-U3
Direction S



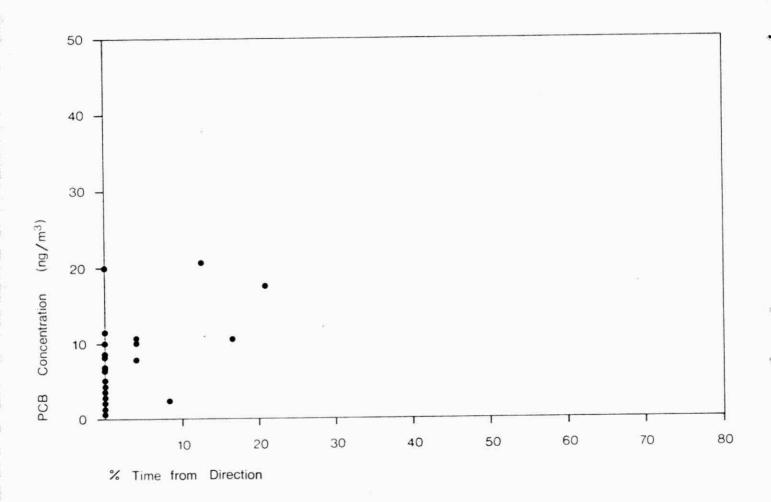


Station SAR-S-I1
Direction NNW



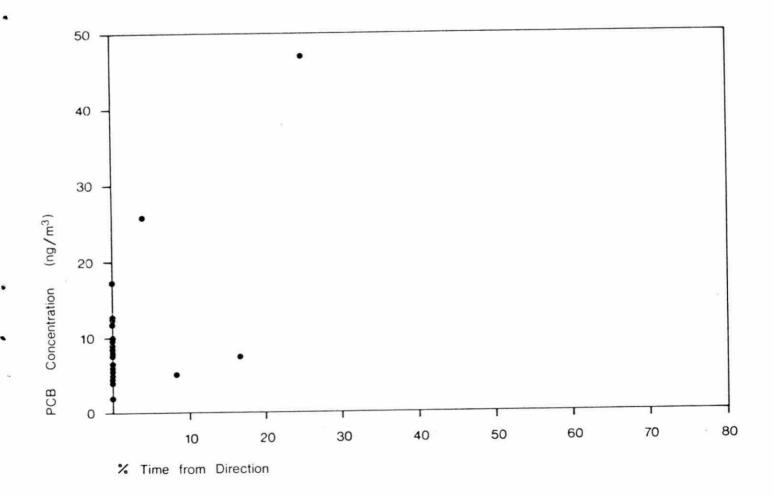


Station SAR-S-I1 Direction NW



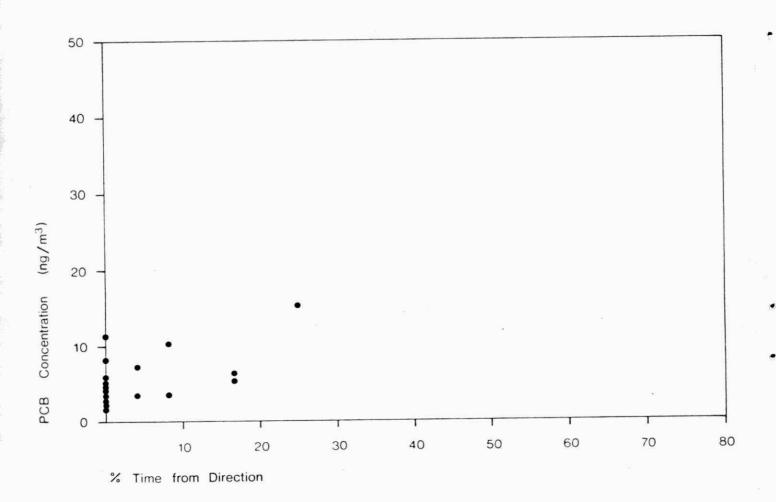


Station SAR-S-U1
Direction NNW



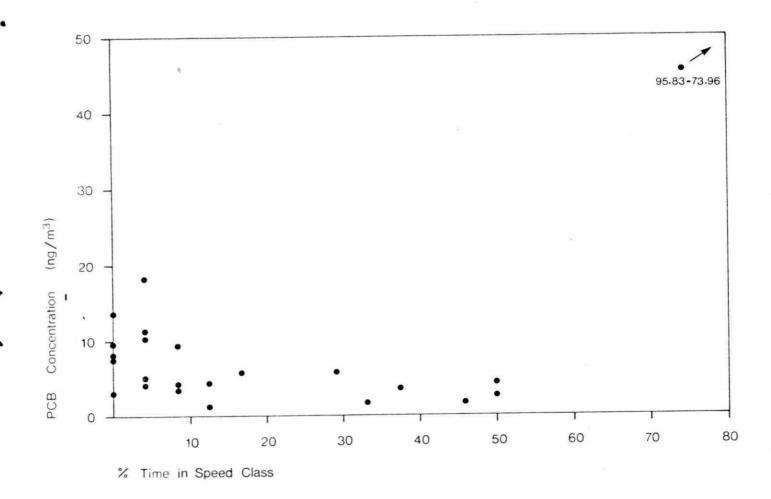


Station TOR-S-S1
Direction N



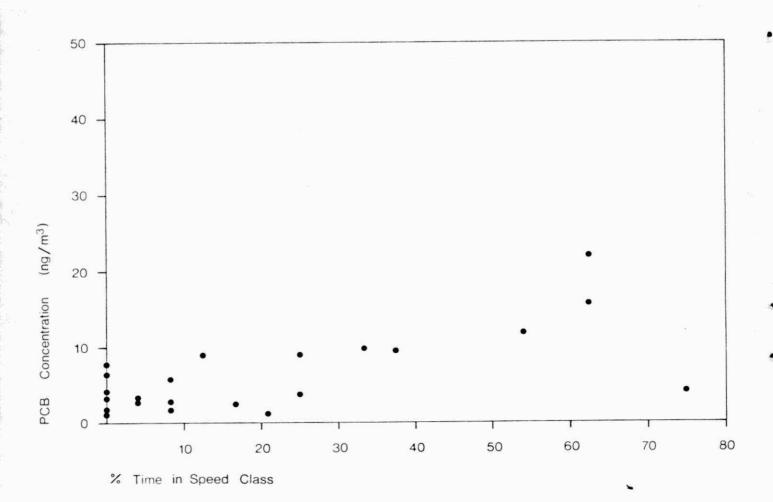


Station HAM-S-U2 Speed Class > 20 km/hr



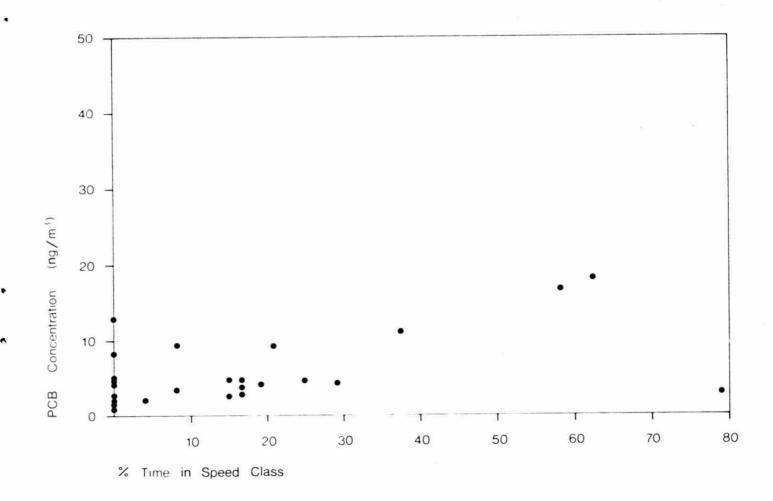


Station HAM-S-U1
Speed Class 0-5 km/hr



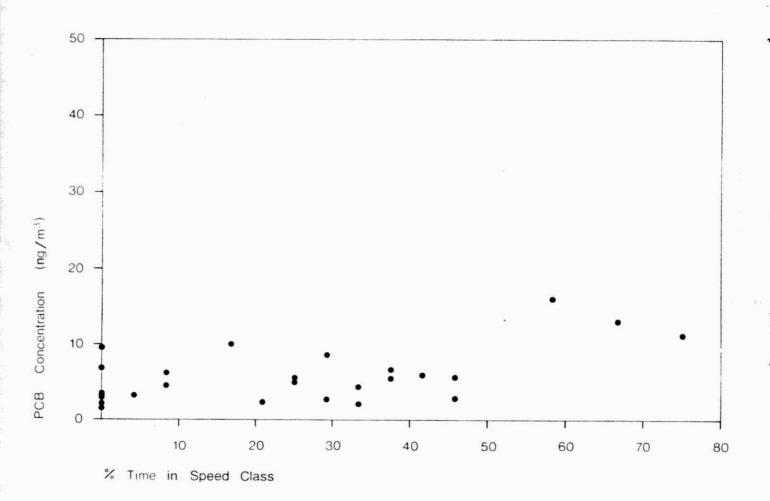


Station HAM-S-I2
Speed Class 0-5 km/hr





Station WIN-S-U1
Speed Class 0-5 km/hr





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